
An Experimental Investigation of Subsonic Flow in a Two-Dimensional U-Duct

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Summary

An experimental study of the low speed internal flow in a two-dimensional strongly-curved U-duct has been conducted in order to acquire fluid dynamic data suitable for evaluating numerical-flow codes. The measurements include surface oil-flow patterns, static pressure distributions obtained with an electronically-scanned pressure system, mean and turbulent velocity profiles acquired with laser-Doppler velocimetry and surface skin friction measured with a laser interferometer skin friction method. The tests were performed at an average Mach number of 0.1, and at Reynolds numbers (based on channel height) of 1×10^5 and 1×10^6 . A high-aspect-ratio geometry together with sidewall boundary-layer suction panels was employed to minimize wall interference effects and obtain nominally two-dimensional flow data.

Nomenclature

AR	aspect ratio (channel width divided by H)
C_f	skin friction coefficient = τ_w/q_{ref}
C_p	static pressure coefficient = $(p - p_{ref})/q_{ref}$
H	channel height (fig. 1)
k	turbulent kinetic energy $\cong 3/4(\langle u'^2 \rangle + \langle v'^2 \rangle)$
M	Mach number
p	static pressure
p_t	total pressure
q	dynamic pressure
Re	Reynolds number based on H and U_b
r	radial distance from center of curvature (fig. 1)
s	downstream distance from channel entrance on duct C.L.
U, V	longitudinal, vertical mean velocities (fig. 1)
u, v	longitudinal, vertical instantaneous velocities

u', v'	longitudinal, vertical instantaneous turbulent velocity fluctuations
$u'v'$	instantaneous turbulent Reynolds stress
x, y	x, y coordinates (fig. 1)
z	transverse direction measured from channel C.L.
θ	angle into bend measured from bend entrance (fig. 1)
ρ	fluid density
τ_t	turbulent shear stress = $-\rho \langle u'v' \rangle$
τ_w	local wall shear stress (or skin friction)
$\langle \rangle$	ensemble (or rms time) average

Superscripts

'	fluctuating component
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Subscripts

b	bulk or average integrated inlet velocity
i, o	inner, outer walls (fig. 1)
r, θ	radial, tangential direction in cylindrical coordinates (fig. 1)
ref	reference conditions based on U_b

Introduction

Computational fluid dynamics (CFD) is beginning to play an increasingly major role in the initial design and/or verification of the internal flow in rocket engine components. Many of these flows have complex flow features such as regions of strong curvature, high turbulence levels, unsteadiness, separation and three-dimensional (3-D) structures. Unfortunately, most existing turbulence models have been developed and verified only for external flows with slight (or no) curvature, so it is not obvious which models can be successfully applied to complex highly-curved internal flows. Therefore, the continued development of computational methods for internal flows requires well-documented experimental studies to suggest better turbulence models and to provide test cases for evaluating new codes. To date, few such experimental studies have been reported.

In response to this need, a basic experimental fluid dynamic study of the low speed internal flow in a two-dimensional strongly-curved U-duct (i.e., 180° bend) has been conducted. The flow contains all of the complex features previously mentioned as often occurring in rocket engine flows. Measurements were made of surface oil-flow patterns, static pressures, mean and turbulent velocities and surface skin friction at a fixed subsonic Mach number, and at a low and at a high Reynolds number. Selected portions of this data were presented in references 1 and 2, where they were compared to CFD predictions using a variety of turbulence models. The objective of the present paper is to provide a complete tabulation of all the experimental data, and to document the test conditions, measurement methods, flowfield uniformity and data accuracy. The presented results should thus provide a comprehensive data base for the validation of numerical simulations.

Apparatus and Techniques

Facility, Test Section and Test Conditions

The investigation was conducted in the NASA Ames High Reynolds Number Channel I (HRC I), which is a blow-down facility using unheated dry air at ambient temperature. The air discharges into a large vacuum sphere for low total pressure runs (i.e., p_t below 2 atm), and into an atmospheric muffler for high total pressure runs (i.e., p_t above 2 atm). The source of high-pressure air is the Ames Underground Air Storage Facility, pressurized to 2×10^7 N/m² (3,000 psi). Available test run times ranged up to 15 min.

A sketch of the 180° turnaround (TAD) or U-duct is shown in figure 1. The entrance nozzle is followed by a rectangular straight upstream section 3.8-cm high, 38-cm wide (i.e., AR of 10), and 83-cm long. The 180° bend has a constant gap spacing equal to the centerline radius of 3.8 cm (i.e., a radius ratio of 1). Following the bend is another 54-cm long straight downstream section. Flow rate is controlled by a throttle plate at the exit of a bottom settling chamber. Large rectangular Plexiglas side windows allowed optical access to the entire bend, and to 12H up or downstream. Inner windows (not shown) incorporated vertical suction slots spaced H apart upstream of the bend to remove the sidewall boundary layers. This minimized "end effects" on the flow in the bend and kept the flow as two-dimensional (2-D) as possible. The two-dimensionality of the flow will be discussed later.

Tests were conducted at a fixed low subsonic Mach number, and at one low and one high Reynolds number. The throttle plate mass flow was adjusted to achieve a nominal M_{ref} of 0.1. Complete data sets were then obtained at p_t of

1.2 and 12 atm, to achieve Re of 1×10^5 and 1×10^6 , respectively. Because the tunnel is a blowdown facility, total temperature varied during a run (and between runs) within the range -18°C to 21°C . During post-run processing, all velocity data were normalized to a reference temperature of -9°C . At this temperature, U_b was 30.1 m/s for $p_t = 1.2$ atm and 31.1 m/s for $p_t = 12$ atm.

Instrumentation

The mean and turbulent velocities were measured with a forward-scattering two-component laser Doppler velocimeter (LDV). A 4-watt argon laser producing paired blue (488 nm) and green (514.5 nm) beams was utilized in the system. One beam of each color was frequency shifted 40 Mhz to avoid directional ambiguity. The measurement directions were fixed at $\pm 45^\circ$ to the tunnel axis, and the data were transformed to the local wall tangential and transverse velocity components. By tilting the beams slightly toward the walls, measurements to within 1 mm of the surfaces were achieved. The LDV was mounted on a computer-controlled traversing carriage which allowed surveys in any radial direction in the bend. A cantilever arm under the tunnel held the receiving optics. Doppler signals were transmitted by a 10-m long optical fiber to remotely-located photomultiplier tubes. Commercial counter-type signal processors set to count 64 Doppler cycles/burst were used to measure the velocities. The flow was seeded with 0.5-micron-diam polystyrene spheres suspended in an alcohol-water mixture. The injection point was sufficiently far upstream to permit the liquid to evaporate by the time the particles reached the test section. Particle lag was estimated to be negligible at the test pressures and flow speeds. Data rates were kept below 1 kHz to provide sufficient time averaging of the flow fluctuations. A total of 5,000 instantaneous velocity pairs were measured at each survey point. At each point, the fraction of the data which exceeded three standard deviations was discarded in forming the velocity histograms. Velocity bias corrections were investigated for selected data sets but were observed to have little effect, so the presented data is all uncorrected. Estimated data accuracy will be discussed later.

The static pressure was measured using a commercial electronically-scanned pressure system. The pressure taps were located on one sidewall, and were distributed along the channel centerline as well as the corner junctions between the sidewall and the inner and outer walls. A potential source of error in interpreting the measured pressures in the bend is the crossflow that normally occurs from the outer wall to the inner wall through the sidewall boundary layer (bl). This causes a turning in of the flow on the inner wall and therefore results in a transverse pressure

gradient. This error was minimized in the present test by utilizing the previously-described sidewall suction. The amount of suction was adjusted until surface oil flows showed that the turning in of the flow was nearly eliminated, and no further changes in measured pressures on the inner wall in the bend occurred. The outer wall pressures and the inner wall pressures up and downstream of the bend were unaffected by the amount of sidewall suction.

The surface skin friction was measured on the centerline of the inner and outer walls of the TAD using a laser interferometer skin friction (LISF) measurement technique (ref. 3). This method uses an incident He-Ne laser beam to measure the rate of change of thickness of a thin oil film applied to the test surface. Knowledge of the rate of thickness change and other properties of the oil are sufficient for calculation of the skin friction with no additional assumptions about the nature of the boundary layer. Measurements could not be performed on the outer wall in the bend because dust centrifuged into the oil in that region disrupted the reflected laser beam.

Error Analysis

The electronically-scanned pressure system measured static pressures to within an uncertainty of ± 0.005 psid. This corresponds to an uncertainty in C_p of ± 0.1 and ± 0.01 at Re of 1×10^5 and 1×10^6 , respectively. The estimated uncertainty in the LISF C_f measurements is $\pm 5\%$ for this speed range (ref. 3).

For the LDV system, the factors which affect the estimated errors will be divided into three groups. The first group consists of those fixed geometric uncertainties which are invariant during a test run, such as beam crossing angles, fringe orientation, etc., and they were evaluated by standard uncertainty analyses. The second group contains the random variations introduced by sample size and turbulence level statistics, and they were evaluated by standard statistical analyses. The third group contains the errors due to signal noise associated with window defects, laser beam flare at the walls, accumulation of LDV particles on the windows, etc. Also included in the third group is scatter in the data in some regions of the flow arising from large-scale unsteadiness. The factors in the third group can't be quantified exactly, but they were approximately evaluated from the repeatability between the many redundant and/or closely-spaced data points which were accumulated for each profile. The uncertainties computed for the measured quantities for the three groups are presented in table 1. The two values given for group 3 errors refer to quiescent and highly-unsteady regions of the flow, respectively. Also shown are the root-sum-square and worst-case combinations. One can see that the third group

accounts for the largest errors in the data. Finally, positioning accuracy for the LDV survey mechanism was within ± 0.03 mm for both axes.

Results and Discussion

The experimental results of this investigation consist of velocity profiles, static-pressure distributions, skin-friction distributions and surface oil-flow patterns. Each result will be discussed separately, and then the issues of Reynolds-number effects and flowfield uniformity will be discussed.

Velocity Profiles

The velocity profiles measured in the TAD are given in tables 2-23 and plotted in figures 2-23 for both $Re = 1 \times 10^5$ and 1×10^6 . Surveys were taken at twenty two axial locations ranging from $x/H = -4$ upstream of the bend, to $x/H = 12$ downstream of the bend, including six locations in the bend itself. Data were taken at both Re on the channel centerline (i.e., $z/H = 0$), and at four transverse positions (i.e., $z/H = 0, 1, 2, 3$) for selected axial locations at $Re = 1 \times 10^6$. The tabulated data consist of four columns, which respectively present the normal distance from the inner wall, axial velocity, vertical velocity, turbulent kinetic energy (TKE) and turbulent shear stress (TSS). The distances are normalized by H and the velocities are nondimensionalized using U_b . Each of the above quantities is also plotted in the correspondingly numbered figures which follow each table. Note that in the plots, k is redefined as 50% larger than the tabulated TKE to approximately account for the unmeasured third component of velocity. This allows a direct comparison of the plotted k with turbulence models that include the three components.

A brief description of the observed flow in the TAD will now be given to aid in the interpretation of the velocity profiles. The flow upstream of the bend at $x/H = -4$ (fig. 2) has fully-turbulent bl's on each wall of about $0.25H$ thickness each, and an inviscid core occupying the remainder of the channel with a measured TKE of about 0.02% of U_b^2 . The flow is not quite symmetric at this station due to an asymmetric entrance section. In the first half of the bend (figs. 6-9), the flow accelerates near the inner wall and decelerates near the outer wall. The TKE and TSS are suppressed near the inner wall, which is consistent with other studies (ref. 4) on the effects of convex curvature on turbulent bl's. Conversely, the TKE and TSS are enhanced near the outer wall, which is also consistent with other studies (ref. 5) on the effects of concave curvature on turbulent bl's. In the second half of the bend (figs. 10-12), the flow decelerates on the inner wall and accelerates on the outer wall. The flow separates on the inner wall near the end of the bend, and reattaches by $x/H = 1.5$ (fig. 15). This unsteady separation creates large peaks in TKE and TSS

near the inner wall. Further downstream (figs. 16-23), the turbulence peaks gradually diffuse across the channel and decay, while the mean velocities gradually relax towards a symmetrical profile once again. However, when the end of the duct is reached (i.e., $x/H = 12$), significant turbulence persists in the entire flow and the velocity profiles remain "fuller" than they were upstream of the bend.

Static Pressure and Skin Friction Distributions

The measured static pressure (C_p) and surface skin friction (C_f) distributions in the TAD are given in table 24 and plotted in figure 24. Note that in the tabulated data, not all measurements were made at every position.

The C_p and C_f distributions in figure 24 are consistent with what was previously observed for the velocity profiles. In the first half of the bend, the pressure drops on the inner wall as the flow there accelerates, and rises on the outer wall as the flow there decelerates. In the second half of the bend, the opposite effects occur, leading to the previously-discussed separation of the bl on the inner wall. Downstream of the bend, C_p levels out at a value below the upstream level. This pressure drop represents the dissipation losses in the flow that are caused by the presence of the bend. The skin friction, C_f , on the inner wall rises steeply in the first half of the bend as the flow accelerates. Near the end of the bend, the inner wall C_f plunges steeply to negative values as the flow separates. Downstream of the bend, both C_f distributions recover and overshoot their upstream values before relaxing back towards those levels.

Surface Oil-Flow Patterns

The surface oil-flow patterns on the TAD inner and outer walls for $Re = 1 \times 10^6$ are shown in figure 25. The patterns extend from 90° in the bend to $x/H = 6$ downstream of the bend, and span the channel between the side walls (i.e., $z/H = -5$ to 5). A fairly straight separation line is observed on the inner wall at about $\theta = 135^\circ$. The separation is caused by an adverse pressure gradient on the inner wall. Although difficult to see, a reattachment line is observed downstream of the bend near $x/H = 1$. Although the goal was to achieve a nominally 2-D flow, some 3-D structures are observed downstream of reattachment on both walls. This issue will be discussed later. Although not shown, similar oil-flow patterns were obtained for $Re = 1 \times 10^5$.

Reynolds Number Effects

One of the goals of this investigation was to test at two widely-separated Re 's to look for Re effects on this type of internal flow. The observed effects are summarized in this section.

From $x/H = -4$ (fig. 2) to $\theta = 60^\circ$ (fig. 8), little difference in measured velocities and turbulence quantities is observed between the two Re 's. Between $\theta = 90^\circ$ (fig. 9) and $\theta = 150^\circ$ (fig. 11), mean velocity profiles remain the same, but peak TKE and TSS for $Re = 1 \times 10^5$ fall considerably below those values for 1×10^6 . Near the end of the bend (figs. 12-14), the mean velocity profiles deviate since separation is much less at $Re = 1 \times 10^5$ than at 1×10^6 . The differences in TKE and TSS are also more pronounced. In the recovery region downstream of the bend (figs. 16-23), the difference between the two Re 's for all quantities once again gradually disappears as the flows relax toward symmetrical profiles.

For the C_p and C_f distributions (fig. 24), some Re effects are also observed. The C_p for $Re = 1 \times 10^5$ is somewhat lower than for 1×10^6 both up and downstream of the bend. The opposite situation is observed for the C_f data. Also, the different amounts of separation for the two Re 's results in considerably higher C_f levels near the end of the bend for $Re = 1 \times 10^5$ than for 1×10^6 .

Flowfield Uniformity

A major concern of this study was to create a nominally 2-D flowfield in the TAD so that comparisons with CFD would not require complex (and uncertain) 3-D corrections. Three-dimensional flow can occur from either sidewall effects, or from processes associated with flow separation and reattachment. These effects will be considered separately.

Two features were incorporated into the design of the TAD to minimize sidewall effects on the flow. First, the channel was built with as large an AR as possible (i.e., $AR = 10$). Second, as previously discussed, sidewall bl suction was incorporated upstream of the bend to thin those bl's. These two features were quite effective in limiting "end effects" on the flow, as can be seen from the oil flows in figure 25. There it can be seen that "turning in" of the flow is limited to a narrow region within $0.5H$ of the sidewalls for both inner and outer walls. This was not the case with the suction turned off. In that case (not shown), significant "turning in" of the flow occurred as far inward from the sidewalls as $1.5H$ for both the inner and outer walls.

A more significant 3-D effect on the flow occurred as a result of flow separation on the TAD inner wall, as can be seen from the oil flow of figure 25(a). At about $z/H = \pm 1$, convergent and divergent flow singularities (i.e., saddle and nodal points) are observed on the separation and reattachment lines, respectively. (They are difficult to see on the figure, but were apparent on the original oil flow.) Downstream of the reattachment nodes, the effects of

counter-rotating pairs of longitudinal vortices are observed. They appear to extend across the channel since some effects are also observed on the outer-wall oil flow (fig. 25(b)). Similar structures have occurred in other nominally 2-D separated flows. For example, Petrie et al. (ref. 6) as well as Ginoux (ref. 7) have observed spanwise cells downstream of reattachment on backward-facing step-flow configurations in supersonic flow. Also, G. Mateer (private communication, 1992) has measured similar transverse cells in the separation region on an axisymmetric open pipe in supersonic flow. Inger (ref. 8) presents a vortex instability model to explain these observed structures. These 3-D structures therefore seem to be common in many types of nominally 2-D separated flows, and are apparently unrelated to the presence or absence of side-walls in the test geometry.

As might be expected, the described 3-D flow structures have some influence on the measured velocity profiles. The flow is 2-D in all respects upstream and in the first half of the bend (see figs. 2-8). In the second half of the bend (see figs. 9-12), the mean velocities remain 2-D, whereas the turbulence quantities reveal some 3-D structures near the outer wall. Downstream of reattachment (see figs. 14-23), the axial mean velocity and turbulence profiles are for the most part similar for $z/H = 0, 2, 3$ but quite different for $z/H = 1$, which is the location of the previously described nodes in the oil-flow patterns. Consequently, it can be concluded that the present TAD data is nominally 2-D except for the velocity data at $z/H = 1$. Data at that transverse location should not be used to compare with 2-D CFD calculations.

Concluding Remarks

Detailed experimental data have been obtained for the flow in a two-dimensional turnaround or U-duct with very strong curvature. The data consist of surface oil flows, static pressures, mean velocities, turbulence stresses and surface skin friction. The flow Mach number was 0.1, and Reynolds number was 1×10^5 and 1×10^6 . The significant observations about the flow are: 1) large turbulence enhancement occurs near the outer (concave) wall; 2) almost total damping of turbulence occurs near the inner (convex) wall; 3) separation, the extent of which increases with increasing Reynolds number, occurs on the inner wall at the bend exit; and 4) high levels of turbulence and unsteadiness occur in all regions of the flow downstream of the bend. These data will be useful for validating turbulence models and numerical codes for computing internal flows such as rocket-engine components and other complex geometries.

References

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Appendix

The data files generated by this study are included on a 3.5-inch low-density diskette inside the back report cover. The diskette is formatted in MS-DOS (UNIX-formatted high-density diskettes are also available from the authors). An explanation file, *instruct.txt*, is included on the diskette. Two files contain pressure and skin friction data, and the remainder contain the LDV mean velocity and turbulence data presented in this report.

The LDV data is given in files named "*Re exp*" "*x/H(or θ)*" "*z/H*". For example, *6_0_0.dat* would be a file for $Re = 1 \times 10^6$, $\theta = 0^\circ$ and $z/H = 0$. A sample LDV file with the name *5_8_0.dat* for $Re = 1 \times 10^5$, $x/H = 8$ and $z/H = 0$ is shown in figure 26. The first line is an integer variable which gives the total rows of data in the file. This number can range up to 100. The rest of the file presents five columns of LDV data. The first column is y/H , the second column is U (m/s), the third column is V (m/s), the fourth column is $1/2(\langle u'^2 \rangle + \langle v'^2 \rangle)$ (m²/s²), and the fifth column is $\langle u'v' \rangle$ (m²/s²). The data may be read into a two-dimensional array dimensioned as `ftarr(5, 100)`.

The pressure and skin friction data is given in two files named "*Re exp*" "*C_p-C_f*". The file *5_C_p-C_f.dat* for $Re = 1 \times 10^5$ is shown in figure 27. Once again, the first line is an integer variable giving the total rows of data in the file. The rest of the file presents seven columns of C_p and C_f data. The first column is s/H , the second column is x/H , the third column is θ (deg), the fourth column is C_p on the inner wall, the fifth column is C_p on the outer wall, the sixth column is C_f on the inner wall, and the seventh column is C_f on the outer wall. The data may be read into a two-dimensional array dimensioned as `ftarr(7, 32)`. Notice in each column that some values equal 100.0. Whenever that occurs, no measurements were made for that variable at that location. Thus the value 100.0 can be used as a test to identify locations that should be deleted from the C_p and C_f data sets.

Table 1. Laser Doppler Velocimetry (LDV) Uncertainties

Quantity	Group 1 (geometry)	Group 2 (statistics)	Group 3 (noise)	Worst case	Root-sum-square
U	$\pm 2\%$	$\pm 0.5\%$	$\pm 1-4\%$	$\pm 6.5\%$	$\pm 2.3-4.5\%$
V	$\pm 0.027U$	$\pm 0.5\%$	$\pm 0.01U$	$\pm 0.037U \pm 0.005V$	$\pm 0.029U \pm 0.005V$
$\langle u'v' \rangle$	$\pm 2\%$	$\pm 3\%$	$\pm 2-7\%$	$\pm 12\%$	$\pm 4.1-7.9\%$
$\langle u'^2 + v'^2 \rangle$	$\pm 2\%$	$\pm 3\%$	$\pm 2-5\%$	$\pm 10\%$	$\pm 4.1-6.2\%$

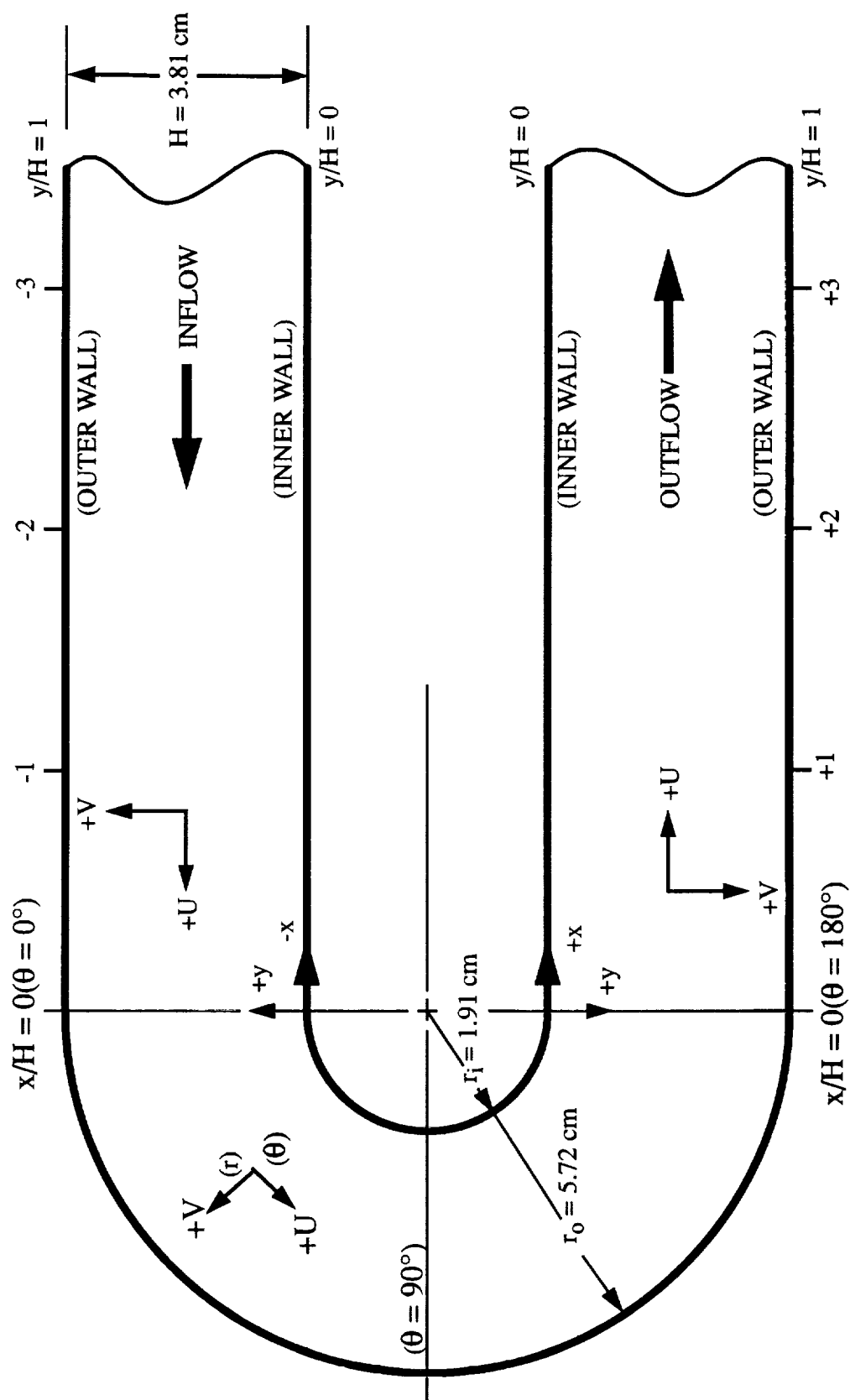


Figure 1. Coordinate system for Ames HRC I turnaround duct (TAD).

Table 2. LDV flowfield in TAD (x/H = -4)

(Re = 1×10^5 , $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.022	0.723	1.656 ⁻³	5.477 ⁻³	-1.531 ⁻³	0.522	1.086	-3.269 ⁻⁴	1.895 ⁻⁴	1.454 ⁻⁵
0.028	0.741	-1.250 ⁻³	4.768 ⁻³	-1.578 ⁻³	0.542	1.083	-5.222 ⁻³	1.924 ⁻⁴	-1.248 ⁻⁵
0.035	0.762	-3.000 ⁻³	4.173 ⁻³	-1.407 ⁻³	0.548	1.091	1.872 ⁻³	2.216 ⁻⁴	5.698 ⁻⁵
0.042	0.784	-4.111 ⁻³	3.847 ⁻³	-1.433 ⁻³	0.562	1.084	-2.656 ⁻³	1.286 ⁻⁴	-4.179 ⁻⁵
0.048	0.800	-3.750 ⁻³	3.655 ⁻³	-1.269 ⁻³	0.575	1.090	2.782 ⁻³	1.812 ⁻⁴	2.820 ⁻⁵
0.055	0.819	-6.099 ⁻³	3.815 ⁻³	-1.385 ⁻³	0.582	1.082	-9.630 ⁻³	2.338 ⁻⁴	1.912 ⁻⁵
0.062	0.833	-6.274 ⁻³	3.669 ⁻³	-1.197 ⁻³	0.602	1.088	-4.960 ⁻³	2.098 ⁻⁴	3.043 ⁻⁵
0.068	0.840	-5.999 ⁻³	3.613 ⁻³	-1.292 ⁻³	0.622	1.084	-4.285 ⁻³	2.132 ⁻⁴	2.043 ⁻⁵
0.075	0.854	-6.834 ⁻³	3.506 ⁻³	-1.192 ⁻³	0.628	1.091	2.717 ⁻³	2.006 ⁻⁴	3.571 ⁻⁵
0.082	0.866	-7.621 ⁻³	3.311 ⁻³	-1.218 ⁻³	0.655	1.092	2.732 ⁻³	2.016 ⁻⁴	4.489 ⁻⁵
0.088	0.875	-6.090 ⁻³	3.130 ⁻³	-1.139 ⁻³	0.662	1.084	-6.688 ⁻³	2.213 ⁻⁴	3.027 ⁻⁵
0.098	0.898	-6.419 ⁻³	3.042 ⁻³	-9.933 ⁻⁴	0.675	1.078	-9.521 ⁻³	3.752 ⁻⁴	1.173 ⁻⁴
0.108	0.908	-5.924 ⁻³	2.900 ⁻³	-9.551 ⁻⁴	0.688	1.080	-7.638 ⁻³	2.645 ⁻⁴	5.335 ⁻⁵
0.118	0.920	-6.874 ⁻³	2.834 ⁻³	-9.217 ⁻⁴	0.702	1.081	-7.143 ⁻³	2.529 ⁻⁴	5.538 ⁻⁵
0.128	0.940	-7.066 ⁻³	2.478 ⁻³	-7.584 ⁻⁴	0.708	1.093	3.291 ⁻³	2.341 ⁻⁴	8.135 ⁻⁵
0.138	0.954	-7.354 ⁻³	2.326 ⁻³	-6.309 ⁻⁴	0.715	1.079	-7.508 ⁻³	3.442 ⁻⁴	9.960 ⁻⁵
0.148	0.961	-7.810 ⁻³	2.214 ⁻³	-6.196 ⁻⁴	0.728	1.082	-4.261 ⁻³	2.681 ⁻⁴	5.872 ⁻⁵
0.158	0.977	-7.300 ⁻³	1.910 ⁻³	-5.202 ⁻⁴	0.735	1.092	3.625 ⁻³	2.858 ⁻⁴	1.036 ⁻⁴
0.168	0.990	-7.547 ⁻³	1.763 ⁻³	-4.965 ⁻⁴	0.742	1.077	-8.464 ⁻³	4.145 ⁻⁴	1.224 ⁻⁴
0.178	1.004	-5.602 ⁻³	1.673 ⁻³	-3.323 ⁻⁴	0.755	1.070	-8.751 ⁻³	6.014 ⁻⁴	1.710 ⁻⁴
0.188	1.007	-4.568 ⁻³	1.534 ⁻³	-3.254 ⁻⁴	0.762	1.079	1.899 ⁻³	7.031 ⁻⁴	2.406 ⁻⁴
0.202	1.023	-4.441 ⁻³	1.375 ⁻³	-2.681 ⁻⁴	0.782	1.065	-7.668 ⁻³	7.449 ⁻⁴	1.854 ⁻⁴
0.215	1.034	-3.757 ⁻³	1.467 ⁻³	-1.638 ⁻⁴	0.795	1.059	-8.599 ⁻³	9.918 ⁻⁴	2.631 ⁻⁴
0.222	1.054	-8.293 ⁻³	7.753 ⁻⁴	-1.272 ⁻⁴	0.805	1.067	-5.543 ⁻³	7.737 ⁻⁴	1.869 ⁻⁴
0.228	1.051	-5.885 ⁻³	9.215 ⁻⁴	-1.501 ⁻⁴	0.815	1.053	-8.229 ⁻³	1.185 ⁻³	2.982 ⁻⁴
0.242	1.055	-2.010 ⁻³	8.407 ⁻⁴	-1.250 ⁻⁴	0.825	1.051	-7.111 ⁻³	1.284 ⁻³	3.100 ⁻⁴
0.248	1.067	-7.172 ⁻³	5.114 ⁻⁴	-8.135 ⁻⁵	0.835	1.048	-7.226 ⁻³	1.414 ⁻³	3.017 ⁻⁴
0.255	1.059	-1.376 ⁻³	8.291 ⁻⁴	-1.022 ⁻⁴	0.845	1.055	-5.941 ⁻³	1.172 ⁻³	2.731 ⁻⁴
0.268	1.066	-4.172 ⁻⁴	7.034 ⁻⁴	-5.175 ⁻⁵	0.855	1.026	-6.944 ⁻³	2.088 ⁻³	5.073 ⁻⁴
0.275	1.069	-6.011 ⁻³	4.713 ⁻⁴	-7.329 ⁻⁵	0.865	1.037	-5.914 ⁻³	1.737 ⁻³	3.847 ⁻⁴
0.282	1.070	-7.756 ⁻⁵	5.943 ⁻⁴	-2.385 ⁻⁵	0.875	1.026	-3.482 ⁻³	2.185 ⁻³	4.818 ⁻⁴
0.302	1.075	-7.988 ⁻³	2.994 ⁻⁴	-4.873 ⁻⁵	0.885	1.036	-1.767 ⁻³	1.810 ⁻³	3.075 ⁻⁴
0.308	1.074	9.607 ⁻⁴	4.724 ⁻⁴	-2.068 ⁻⁵	0.895	1.014	-3.198 ⁻³	2.676 ⁻³	5.463 ⁻⁴
0.328	1.077	-5.591 ⁻³	2.630 ⁻⁴	-3.163 ⁻⁵	0.902	0.999	-1.938 ⁻³	3.116 ⁻³	5.916 ⁻⁴
0.342	1.079	1.459 ⁻³	3.609 ⁻⁴	5.626 ⁻⁵	0.908	0.987	-3.872 ⁻³	3.169 ⁻³	6.479 ⁻⁴
0.355	1.080	-6.315 ⁻³	1.744 ⁻⁴	-1.886 ⁻⁵	0.915	1.000	-1.289 ⁻³	3.029 ⁻³	6.219 ⁻⁴
0.382	1.081	-4.895 ⁻⁴	2.174 ⁻⁴	-7.052 ⁻⁶	0.922	0.985	-1.692 ⁻³	3.632 ⁻³	6.821 ⁻⁴
0.402	1.084	3.046 ⁻³	2.259 ⁻⁴	-5.974 ⁻⁶	0.928	0.952	-3.468 ⁻³	4.005 ⁻³	7.558 ⁻⁴
0.408	1.081	-3.525 ⁻³	1.411 ⁻⁴	-1.227 ⁻⁵	0.935	0.943	-3.552 ⁻³	3.974 ⁻³	8.243 ⁻⁴
0.422	1.084	1.821 ⁻³	2.590 ⁻⁴	6.710 ⁻⁵	0.942	0.952	-2.670 ⁻³	4.003 ⁻³	6.654 ⁻⁴
0.435	1.084	-3.871 ⁻³	1.497 ⁻⁴	-1.162 ⁻⁵	0.948	0.945	-1.859 ⁻³	4.708 ⁻³	8.804 ⁻⁴
0.482	1.087	-4.642 ⁻³	1.907 ⁻⁴	5.350 ⁻⁶	0.955	0.915	-6.612 ⁻⁴	5.042 ⁻³	7.584 ⁻⁴
0.502	1.086	-3.307 ⁻³	1.895 ⁻⁴	5.473 ⁻⁶	0.962	0.924	2.294 ⁻³	5.911 ⁻³	1.175 ⁻³

Table 2. Continued ($x/H = -4$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.019	0.749	3.683^{-3}	2.708^{-3}	-9.480^{-4}	0.499	1.081	7.399^{-3}	1.738^{-4}	-8.441^{-6}
0.026	0.776	3.146^{-3}	2.620^{-3}	-8.568^{-4}	0.519	1.082	5.627^{-3}	1.773^{-4}	-4.519^{-6}
0.032	0.804	8.945^{-4}	2.758^{-3}	-9.109^{-4}	0.539	1.077	6.993^{-3}	2.416^{-4}	1.079^{-5}
0.039	0.818	3.491^{-3}	2.456^{-3}	-7.744^{-4}	0.546	1.087	6.351^{-3}	1.915^{-4}	-8.851^{-6}
0.046	0.828	3.280^{-3}	2.423^{-3}	-7.439^{-4}	0.572	1.087	6.577^{-3}	1.850^{-4}	1.949^{-6}
0.052	0.842	2.345^{-3}	2.251^{-3}	-7.987^{-4}	0.599	1.082	7.218^{-3}	1.841^{-4}	5.609^{-6}
0.059	0.862	2.086^{-3}	2.334^{-3}	-6.729^{-4}	0.619	1.076	1.156^{-2}	2.239^{-4}	2.015^{-5}
0.066	0.852	3.369^{-3}	2.325^{-3}	-6.917^{-4}	0.626	1.087	5.529^{-3}	1.760^{-4}	5.137^{-6}
0.072	0.885	1.541^{-3}	2.151^{-3}	-6.627^{-4}	0.639	1.075	7.643^{-3}	2.852^{-4}	4.663^{-5}
0.079	0.903	1.015^{-3}	2.108^{-3}	-6.486^{-4}	0.652	1.085	1.159^{-2}	1.685^{-4}	-9.510^{-6}
0.086	0.912	1.147^{-3}	1.850^{-3}	-4.972^{-4}	0.659	1.075	9.019^{-3}	2.707^{-4}	6.054^{-5}
0.096	0.931	1.869^{-3}	1.944^{-3}	-6.109^{-4}	0.679	1.079	6.357^{-3}	3.155^{-4}	9.039^{-5}
0.106	0.942	2.061^{-4}	1.748^{-3}	-5.121^{-4}	0.692	1.074	8.885^{-3}	2.480^{-4}	7.040^{-5}
0.116	0.957	6.825^{-4}	1.803^{-3}	-4.960^{-4}	0.706	1.081	6.560^{-3}	2.520^{-4}	4.617^{-5}
0.126	0.969	2.524^{-3}	1.717^{-3}	-4.738^{-4}	0.719	1.073	8.892^{-3}	3.258^{-4}	1.074^{-4}
0.136	0.983	1.508^{-3}	1.392^{-3}	-3.274^{-4}	0.732	1.079	6.635^{-3}	2.933^{-4}	8.252^{-5}
0.146	1.005	1.653^{-3}	1.292^{-3}	-3.742^{-4}	0.746	1.074	9.700^{-3}	3.405^{-4}	9.703^{-5}
0.156	0.998	2.310^{-3}	1.327^{-3}	-3.389^{-4}	0.759	1.076	5.716^{-3}	4.445^{-4}	1.389^{-4}
0.166	0.995	3.338^{-3}	1.253^{-3}	-3.402^{-4}	0.772	1.064	8.025^{-3}	5.872^{-4}	1.620^{-4}
0.176	1.016	3.948^{-3}	1.044^{-3}	-2.897^{-4}	0.786	1.063	8.883^{-3}	6.737^{-4}	2.370^{-4}
0.186	1.027	3.330^{-3}	1.023^{-3}	-2.766^{-4}	0.799	1.058	6.166^{-3}	8.311^{-4}	3.126^{-4}
0.199	1.028	4.512^{-3}	9.549^{-4}	-2.448^{-4}	0.812	1.049	6.739^{-3}	1.357^{-3}	5.656^{-4}
0.212	1.045	3.506^{-3}	7.296^{-4}	-1.620^{-4}	0.822	1.055	9.546^{-3}	1.028^{-3}	4.151^{-4}
0.226	1.043	4.952^{-3}	7.615^{-4}	-1.466^{-4}	0.832	1.035	4.783^{-3}	1.574^{-3}	5.159^{-4}
0.239	1.065	4.791^{-3}	3.822^{-4}	-8.397^{-5}	0.842	1.034	6.107^{-3}	2.036^{-3}	7.024^{-4}
0.252	1.068	2.732^{-3}	3.960^{-4}	-7.962^{-5}	0.852	1.024	5.261^{-3}	2.110^{-3}	7.527^{-4}
0.266	1.067	6.788^{-3}	2.496^{-4}	-2.330^{-5}	0.862	1.017	6.508^{-3}	1.806^{-3}	6.314^{-4}
0.279	1.072	5.384^{-3}	2.218^{-4}	-1.012^{-5}	0.872	1.021	8.417^{-3}	2.181^{-3}	7.607^{-4}
0.292	1.074	6.015^{-3}	1.917^{-4}	-1.344^{-5}	0.882	1.020	8.714^{-3}	2.130^{-3}	6.840^{-4}
0.306	1.076	5.784^{-3}	1.545^{-4}	-1.442^{-5}	0.892	0.975	3.757^{-3}	2.803^{-3}	8.571^{-4}
0.319	1.074	5.825^{-3}	1.977^{-4}	-2.674^{-5}	0.902	0.984	7.296^{-3}	2.641^{-3}	8.627^{-4}
0.339	1.078	4.694^{-3}	1.629^{-4}	-2.305^{-5}	0.912	0.973	4.844^{-3}	2.619^{-3}	8.147^{-4}
0.346	1.076	2.729^{-3}	1.802^{-4}	-1.637^{-5}	0.919	0.951	5.153^{-3}	2.756^{-3}	7.996^{-4}
0.359	1.078	4.193^{-3}	1.338^{-4}	-9.298^{-7}	0.926	0.946	4.914^{-3}	2.913^{-3}	1.009^{-3}
0.372	1.073	6.896^{-3}	1.705^{-4}	-1.250^{-5}	0.932	0.936	4.054^{-3}	3.053^{-3}	8.057^{-4}
0.379	1.082	6.449^{-3}	1.643^{-4}	-1.442^{-5}	0.939	0.904	-7.767^{-6}	3.688^{-3}	1.092^{-3}
0.399	1.077	6.826^{-3}	1.610^{-4}	-9.285^{-6}	0.946	0.894	-3.119^{-5}	3.740^{-3}	1.056^{-3}
0.419	1.083	8.380^{-3}	1.623^{-4}	-1.408^{-5}	0.952	0.879	3.353^{-3}	3.716^{-3}	9.833^{-4}
0.426	1.075	7.188^{-3}	1.775^{-4}	-3.960^{-6}	0.959	0.872	1.853^{-3}	3.776^{-3}	9.976^{-4}
0.439	1.083	4.645^{-3}	1.843^{-4}	-2.495^{-5}	0.966	0.847	3.119^{-3}	3.794^{-3}	9.854^{-4}
0.452	1.076	6.976^{-3}	1.781^{-4}	-4.439^{-6}	0.972	0.823	2.535^{-3}	4.171^{-3}	1.058^{-3}
0.459	1.083	9.742^{-3}	1.416^{-4}	-9.261^{-6}	0.979	0.797	2.741^{-3}	4.257^{-3}	9.989^{-4}
0.479	1.080	8.402^{-3}	1.568^{-4}	-6.581^{-6}					

Table 2. Continued ($x/H = -4$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.019	0.786	4.385 ⁻³	3.255 ⁻³	-1.065 ⁻³	0.459	1.086	-7.796 ⁻³	2.724 ⁻⁴	4.721 ⁻⁵
0.026	0.810	3.220 ⁻³	3.078 ⁻³	-8.794 ⁻⁴	0.479	1.082	-5.552 ⁻³	3.054 ⁻⁴	3.914 ⁻⁵
0.032	0.844	7.479 ⁻⁴	3.100 ⁻³	-7.638 ⁻⁴	0.499	1.086	-4.434 ⁻⁴	2.397 ⁻⁴	-1.213 ⁻⁵
0.039	0.861	3.108 ⁻³	2.969 ⁻³	-7.833 ⁻⁴	0.519	1.084	-7.773 ⁻³	2.973 ⁻⁴	3.668 ⁻⁵
0.046	0.863	9.641 ⁻⁴	2.799 ⁻³	-8.899 ⁻⁴	0.539	1.079	-4.224 ⁻³	3.050 ⁻⁴	3.027 ⁻⁵
0.052	0.892	2.597 ⁻³	2.870 ⁻³	-7.930 ⁻⁴	0.546	1.087	1.831 ⁻³	2.840 ⁻⁴	4.778 ⁻⁵
0.059	0.898	2.411 ⁻³	2.639 ⁻³	-7.757 ⁻⁴	0.559	1.078	-4.606 ⁻³	3.019 ⁻⁴	4.812 ⁻⁶
0.066	0.919	2.606 ⁻³	2.597 ⁻³	-6.438 ⁻⁴	0.572	1.086	-3.065 ⁻³	3.043 ⁻⁴	8.342 ⁻⁵
0.072	0.940	1.945 ⁻³	2.430 ⁻³	-7.103 ⁻⁴	0.579	1.079	-3.226 ⁻³	3.127 ⁻⁴	5.526 ⁻⁵
0.079	0.913	4.093 ⁻³	2.089 ⁻³	-7.152 ⁻⁴	0.599	1.082	-3.252 ⁻³	3.369 ⁻⁴	9.897 ⁻⁵
0.086	0.942	2.123 ⁻³	2.299 ⁻³	-6.635 ⁻⁴	0.619	1.080	-1.433 ⁻³	2.509 ⁻⁴	1.495 ⁻⁵
0.096	0.969	3.097 ⁻³	2.100 ⁻³	-4.807 ⁻⁴	0.626	1.080	-1.686 ⁻³	5.079 ⁻⁴	2.085 ⁻⁴
0.106	0.966	3.308 ⁻³	1.865 ⁻³	-5.297 ⁻⁴	0.639	1.076	-2.620 ⁻³	3.169 ⁻⁴	5.634 ⁻⁶
0.116	0.985	2.201 ⁻³	1.979 ⁻³	-4.656 ⁻⁴	0.659	1.080	-1.019 ⁻³	2.773 ⁻⁴	5.396 ⁻⁵
0.126	1.008	-2.026 ⁻⁵	1.545 ⁻³	-3.909 ⁻⁴	0.679	1.065	-7.818 ⁻³	7.303 ⁻⁴	2.206 ⁻⁴
0.136	1.011	1.732 ⁻³	1.597 ⁻³	-4.212 ⁻⁴	0.692	1.074	-2.664 ⁻³	4.869 ⁻⁴	1.682 ⁻⁴
0.146	1.021	2.853 ⁻³	1.443 ⁻³	-3.294 ⁻⁴	0.719	1.063	-7.996 ⁻³	6.624 ⁻⁴	1.950 ⁻⁴
0.156	1.034	2.549 ⁻³	1.222 ⁻³	-2.949 ⁻⁴	0.732	1.059	-6.814 ⁻³	8.084 ⁻⁴	2.585 ⁻⁴
0.166	1.047	1.114 ⁻³	9.836 ⁻⁴	-2.625 ⁻⁴	0.746	1.065	-1.350 ⁻³	5.507 ⁻⁴	2.180 ⁻⁴
0.176	1.051	1.988 ⁻³	8.493 ⁻⁴	-1.603 ⁻⁴	0.759	1.058	-3.950 ⁻³	8.465 ⁻⁴	3.359 ⁻⁴
0.186	1.037	5.031 ⁻³	9.671 ⁻⁴	-2.368 ⁻⁴	0.786	1.058	-2.925 ⁻³	7.611 ⁻⁴	2.945 ⁻⁴
0.199	1.042	5.607 ⁻³	8.598 ⁻⁴	-2.030 ⁻⁴	0.799	1.043	-4.317 ⁻³	1.271 ⁻³	3.466 ⁻⁴
0.212	1.057	1.756 ⁻³	6.921 ⁻⁴	-1.652 ⁻⁴	0.812	1.037	-4.334 ⁻³	1.479 ⁻³	4.676 ⁻⁴
0.226	1.075	9.554 ⁻⁴	4.134 ⁻⁴	-9.606 ⁻⁵	0.832	1.034	-4.185 ⁻³	1.393 ⁻³	4.456 ⁻⁴
0.239	1.076	-1.007 ⁻³	3.975 ⁻⁴	-1.008 ⁻⁴	0.842	1.016	-5.223 ⁻³	1.889 ⁻³	5.334 ⁻⁴
0.252	1.069	3.810 ⁻³	4.845 ⁻⁴	-1.125 ⁻⁴	0.852	0.992	-7.138 ⁻³	2.160 ⁻³	5.590 ⁻⁴
0.266	1.075	4.061 ⁻³	3.231 ⁻⁴	-6.723 ⁻⁵	0.862	1.012	-3.700 ⁻³	1.932 ⁻³	5.663 ⁻⁴
0.279	1.075	5.394 ⁻³	3.588 ⁻⁴	-7.927 ⁻⁵	0.872	1.001	-3.107 ⁻³	1.945 ⁻³	5.358 ⁻⁴
0.292	1.074	-6.471 ⁻⁴	3.094 ⁻⁴	-5.367 ⁻⁵	0.882	0.950	-7.185 ⁻³	2.653 ⁻³	7.023 ⁻⁴
0.306	1.083	5.728 ⁻³	2.201 ⁻⁴	-2.008 ⁻⁵	0.892	0.984	-3.171 ⁻³	2.371 ⁻³	5.998 ⁻⁴
0.319	1.079	-2.200 ⁻⁴	2.783 ⁻⁴	-4.096 ⁻⁵	0.902	0.947	-6.945 ⁻³	2.655 ⁻³	7.593 ⁻⁴
0.339	1.083	6.059 ⁻³	2.149 ⁻⁴	-3.497 ⁻⁵	0.912	0.966	-4.024 ⁻³	2.850 ⁻³	8.166 ⁻⁴
0.346	1.071	-1.715 ⁻³	3.548 ⁻⁴	-9.324 ⁻⁵	0.919	0.929	-5.806 ⁻³	3.203 ⁻³	8.898 ⁻⁴
0.359	1.083	4.618 ⁻³	2.302 ⁻⁴	-3.917 ⁻⁵	0.926	0.912	-4.051 ⁻³	3.105 ⁻³	7.543 ⁻⁴
0.372	1.075	3.231 ⁻⁴	2.993 ⁻⁴	-6.148 ⁻⁵	0.932	0.914	-3.859 ⁻³	3.028 ⁻³	7.508 ⁻⁴
0.379	1.087	1.552 ⁻³	2.054 ⁻⁴	-2.838 ⁻⁵	0.939	0.907	-3.229 ⁻³	2.876 ⁻³	7.523 ⁻⁴
0.399	1.083	-1.723 ⁻³	2.071 ⁻⁴	-1.254 ⁻⁵	0.946	0.863	-5.904 ⁻³	3.884 ⁻³	1.028 ⁻³
0.419	1.087	4.231 ⁻³	1.769 ⁻⁴	-3.759 ⁻⁵	0.952	0.850	-5.858 ⁻³	3.209 ⁻³	9.253 ⁻⁴
0.426	1.079	-4.493 ⁻³	2.883 ⁻⁴	-6.833 ⁻⁵	0.959	0.851	-5.365 ⁻³	3.456 ⁻³	7.872 ⁻⁴
0.439	1.087	-4.315 ⁻³	2.625 ⁻⁴	1.796 ⁻⁵	0.966	0.824	-2.760 ⁻³	3.402 ⁻³	8.337 ⁻⁴
0.452	1.080	1.124 ⁻³	2.901 ⁻⁴	-2.380 ⁻⁵	0.979	0.792	-1.398 ⁻³	3.773 ⁻³	9.732 ⁻⁴

Table 2. Continued ($x/H = -4$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

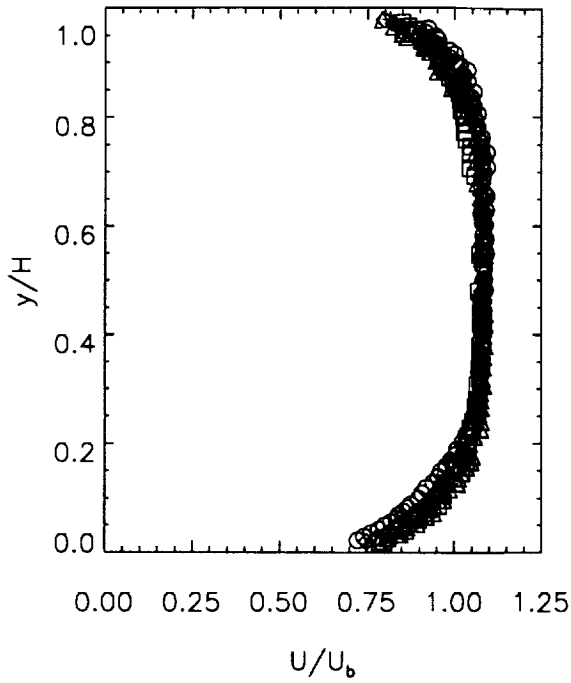
y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.019	0.798	3.375^{-3}	2.819^{-3}	-8.077^{-4}	0.419	1.075	1.034^{-2}	1.712^{-4}	1.055^{-5}
0.026	0.810	4.370^{-3}	2.636^{-3}	-7.615^{-4}	0.439	1.076	1.081^{-2}	2.378^{-4}	-1.266^{-5}
0.032	0.830	3.411^{-3}	2.543^{-3}	-7.957^{-4}	0.459	1.077	5.054^{-3}	2.258^{-4}	2.559^{-5}
0.039	0.843	3.776^{-3}	2.629^{-3}	-8.048^{-4}	0.479	1.070	1.229^{-3}	3.009^{-4}	1.060^{-4}
0.046	0.850	5.735^{-3}	2.632^{-3}	-8.868^{-4}	0.546	1.074	7.151^{-3}	2.812^{-4}	6.026^{-5}
0.052	0.871	3.673^{-3}	2.467^{-3}	-7.816^{-4}	0.692	1.059	-4.095^{-3}	5.699^{-4}	2.779^{-4}
0.059	0.877	4.090^{-3}	2.258^{-3}	-6.256^{-4}	0.706	1.047	-9.789^{-3}	9.019^{-4}	3.661^{-4}
0.066	0.899	3.729^{-3}	2.133^{-3}	-6.188^{-4}	0.732	1.046	-7.162^{-3}	9.438^{-4}	3.176^{-4}
0.072	0.918	3.119^{-3}	2.134^{-3}	-6.237^{-4}	0.746	1.049	-4.261^{-3}	7.681^{-4}	2.916^{-4}
0.079	0.926	3.150^{-3}	2.331^{-3}	-6.533^{-4}	0.759	1.033	-5.615^{-3}	1.290^{-3}	4.608^{-4}
0.086	0.955	2.528^{-3}	2.144^{-3}	-5.954^{-4}	0.772	1.028	-9.447^{-3}	1.576^{-3}	5.566^{-4}
0.096	0.950	2.442^{-3}	1.864^{-3}	-5.169^{-4}	0.786	1.033	-8.254^{-3}	1.281^{-3}	4.628^{-4}
0.106	0.967	4.093^{-3}	1.820^{-3}	-4.779^{-4}	0.799	1.027	-8.035^{-3}	1.358^{-3}	4.559^{-4}
0.116	0.961	3.451^{-3}	1.705^{-3}	-4.608^{-4}	0.812	1.020	-7.453^{-3}	1.538^{-3}	4.717^{-4}
0.126	0.973	4.618^{-3}	1.362^{-3}	-4.120^{-4}	0.822	1.023	-6.022^{-3}	1.658^{-3}	5.441^{-4}
0.136	0.977	5.400^{-3}	1.733^{-3}	-4.347^{-4}	0.832	1.017	-7.030^{-3}	1.701^{-3}	5.132^{-4}
0.146	1.020	3.349^{-3}	1.075^{-3}	-2.144^{-4}	0.842	1.013	-7.836^{-3}	1.710^{-3}	5.289^{-4}
0.156	1.006	5.204^{-3}	1.239^{-3}	-3.122^{-4}	0.862	0.997	-7.606^{-3}	1.932^{-3}	5.839^{-4}
0.166	1.033	2.769^{-3}	1.053^{-3}	-2.337^{-4}	0.872	0.986	-7.868^{-3}	2.199^{-3}	5.950^{-4}
0.176	1.035	2.518^{-3}	1.164^{-3}	-2.849^{-4}	0.882	0.971	-9.200^{-3}	2.369^{-3}	5.544^{-4}
0.186	1.037	6.482^{-3}	8.100^{-4}	-1.708^{-4}	0.892	0.963	-9.105^{-3}	2.170^{-3}	6.117^{-4}
0.199	1.038	6.576^{-3}	7.382^{-4}	-1.504^{-4}	0.902	0.952	-9.185^{-3}	2.617^{-3}	6.993^{-4}
0.212	1.041	8.491^{-3}	8.093^{-4}	-1.891^{-4}	0.912	0.957	-6.911^{-3}	2.522^{-3}	7.959^{-4}
0.226	1.046	8.723^{-3}	5.944^{-4}	-1.061^{-4}	0.919	0.948	-8.905^{-3}	2.643^{-3}	8.376^{-4}
0.239	1.053	2.287^{-3}	7.719^{-4}	2.954^{-5}	0.926	0.934	-7.590^{-3}	2.884^{-3}	7.399^{-4}
0.252	1.062	5.521^{-3}	3.841^{-4}	-8.101^{-5}	0.932	0.924	-8.612^{-3}	2.567^{-3}	7.225^{-4}
0.266	1.061	6.501^{-4}	3.866^{-4}	3.222^{-5}	0.939	0.918	-6.995^{-3}	2.579^{-3}	7.249^{-4}
0.279	1.065	7.703^{-3}	3.113^{-4}	-4.146^{-5}	0.946	0.903	-7.614^{-3}	2.563^{-3}	6.959^{-4}
0.306	1.066	1.106^{-2}	2.003^{-4}	-1.040^{-5}	0.952	0.892	-7.275^{-3}	2.633^{-3}	6.894^{-4}
0.339	1.072	9.419^{-3}	2.984^{-4}	-3.410^{-5}	0.959	0.885	-6.905^{-3}	2.797^{-3}	7.448^{-4}
0.359	1.074	1.053^{-2}	2.444^{-4}	-1.537^{-5}	0.966	0.866	-4.923^{-3}	2.837^{-3}	8.216^{-4}
0.379	1.075	8.929^{-3}	2.843^{-4}	-9.218^{-5}	0.972	0.849	-3.539^{-3}	3.032^{-3}	7.688^{-4}

Table 2. Concluded ($x/H = -4$)

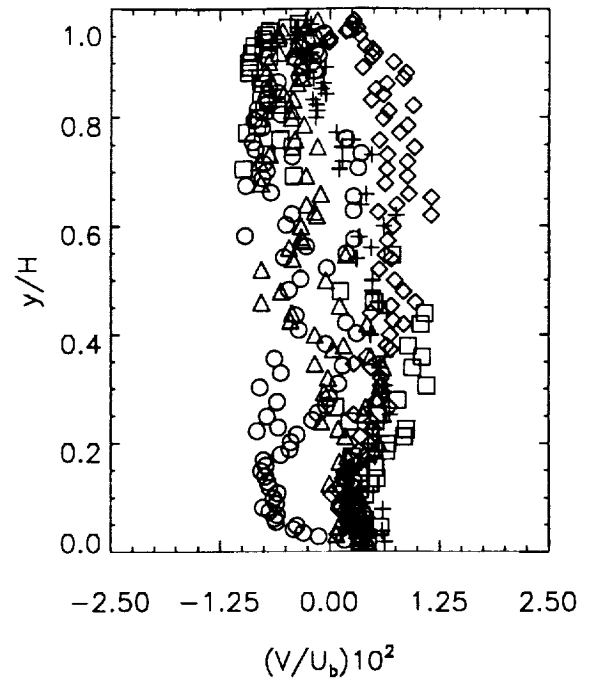
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.019	0.819	6.267 ⁻³	3.706 ⁻³	-7.080 ⁻⁴	0.479	1.080	4.871 ⁻³	1.701 ⁻⁴	5.482 ⁻⁵
0.026	0.833	4.304 ⁻³	3.226 ⁻³	-8.632 ⁻⁴	0.499	1.081	4.875 ⁻³	1.686 ⁻⁴	2.468 ⁻⁵
0.032	0.854	4.578 ⁻³	3.154 ⁻³	-8.893 ⁻⁴	0.539	1.079	3.052 ⁻³	1.776 ⁻⁴	3.546 ⁻⁵
0.039	0.865	5.971 ⁻³	3.050 ⁻³	-7.862 ⁻⁴	0.559	1.083	4.726 ⁻³	1.752 ⁻⁴	1.664 ⁻⁵
0.046	0.872	3.591 ⁻³	2.774 ⁻³	-7.862 ⁻⁴	0.579	1.081	3.358 ⁻³	1.960 ⁻⁴	2.427 ⁻⁵
0.052	0.888	3.140 ⁻³	2.875 ⁻³	-6.108 ⁻⁴	0.599	1.083	6.192 ⁻³	1.994 ⁻⁴	6.438 ⁻⁵
0.059	0.900	3.812 ⁻³	2.705 ⁻³	-7.169 ⁻⁴	0.619	1.081	7.575 ⁻³	2.015 ⁻⁴	3.000 ⁻⁵
0.066	0.911	4.112 ⁻³	2.452 ⁻³	-7.320 ⁻⁴	0.639	1.082	3.562 ⁻³	2.188 ⁻⁴	4.530 ⁻⁵
0.072	0.918	2.627 ⁻³	2.274 ⁻³	-7.035 ⁻⁴	0.659	1.080	4.165 ⁻³	2.076 ⁻⁴	3.898 ⁻⁵
0.079	0.934	6.011 ⁻³	2.862 ⁻³	-5.397 ⁻⁴	0.706	1.077	1.113 ⁻³	3.251 ⁻⁴	9.933 ⁻⁵
0.086	0.941	1.959 ⁻³	2.073 ⁻³	-5.679 ⁻⁴	0.719	1.073	1.492 ⁻³	4.341 ⁻⁴	1.411 ⁻⁴
0.096	0.957	2.852 ⁻³	2.025 ⁻³	-5.480 ⁻⁴	0.732	1.074	4.862 ⁻³	4.695 ⁻⁴	1.553 ⁻⁴
0.106	0.969	1.813 ⁻³	1.740 ⁻³	-5.014 ⁻⁴	0.746	1.068	1.444 ⁻³	6.538 ⁻⁴	2.453 ⁻⁴
0.116	0.982	3.562 ⁻³	1.808 ⁻³	-4.612 ⁻⁴	0.759	1.069	2.616 ⁻³	5.317 ⁻⁴	1.755 ⁻⁴
0.126	0.988	1.955 ⁻³	1.682 ⁻³	-5.452 ⁻⁴	0.772	1.061	7.520 ⁻⁴	8.526 ⁻⁴	2.661 ⁻⁴
0.136	0.999	1.697 ⁻³	1.527 ⁻³	-3.302 ⁻⁴	0.799	1.031	-1.598 ⁻³	1.369 ⁻³	4.045 ⁻⁴
0.146	1.012	2.261 ⁻³	1.476 ⁻³	-3.188 ⁻⁴	0.812	1.030	-1.482 ⁻³	1.443 ⁻³	4.497 ⁻⁴
0.156	1.015	3.186 ⁻³	1.261 ⁻³	-2.700 ⁻⁴	0.822	1.022	-1.561 ⁻³	1.568 ⁻³	4.589 ⁻⁴
0.166	1.028	4.477 ⁻³	1.056 ⁻³	-2.201 ⁻⁴	0.832	1.021	-1.975 ⁻³	1.683 ⁻³	5.026 ⁻⁴
0.176	1.024	5.125 ⁻³	1.179 ⁻³	-2.742 ⁻⁴	0.842	1.003	-4.521 ⁻⁴	2.004 ⁻³	5.992 ⁻⁴
0.186	1.035	6.016 ⁻³	1.132 ⁻³	-2.049 ⁻⁴	0.852	1.001	-9.852 ⁻⁴	1.826 ⁻³	5.689 ⁻⁴
0.199	1.041	4.405 ⁻³	8.774 ⁻⁴	-1.834 ⁻⁴	0.862	0.998	-7.321 ⁻⁴	2.064 ⁻³	6.062 ⁻⁴
0.212	1.054	5.603 ⁻³	6.855 ⁻⁴	-9.045 ⁻⁵	0.872	0.973	-1.869 ⁻³	2.133 ⁻³	6.562 ⁻⁴
0.226	1.063	4.953 ⁻³	4.968 ⁻⁴	-7.006 ⁻⁵	0.882	0.963	-2.370 ⁻³	2.308 ⁻³	6.268 ⁻⁴
0.239	1.061	6.182 ⁻³	6.367 ⁻⁴	-5.565 ⁻⁵	0.892	0.959	-5.260 ⁻⁴	2.400 ⁻³	8.063 ⁻⁴
0.252	1.065	6.830 ⁻³	4.944 ⁻⁴	-6.001 ⁻⁵	0.902	0.938	-2.346 ⁻³	2.627 ⁻³	7.986 ⁻⁴
0.266	1.065	4.398 ⁻³	4.791 ⁻⁴	-7.190 ⁻⁵	0.912	0.933	-2.711 ⁻³	2.789 ⁻³	8.884 ⁻⁴
0.292	1.074	5.960 ⁻³	2.500 ⁻⁴	1.619 ⁻⁵	0.919	0.914	-2.145 ⁻³	2.866 ⁻³	8.373 ⁻⁴
0.306	1.076	6.257 ⁻³	2.829 ⁻⁴	9.819 ⁻⁵	0.926	0.902	-3.100 ⁻³	2.859 ⁻³	8.552 ⁻⁴
0.339	1.076	5.683 ⁻³	1.994 ⁻⁴	2.171 ⁻⁵	0.952	0.856	-3.550 ⁻³	3.254 ⁻³	9.850 ⁻⁴
0.359	1.077	6.300 ⁻³	1.415 ⁻⁴	2.079 ⁻⁵	0.959	0.839	-2.145 ⁻³	3.694 ⁻³	1.152 ⁻³
0.399	1.076	4.593 ⁻³	2.222 ⁻⁴	3.953 ⁻⁵	0.966	0.831	-3.669 ⁻³	3.663 ⁻³	1.202 ⁻³
0.439	1.081	6.455 ⁻³	1.501 ⁻⁴	1.795 ⁻⁵	0.972	0.824	-2.159 ⁻³	3.646 ⁻³	1.008 ⁻³
0.459	1.081	5.548 ⁻³	1.876 ⁻⁴	7.743 ⁻⁵	0.979	0.814	-2.711 ⁻³	3.999 ⁻³	1.286 ⁻³

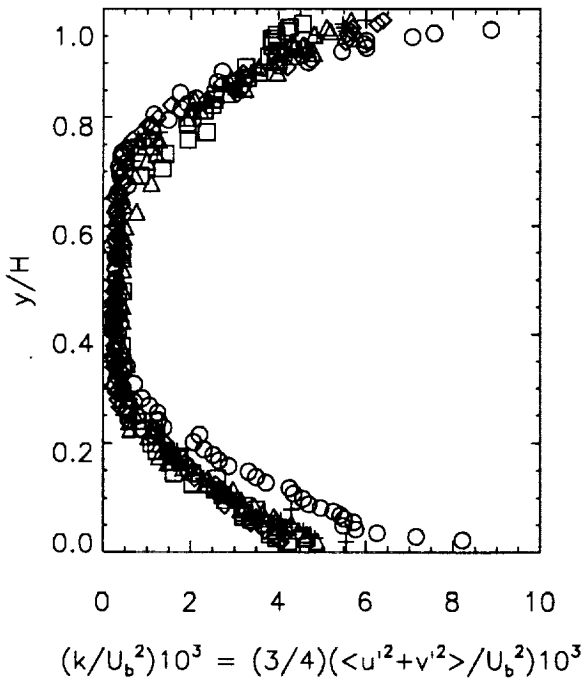
Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)



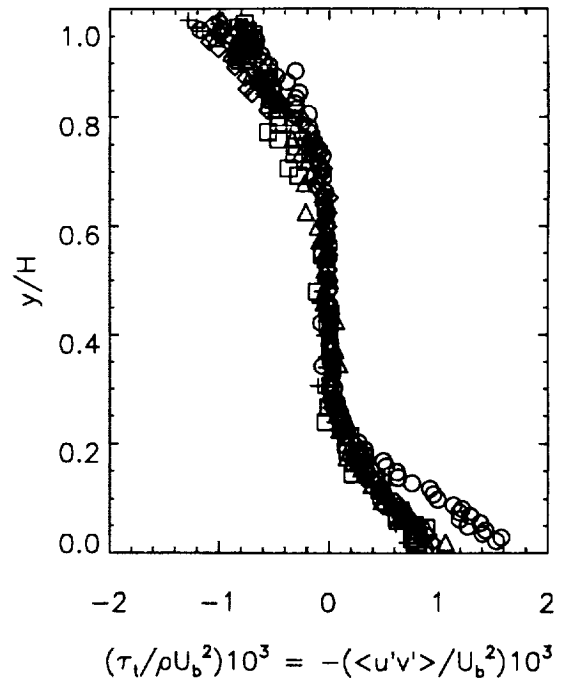
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

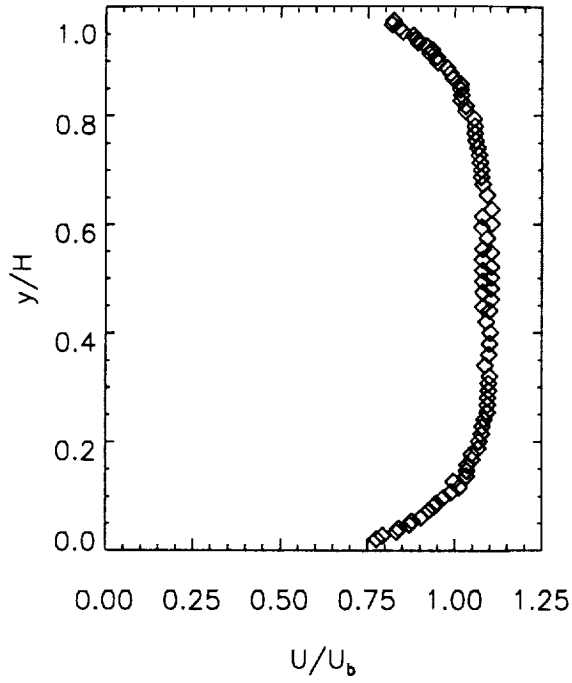
Figure 2. Summary of Table 2 ($x/H = -4$).

Table 3. LDV flowfield data in TAD ($x/H = -3$)

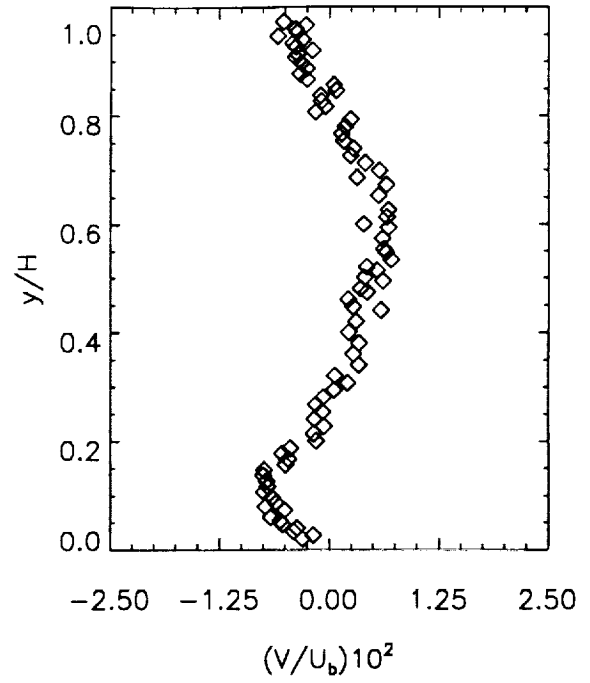
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.776	-3.043 ⁻³	2.793 ⁻³	-8.521 ⁻⁴	0.514	1.080	5.446 ⁻³	1.949 ⁻⁴	-5.168 ⁻⁶
0.027	0.792	-1.816 ⁻³	3.265 ⁻³	-1.047 ⁻³	0.520	1.104	4.298 ⁻³	2.491 ⁻⁴	-2.985 ⁻⁵
0.034	0.833	-4.029 ⁻³	2.923 ⁻³	-7.837 ⁻⁴	0.534	1.079	7.070 ⁻³	1.603 ⁻⁴	-2.408 ⁻⁷
0.040	0.839	-3.653 ⁻³	3.086 ⁻³	-8.811 ⁻⁴	0.547	1.104	6.493 ⁻³	1.751 ⁻⁴	-1.062 ⁻⁵
0.047	0.870	-5.297 ⁻³	3.516 ⁻³	-7.548 ⁻⁴	0.554	1.080	6.228 ⁻³	2.399 ⁻⁴	2.528 ⁻⁵
0.054	0.877	-5.559 ⁻³	2.736 ⁻³	-8.251 ⁻⁴	0.574	1.092	6.095 ⁻³	2.084 ⁻⁴	-3.880 ⁻⁶
0.060	0.904	-6.648 ⁻³	2.713 ⁻³	-7.034 ⁻⁴	0.594	1.077	6.780 ⁻³	2.592 ⁻⁴	4.835 ⁻⁵
0.074	0.926	-5.093 ⁻³	2.808 ⁻³	-6.291 ⁻⁴	0.600	1.106	3.959 ⁻³	2.094 ⁻⁴	1.009 ⁻⁵
0.080	0.939	-7.269 ⁻³	2.500 ⁻³	-6.086 ⁻⁴	0.614	1.079	6.593 ⁻³	1.945 ⁻⁴	2.241 ⁻⁵
0.087	0.947	-6.023 ⁻³	2.573 ⁻³	-6.976 ⁻⁴	0.627	1.105	6.771 ⁻³	2.114 ⁻⁴	1.003 ⁻⁵
0.097	0.967	-6.506 ⁻³	2.276 ⁻³	-5.283 ⁻⁴	0.654	1.092	5.680 ⁻³	2.209 ⁻⁴	2.701 ⁻⁶
0.107	0.989	-7.445 ⁻³	2.224 ⁻³	-4.693 ⁻⁴	0.674	1.080	6.565 ⁻³	3.161 ⁻⁴	7.712 ⁻⁵
0.117	1.013	-7.006 ⁻³	2.174 ⁻³	-4.785 ⁻⁴	0.687	1.075	3.210 ⁻³	3.794 ⁻⁴	1.306 ⁻⁴
0.127	0.996	-7.155 ⁻³	1.954 ⁻³	-5.228 ⁻⁴	0.700	1.075	5.778 ⁻³	3.612 ⁻⁴	1.049 ⁻⁴
0.137	1.033	-7.505 ⁻³	1.802 ⁻³	-3.757 ⁻⁴	0.714	1.072	4.157 ⁻³	5.653 ⁻⁴	1.973 ⁻⁴
0.147	1.034	-7.426 ⁻³	1.663 ⁻³	-3.717 ⁻⁴	0.727	1.069	2.479 ⁻³	6.139 ⁻⁴	2.102 ⁻⁴
0.157	1.036	-4.967 ⁻³	1.442 ⁻³	-3.325 ⁻⁴	0.740	1.065	2.790 ⁻³	6.769 ⁻⁴	2.114 ⁻⁴
0.167	1.049	-4.650 ⁻³	1.234 ⁻³	-2.470 ⁻⁴	0.754	1.060	1.680 ⁻³	7.703 ⁻⁴	2.487 ⁻⁴
0.177	1.048	-5.374 ⁻³	1.425 ⁻³	-2.808 ⁻⁴	0.767	1.057	1.436 ⁻³	1.076 ⁻³	3.614 ⁻⁴
0.187	1.066	-4.450 ⁻³	9.081 ⁻⁴	-1.705 ⁻⁴	0.780	1.057	1.861 ⁻³	1.057 ⁻³	3.251 ⁻⁴
0.200	1.069	-1.506 ⁻³	6.904 ⁻⁴	-1.393 ⁻⁴	0.794	1.054	2.463 ⁻³	1.047 ⁻³	3.603 ⁻⁴
0.214	1.076	-1.764 ⁻³	7.874 ⁻⁴	-1.717 ⁻⁴	0.807	1.031	-1.534 ⁻³	1.668 ⁻³	4.675 ⁻⁴
0.227	1.079	-5.980 ⁻⁴	6.774 ⁻⁴	-1.154 ⁻⁴	0.817	1.031	-4.332 ⁻⁴	1.725 ⁻³	5.448 ⁻⁴
0.240	1.084	-1.683 ⁻³	4.378 ⁻⁴	-8.197 ⁻⁵	0.827	1.016	-8.689 ⁻⁴	2.015 ⁻³	5.689 ⁻⁴
0.254	1.092	-7.671 ⁻⁴	3.689 ⁻⁴	-4.300 ⁻⁵	0.837	1.018	-9.634 ⁻⁴	2.057 ⁻³	6.128 ⁻⁴
0.267	1.094	-1.528 ⁻³	3.418 ⁻⁴	-6.079 ⁻⁵	0.847	1.016	8.134 ⁻⁴	1.995 ⁻³	5.426 ⁻⁴
0.280	1.094	-7.063 ⁻⁴	3.484 ⁻⁴	-6.232 ⁻⁵	0.857	1.016	5.632 ⁻⁴	2.013 ⁻³	5.988 ⁻⁴
0.294	1.097	5.416 ⁻⁴	2.413 ⁻⁴	-3.772 ⁻⁵	0.867	0.994	-2.540 ⁻³	2.287 ⁻³	6.364 ⁻⁴
0.307	1.096	2.078 ⁻³	2.148 ⁻⁴	-1.113 ⁻⁵	0.877	0.986	-3.312 ⁻³	2.466 ⁻³	7.348 ⁻⁴
0.320	1.100	6.347 ⁻⁴	1.898 ⁻⁴	-1.043 ⁻⁵	0.887	0.977	-2.576 ⁻³	2.578 ⁻³	7.388 ⁻⁴
0.340	1.086	3.353 ⁻³	2.903 ⁻⁴	-5.958 ⁻⁵	0.897	0.951	-3.198 ⁻³	3.049 ⁻³	9.113 ⁻⁴
0.360	1.097	2.729 ⁻³	2.473 ⁻⁴	-4.744 ⁻⁵	0.907	0.947	-3.854 ⁻³	2.954 ⁻³	8.065 ⁻⁴
0.380	1.099	3.387 ⁻³	2.040 ⁻⁴	-1.977 ⁻⁵	0.914	0.927	-3.617 ⁻³	3.075 ⁻³	8.073 ⁻⁴
0.400	1.101	2.224 ⁻³	1.877 ⁻⁴	-1.901 ⁻⁵	0.920	0.934	-1.918 ⁻³	3.091 ⁻³	8.969 ⁻⁴
0.420	1.090	3.066 ⁻³	1.829 ⁻⁴	-1.889 ⁻⁵	0.927	0.917	-3.821 ⁻³	3.236 ⁻³	8.916 ⁻⁴
0.440	1.100	5.889 ⁻³	2.002 ⁻⁴	-1.570 ⁻⁵	0.934	0.893	-4.152 ⁻³	3.532 ⁻³	1.113 ⁻³
0.447	1.080	2.730 ⁻³	1.959 ⁻⁴	-1.873 ⁻⁵	0.940	0.888	-3.049 ⁻³	3.283 ⁻³	1.008 ⁻³
0.460	1.104	2.179 ⁻³	2.231 ⁻⁴	-1.522 ⁻⁵	0.947	0.880	-5.848 ⁻³	3.285 ⁻³	9.375 ⁻⁴
0.474	1.080	4.311 ⁻³	1.937 ⁻⁴	-3.551 ⁻⁶	0.954	0.849	-3.685 ⁻³	3.570 ⁻³	1.060 ⁻³
0.480	1.104	3.580 ⁻³	1.914 ⁻⁴	-1.544 ⁻⁵	0.960	0.838	-3.843 ⁻³	3.635 ⁻³	1.051 ⁻³
0.494	1.080	6.126 ⁻³	2.019 ⁻⁴	-3.331 ⁻⁶	0.967	0.819	-2.668 ⁻³	3.485 ⁻³	1.004 ⁻³
0.500	1.104	4.055 ⁻³	1.979 ⁻⁴	-4.451 ⁻⁶	0.974	0.823	-5.195 ⁻³	3.287 ⁻³	1.019 ⁻³

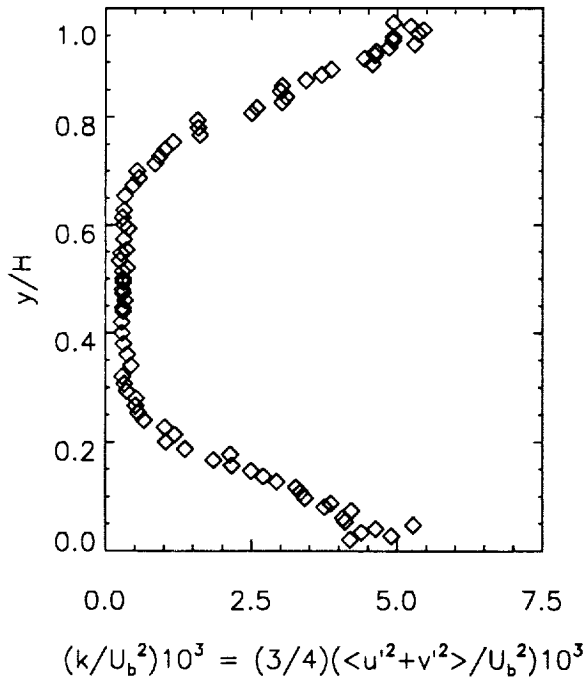
Legend: $Re = 1 \times 10^5$; $z/H = 0(\diamond)$



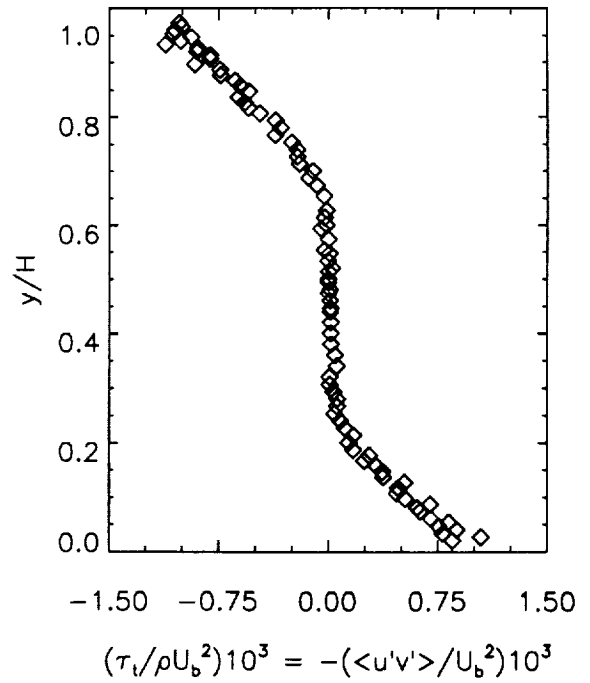
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 3. Summary of Table 3 ($x/H = -3$).

Table 4. LDV flowfield data in TAD ($x/H = -2$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.024	0.734	2.673^{-3}	5.473^{-3}	-1.022^{-3}	0.491	1.097	1.076^{-3}	1.408^{-4}	-5.207^{-7}
0.031	0.746	-1.540^{-4}	4.553^{-3}	-1.197^{-3}	0.511	1.099	-2.881^{-3}	1.884^{-4}	6.670^{-6}
0.037	0.766	-2.934^{-3}	3.801^{-3}	-1.297^{-3}	0.524	1.096	-9.442^{-4}	2.769^{-4}	7.251^{-5}
0.044	0.787	-4.865^{-3}	3.978^{-3}	-1.213^{-3}	0.531	1.098	-3.582^{-3}	2.126^{-4}	2.027^{-5}
0.051	0.805	-5.607^{-3}	3.391^{-3}	-1.152^{-3}	0.551	1.098	2.431^{-3}	2.810^{-4}	9.324^{-5}
0.057	0.816	-6.237^{-3}	3.465^{-3}	-1.255^{-3}	0.571	1.099	-5.852^{-3}	2.287^{-4}	4.334^{-5}
0.064	0.828	-6.462^{-3}	3.333^{-3}	-1.076^{-3}	0.577	1.096	4.194^{-3}	3.579^{-4}	1.366^{-4}
0.071	0.841	-8.339^{-3}	3.000^{-3}	-1.134^{-3}	0.591	1.100	1.892^{-3}	1.763^{-4}	-1.183^{-6}
0.077	0.846	-8.515^{-3}	2.895^{-3}	-1.124^{-3}	0.611	1.100	2.376^{-3}	1.520^{-4}	9.216^{-6}
0.084	0.857	-8.681^{-3}	2.811^{-3}	-1.078^{-3}	0.631	1.099	1.005^{-3}	3.781^{-4}	1.753^{-4}
0.091	0.868	-8.518^{-3}	2.711^{-3}	-1.069^{-3}	0.651	1.096	-4.590^{-3}	2.998^{-4}	6.389^{-5}
0.101	0.881	-8.853^{-3}	2.632^{-3}	-1.019^{-3}	0.657	1.096	3.610^{-3}	4.056^{-4}	1.880^{-4}
0.111	0.896	-8.328^{-3}	2.498^{-3}	-8.771^{-4}	0.671	1.097	2.742^{-5}	2.561^{-4}	6.039^{-5}
0.121	0.915	-9.476^{-3}	2.305^{-3}	-7.287^{-4}	0.684	1.098	3.007^{-3}	4.771^{-4}	2.627^{-4}
0.131	0.930	-1.077^{-2}	2.276^{-3}	-8.078^{-4}	0.697	1.090	-5.871^{-3}	4.284^{-4}	1.347^{-4}
0.141	0.940	-8.465^{-3}	2.244^{-3}	-6.407^{-4}	0.711	1.090	-1.777^{-3}	5.856^{-4}	2.477^{-4}
0.151	0.951	-7.236^{-3}	2.125^{-3}	-6.297^{-4}	0.724	1.086	-4.039^{-3}	5.780^{-4}	1.708^{-4}
0.161	0.977	-8.642^{-3}	2.058^{-3}	-5.614^{-4}	0.737	1.083	-3.681^{-3}	7.580^{-4}	3.032^{-4}
0.171	0.983	-8.267^{-3}	1.863^{-3}	-3.612^{-4}	0.751	1.073	-7.188^{-3}	1.055^{-3}	3.162^{-4}
0.181	0.989	-7.790^{-3}	1.681^{-3}	-3.821^{-4}	0.764	1.082	-1.771^{-3}	8.243^{-4}	2.742^{-4}
0.191	1.010	-7.540^{-3}	1.657^{-3}	-3.836^{-4}	0.777	1.073	-3.571^{-3}	9.731^{-4}	2.859^{-4}
0.204	1.014	-5.182^{-3}	1.486^{-3}	-2.965^{-4}	0.804	1.066	-2.205^{-3}	1.238^{-3}	3.374^{-4}
0.217	1.019	-3.595^{-3}	1.423^{-3}	-3.070^{-4}	0.814	1.070	4.026^{-4}	1.112^{-3}	2.897^{-4}
0.231	1.034	-2.993^{-3}	1.265^{-3}	-2.512^{-4}	0.824	1.075	9.827^{-4}	1.034^{-3}	2.353^{-4}
0.244	1.040	-2.767^{-4}	1.390^{-3}	-1.232^{-4}	0.834	1.070	3.851^{-4}	1.159^{-3}	2.999^{-4}
0.257	1.045	-7.760^{-4}	1.104^{-3}	-1.812^{-4}	0.844	1.053	-1.211^{-3}	1.781^{-3}	3.943^{-4}
0.271	1.058	-1.330^{-4}	9.099^{-4}	-1.564^{-4}	0.854	1.045	-1.486^{-3}	1.836^{-3}	4.041^{-4}
0.284	1.067	-7.971^{-4}	7.670^{-4}	-1.150^{-4}	0.864	1.047	3.025^{-4}	1.927^{-3}	3.962^{-4}
0.297	1.067	1.586^{-3}	7.321^{-4}	-9.472^{-5}	0.874	1.042	4.822^{-5}	1.931^{-3}	3.862^{-4}
0.311	1.081	-9.662^{-4}	5.375^{-4}	-6.875^{-5}	0.884	1.024	-7.226^{-4}	2.483^{-3}	5.668^{-4}
0.324	1.081	2.138^{-3}	5.357^{-4}	-4.953^{-5}	0.894	1.028	-4.932^{-4}	2.241^{-3}	4.726^{-4}
0.337	1.092	-3.890^{-3}	2.975^{-4}	-4.325^{-5}	0.904	1.003	-8.155^{-4}	2.812^{-3}	6.007^{-4}
0.344	1.082	1.130^{-3}	4.905^{-4}	-5.754^{-5}	0.911	0.976	-3.366^{-3}	3.469^{-3}	6.281^{-4}
0.364	1.092	-1.459^{-3}	2.982^{-4}	-2.083^{-5}	0.917	0.944	-4.119^{-3}	3.823^{-3}	6.899^{-4}
0.391	1.096	-4.970^{-3}	2.140^{-4}	-1.808^{-5}	0.937	0.992	-1.346^{-3}	3.602^{-3}	6.648^{-4}
0.417	1.098	-2.796^{-3}	1.688^{-4}	-1.170^{-5}	0.944	0.976	-3.116^{-4}	3.726^{-3}	8.438^{-4}
0.444	1.096	-4.560^{-4}	2.201^{-4}	1.134^{-5}	0.957	0.979	6.061^{-4}	4.277^{-3}	6.002^{-4}
0.471	1.100	-5.081^{-3}	1.894^{-4}	8.336^{-7}	0.964	0.942	1.779^{-3}	5.127^{-3}	6.503^{-4}
0.484	1.095	3.239^{-3}	2.340^{-4}	2.994^{-5}					

Table 4. Continued ($x/H = -2$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.021	0.788	1.035^{-2}	3.753^{-3}	-4.867^{-4}	0.541	1.081	9.872^{-3}	2.676^{-4}	-2.152^{-5}
0.028	0.807	8.195^{-3}	3.445^{-3}	-6.387^{-4}	0.561	1.083	5.786^{-3}	2.522^{-4}	4.326^{-7}
0.035	0.831	8.178^{-3}	3.363^{-3}	-7.726^{-4}	0.581	1.081	4.450^{-3}	2.728^{-4}	1.425^{-5}
0.041	0.856	9.617^{-3}	3.419^{-3}	-6.812^{-4}	0.621	1.082	8.108^{-3}	2.648^{-4}	4.824^{-5}
0.048	0.857	5.028^{-3}	2.916^{-3}	-6.653^{-4}	0.628	1.082	1.171^{-2}	4.583^{-4}	2.358^{-4}
0.055	0.873	8.364^{-3}	2.928^{-3}	-6.948^{-4}	0.641	1.081	7.517^{-3}	2.762^{-4}	2.767^{-5}
0.061	0.892	7.922^{-3}	2.865^{-3}	-6.385^{-4}	0.661	1.078	5.876^{-3}	3.628^{-4}	1.021^{-4}
0.068	0.892	8.063^{-3}	2.799^{-3}	-5.655^{-4}	0.681	1.082	1.082^{-2}	4.904^{-4}	2.503^{-4}
0.081	0.908	7.820^{-3}	3.029^{-3}	-6.102^{-4}	0.695	1.073	5.243^{-3}	4.396^{-4}	1.528^{-4}
0.088	0.922	5.577^{-3}	2.360^{-3}	-6.521^{-4}	0.721	1.069	4.073^{-3}	4.586^{-4}	1.309^{-4}
0.098	0.931	7.889^{-3}	2.207^{-3}	-3.664^{-4}	0.735	1.074	8.923^{-3}	7.468^{-4}	3.744^{-4}
0.108	0.945	8.595^{-3}	2.725^{-3}	-4.206^{-4}	0.748	1.061	3.152^{-3}	7.563^{-4}	2.580^{-4}
0.118	0.963	6.193^{-3}	1.992^{-3}	-4.253^{-4}	0.775	1.058	7.184^{-3}	9.624^{-4}	3.042^{-4}
0.128	0.957	8.403^{-3}	1.737^{-3}	-4.500^{-4}	0.788	1.061	8.867^{-3}	7.937^{-4}	2.740^{-4}
0.138	0.974	7.409^{-3}	1.729^{-3}	-3.577^{-4}	0.801	1.053	7.169^{-3}	1.129^{-3}	3.402^{-4}
0.148	0.977	9.511^{-3}	1.844^{-3}	-3.434^{-4}	0.815	1.054	7.660^{-3}	9.447^{-4}	2.465^{-4}
0.158	0.982	1.048^{-2}	1.802^{-3}	-2.997^{-4}	0.825	1.032	3.267^{-3}	1.567^{-3}	4.476^{-4}
0.168	1.005	8.479^{-3}	1.668^{-3}	-2.038^{-4}	0.835	1.022	3.705^{-3}	1.694^{-3}	5.012^{-4}
0.178	1.010	1.034^{-2}	1.564^{-3}	-2.711^{-4}	0.845	1.025	5.387^{-3}	1.553^{-3}	4.227^{-4}
0.241	1.045	7.853^{-3}	7.936^{-4}	-1.992^{-4}	0.855	1.002	3.504^{-3}	2.301^{-3}	6.034^{-4}
0.255	1.045	1.145^{-2}	8.026^{-4}	-1.705^{-4}	0.865	0.996	2.956^{-3}	2.141^{-3}	6.537^{-4}
0.268	1.058	9.641^{-3}	7.078^{-4}	-1.517^{-4}	0.875	0.990	1.443^{-3}	2.466^{-3}	6.941^{-4}
0.281	1.056	1.195^{-2}	6.375^{-4}	-1.389^{-4}	0.885	0.977	1.252^{-3}	2.656^{-3}	7.387^{-4}
0.295	1.064	1.092^{-2}	5.126^{-4}	-1.234^{-4}	0.895	0.974	1.894^{-3}	2.499^{-3}	7.422^{-4}
0.308	1.069	1.066^{-2}	3.877^{-4}	-2.522^{-5}	0.905	0.975	1.939^{-3}	2.408^{-3}	7.160^{-4}
0.321	1.069	8.607^{-3}	4.140^{-4}	-8.142^{-5}	0.915	0.943	2.233^{-3}	2.914^{-3}	8.740^{-4}
0.341	1.067	1.321^{-2}	4.778^{-4}	-7.420^{-5}	0.921	0.930	1.486^{-3}	2.687^{-3}	8.062^{-4}
0.348	1.077	3.444^{-3}	4.177^{-4}	-1.153^{-4}	0.928	0.927	2.971^{-3}	2.695^{-3}	7.661^{-4}
0.361	1.072	1.252^{-2}	3.340^{-4}	-2.413^{-5}	0.935	0.910	-1.327^{-3}	2.929^{-3}	8.303^{-4}
0.375	1.082	4.983^{-3}	1.885^{-4}	-3.853^{-5}	0.941	0.911	3.077^{-3}	2.711^{-3}	8.285^{-4}
0.381	1.077	1.158^{-2}	2.377^{-4}	-3.273^{-5}	0.948	0.893	2.208^{-3}	2.666^{-3}	8.744^{-4}
0.421	1.078	1.196^{-2}	2.510^{-4}	-1.114^{-5}	0.955	0.881	9.039^{-4}	2.939^{-3}	8.279^{-4}
0.428	1.081	7.544^{-3}	1.953^{-4}	-2.021^{-5}	0.961	0.862	-1.025^{-3}	2.927^{-3}	8.481^{-4}
0.441	1.082	1.241^{-2}	2.276^{-4}	3.472^{-5}	0.968	0.836	-5.643^{-4}	2.906^{-3}	8.932^{-4}
0.455	1.080	6.613^{-3}	2.299^{-4}	-3.704^{-5}	0.975	0.820	-9.491^{-4}	2.925^{-3}	8.893^{-4}
0.501	1.085	8.255^{-3}	3.604^{-4}	1.340^{-4}	0.981	0.797	9.541^{-4}	3.107^{-3}	8.613^{-4}

Table 4. Continued ($x/H = -2$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.021	0.798	4.382^{-3}	2.901^{-3}	-6.466^{-4}	0.715	1.038	-4.198^{-3}	1.540^{-3}	4.636^{-4}
0.028	0.819	6.578^{-3}	2.966^{-3}	-6.611^{-4}	0.728	1.042	-1.698^{-3}	1.427^{-3}	4.288^{-4}
0.035	0.851	5.056^{-3}	2.766^{-3}	-8.195^{-4}	0.741	1.053	2.801^{-3}	1.307^{-3}	4.743^{-4}
0.041	0.844	5.631^{-3}	2.546^{-3}	-6.489^{-4}	0.755	1.041	2.852^{-4}	1.746^{-3}	5.821^{-4}
0.048	0.855	6.875^{-3}	2.597^{-3}	-6.069^{-4}	0.768	1.028	-2.104^{-4}	1.781^{-3}	5.641^{-4}
0.055	0.855	6.519^{-3}	2.474^{-3}	-5.708^{-4}	0.781	1.021	-5.245^{-4}	2.009^{-3}	6.011^{-4}
0.061	0.904	5.574^{-3}	2.478^{-3}	-6.078^{-4}	0.795	1.023	1.736^{-3}	2.135^{-3}	6.238^{-4}
0.068	0.897	4.300^{-3}	2.142^{-3}	-4.656^{-4}	0.808	0.999	-5.661^{-4}	2.085^{-3}	6.219^{-4}
0.081	0.902	3.831^{-3}	1.772^{-3}	-4.055^{-4}	0.828	0.972	-2.806^{-3}	2.736^{-3}	7.390^{-4}
0.088	0.916	2.640^{-3}	1.799^{-3}	-3.009^{-4}	0.838	0.994	9.291^{-4}	2.484^{-3}	7.051^{-4}
0.098	0.912	4.829^{-3}	1.891^{-3}	-4.048^{-4}	0.848	0.979	-3.668^{-4}	2.873^{-3}	7.273^{-4}
0.108	0.946	5.062^{-3}	1.848^{-3}	-3.745^{-4}	0.858	0.980	4.147^{-4}	2.795^{-3}	7.519^{-4}
0.118	0.949	4.759^{-3}	1.606^{-3}	-2.923^{-4}	0.868	0.971	1.139^{-4}	2.976^{-3}	7.800^{-4}
0.138	0.992	1.045^{-3}	9.769^{-4}	-2.288^{-4}	0.878	0.929	-3.568^{-3}	2.927^{-3}	7.618^{-4}
0.288	1.073	2.296^{-3}	4.054^{-4}	-1.143^{-4}	0.888	0.941	-1.386^{-3}	2.732^{-3}	7.513^{-4}
0.315	1.075	5.030^{-3}	3.766^{-4}	-8.202^{-5}	0.898	0.932	-1.036^{-3}	2.885^{-3}	8.153^{-4}
0.368	1.080	9.072^{-4}	2.835^{-4}	-1.912^{-5}	0.908	0.927	-1.031^{-3}	3.052^{-3}	8.115^{-4}
0.395	1.082	-5.058^{-3}	2.840^{-4}	2.637^{-5}	0.915	0.895	-2.077^{-3}	2.885^{-3}	7.556^{-4}
0.448	1.081	-2.165^{-3}	3.259^{-4}	5.459^{-5}	0.921	0.898	-1.102^{-3}	2.809^{-3}	7.733^{-4}
0.475	1.082	-6.453^{-5}	3.335^{-4}	6.050^{-5}	0.928	0.890	-2.718^{-3}	2.906^{-3}	8.214^{-4}
0.495	1.081	1.549^{-3}	3.718^{-4}	4.862^{-5}	0.935	0.881	-7.962^{-4}	3.346^{-3}	8.391^{-4}
0.535	1.084	6.730^{-3}	2.581^{-4}	3.021^{-5}	0.941	0.860	-1.337^{-3}	3.142^{-3}	7.953^{-4}
0.555	1.075	-7.703^{-4}	5.546^{-4}	1.687^{-4}	0.948	0.875	-1.818^{-3}	3.054^{-3}	8.018^{-4}
0.595	1.077	-2.968^{-3}	4.906^{-4}	1.725^{-4}	0.955	0.857	-1.244^{-3}	3.154^{-3}	8.986^{-4}
0.615	1.072	-1.769^{-3}	6.253^{-4}	2.186^{-4}	0.961	0.847	3.200^{-4}	2.940^{-3}	8.466^{-4}
0.675	1.072	2.726^{-3}	6.669^{-4}	2.453^{-4}	0.968	0.820	-2.094^{-3}	3.023^{-3}	8.153^{-4}
0.688	1.056	-2.109^{-3}	1.212^{-3}	4.610^{-4}	0.975	0.796	-6.592^{-4}	3.547^{-3}	1.098^{-3}
0.701	1.050	-8.929^{-4}	1.367^{-3}	4.455^{-4}					

Table 4. Continued ($x/H = -2$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.021	0.775	4.984^{-3}	3.982^{-3}	-1.067^{-3}	0.461	1.072	1.161^{-2}	2.171^{-4}	7.237^{-8}
0.028	0.790	5.434^{-3}	3.670^{-3}	-9.832^{-4}	0.475	1.073	1.146^{-2}	2.166^{-4}	2.845^{-5}
0.035	0.810	3.601^{-3}	3.569^{-3}	-1.076^{-3}	0.481	1.074	6.174^{-3}	1.944^{-4}	8.271^{-8}
0.041	0.825	5.466^{-3}	3.369^{-3}	-9.884^{-4}	0.495	1.076	8.584^{-3}	1.862^{-4}	1.122^{-5}
0.048	0.838	5.531^{-3}	3.164^{-3}	-9.543^{-4}	0.501	1.073	8.135^{-3}	2.068^{-4}	1.447^{-5}
0.055	0.847	4.823^{-3}	2.911^{-3}	-8.313^{-4}	0.515	1.075	9.244^{-3}	1.615^{-4}	1.075^{-5}
0.061	0.854	5.659^{-3}	2.890^{-3}	-9.067^{-4}	0.521	1.074	1.193^{-2}	1.902^{-4}	2.171^{-5}
0.068	0.881	5.466^{-3}	3.030^{-3}	-8.106^{-4}	0.535	1.074	9.225^{-3}	2.215^{-4}	2.784^{-5}
0.075	0.878	5.273^{-3}	2.653^{-3}	-7.961^{-4}	0.548	1.071	7.492^{-3}	2.512^{-4}	3.825^{-5}
0.081	0.885	4.791^{-3}	2.611^{-3}	-7.858^{-4}	0.555	1.068	2.432^{-3}	4.670^{-4}	1.583^{-4}
0.088	0.905	4.244^{-3}	2.556^{-3}	-7.279^{-4}	0.575	1.069	3.563^{-3}	3.414^{-4}	1.079^{-4}
0.098	0.912	4.051^{-3}	2.493^{-3}	-6.658^{-4}	0.595	1.068	2.071^{-3}	3.944^{-4}	1.051^{-4}
0.108	0.937	2.508^{-3}	2.142^{-3}	-5.294^{-4}	0.601	1.067	6.174^{-3}	4.539^{-4}	1.582^{-4}
0.118	0.927	5.498^{-3}	2.397^{-3}	-6.234^{-4}	0.615	1.070	5.419^{-3}	3.544^{-4}	1.065^{-4}
0.128	0.957	3.762^{-3}	1.778^{-3}	-4.146^{-4}	0.635	1.072	6.370^{-3}	4.226^{-4}	1.503^{-4}
0.138	0.966	3.537^{-3}	1.621^{-3}	-3.670^{-4}	0.675	1.058	5.685^{-3}	6.892^{-4}	2.524^{-4}
0.148	0.972	4.855^{-3}	1.705^{-3}	-4.425^{-4}	0.701	1.059	9.148^{-3}	7.289^{-4}	2.606^{-4}
0.158	0.981	5.145^{-3}	1.547^{-3}	-4.053^{-4}	0.741	1.050	5.589^{-3}	9.507^{-4}	3.270^{-4}
0.168	0.993	7.460^{-3}	1.874^{-3}	-3.691^{-4}	0.781	1.031	7.237^{-3}	1.766^{-3}	5.171^{-4}
0.178	1.001	7.717^{-3}	1.554^{-3}	-3.546^{-4}	0.795	1.021	4.742^{-3}	1.980^{-3}	6.310^{-4}
0.188	0.990	7.717^{-3}	1.579^{-3}	-3.856^{-4}	0.818	1.008	4.082^{-3}	2.135^{-3}	6.737^{-4}
0.201	1.013	7.299^{-3}	1.469^{-3}	-3.215^{-4}	0.828	1.015	4.266^{-3}	1.930^{-3}	5.970^{-4}
0.215	1.028	6.141^{-3}	1.101^{-3}	-2.709^{-4}	0.838	1.009	7.427^{-3}	2.054^{-3}	5.588^{-4}
0.228	1.018	9.196^{-3}	1.313^{-3}	-2.306^{-4}	0.848	1.012	7.944^{-3}	2.161^{-3}	6.680^{-4}
0.241	1.036	7.910^{-3}	9.739^{-4}	-1.820^{-4}	0.858	0.979	6.743^{-3}	2.241^{-3}	6.160^{-4}
0.255	1.042	7.074^{-3}	6.875^{-4}	-1.354^{-4}	0.868	0.986	5.961^{-3}	2.326^{-3}	7.161^{-4}
0.268	1.044	8.842^{-3}	8.447^{-4}	-1.530^{-4}	0.878	0.954	1.593^{-3}	2.887^{-3}	8.191^{-4}
0.281	1.056	7.942^{-3}	5.107^{-4}	-5.066^{-5}	0.888	0.958	5.395^{-3}	2.615^{-3}	8.687^{-4}
0.295	1.058	9.550^{-3}	5.335^{-4}	-8.685^{-5}	0.898	0.916	-9.414^{-4}	3.215^{-3}	8.396^{-4}
0.308	1.061	1.113^{-2}	4.115^{-4}	-5.480^{-5}	0.908	0.932	2.172^{-3}	3.127^{-3}	9.451^{-4}
0.321	1.054	1.096^{-2}	5.686^{-4}	-1.137^{-4}	0.915	0.923	4.286^{-3}	3.445^{-3}	8.990^{-4}
0.341	1.062	1.095^{-2}	3.704^{-4}	-5.938^{-5}	0.921	0.903	2.090^{-3}	3.612^{-3}	1.048^{-3}
0.361	1.072	7.460^{-3}	1.840^{-4}	-7.237^{-5}	0.928	0.911	2.156^{-3}	3.157^{-3}	8.836^{-4}
0.368	1.069	1.061^{-2}	2.774^{-4}	-2.306^{-5}	0.935	0.893	8.662^{-4}	3.487^{-3}	9.734^{-4}
0.381	1.067	8.810^{-3}	2.140^{-4}	-1.964^{-5}	0.941	0.841	-1.688^{-3}	3.710^{-3}	9.192^{-4}
0.401	1.069	6.624^{-3}	1.799^{-4}	-8.271^{-6}	0.948	0.867	4.768^{-5}	3.569^{-3}	9.470^{-4}
0.441	1.072	9.518^{-3}	1.892^{-4}	6.203^{-6}	0.955	0.835	7.935^{-4}	4.234^{-3}	1.048^{-3}
0.448	1.072	9.350^{-3}	2.606^{-4}	4.098^{-5}					

Table 4. Concluded ($x/H = -2$)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.021	0.813	8.952 ⁻⁴	2.706 ⁻³	-8.220 ⁻⁴	0.521	1.072	6.558 ⁻³	1.353 ⁻⁴	3.346 ⁻⁵
0.028	0.837	5.918 ⁻⁴	2.724 ⁻³	-7.843 ⁻⁴	0.528	1.082	6.637 ⁻³	1.419 ⁻⁴	2.015 ⁻⁵
0.035	0.851	-3.898 ⁻⁴	2.492 ⁻³	-8.184 ⁻⁴	0.548	1.077	4.705 ⁻³	1.207 ⁻⁴	2.109 ⁻⁵
0.041	0.856	-6.589 ⁻⁴	2.703 ⁻³	-7.675 ⁻⁴	0.568	1.081	5.640 ⁻³	1.294 ⁻⁴	1.609 ⁻⁵
0.048	0.896	-1.368 ⁻³	2.167 ⁻³	-6.651 ⁻⁴	0.575	1.074	1.876 ⁻³	1.556 ⁻⁴	6.952 ⁻⁵
0.055	0.898	-2.700 ⁻³	2.014 ⁻³	-6.429 ⁻⁴	0.588	1.083	4.206 ⁻³	1.379 ⁻⁴	2.084 ⁻⁵
0.061	0.908	-2.846 ⁻³	1.748 ⁻³	-5.234 ⁻⁴	0.601	1.071	3.043 ⁻³	1.560 ⁻⁴	4.416 ⁻⁵
0.068	0.898	-7.134 ⁻⁴	2.399 ⁻³	-6.500 ⁻⁴	0.608	1.084	4.382 ⁻³	1.532 ⁻⁴	2.154 ⁻⁵
0.075	0.925	-3.137 ⁻³	1.723 ⁻³	-4.551 ⁻⁴	0.628	1.083	5.390 ⁻³	1.500 ⁻⁴	2.098 ⁻⁵
0.081	0.915	-7.318 ⁻⁴	1.809 ⁻³	-5.529 ⁻⁴	0.648	1.081	5.871 ⁻³	2.001 ⁻⁴	4.571 ⁻⁵
0.088	0.938	-1.697 ⁻³	1.758 ⁻³	-4.597 ⁻⁴	0.668	1.079	3.899 ⁻³	2.329 ⁻⁴	5.178 ⁻⁵
0.098	0.958	-2.293 ⁻³	1.488 ⁻³	-4.057 ⁻⁴	0.681	1.074	3.032 ⁻³	3.865 ⁻⁴	9.253 ⁻⁵
0.108	0.978	-3.459 ⁻³	1.291 ⁻³	-3.340 ⁻⁴	0.695	1.075	3.741 ⁻³	3.927 ⁻⁴	1.134 ⁻⁴
0.118	0.968	-1.789 ⁻³	1.398 ⁻³	-4.143 ⁻⁴	0.708	1.067	3.029 ⁻³	6.388 ⁻⁴	2.079 ⁻⁴
0.128	1.003	-2.413 ⁻³	1.142 ⁻³	-2.569 ⁻⁴	0.721	1.066	4.764 ⁻³	5.909 ⁻⁴	1.631 ⁻⁴
0.138	1.009	-1.720 ⁻³	8.784 ⁻⁴	-1.884 ⁻⁴	0.735	1.055	3.931 ⁻³	8.117 ⁻⁴	1.996 ⁻⁴
0.148	1.021	-1.950 ⁻³	9.565 ⁻⁴	-1.722 ⁻⁴	0.748	1.053	4.144 ⁻³	7.756 ⁻⁴	2.567 ⁻⁴
0.158	1.033	-8.652 ⁻⁴	6.455 ⁻⁴	-1.106 ⁻⁴	0.761	1.048	3.911 ⁻³	9.009 ⁻⁴	2.518 ⁻⁴
0.168	1.048	-3.101 ⁻³	4.233 ⁻⁴	-4.215 ⁻⁵	0.775	1.034	2.757 ⁻³	1.172 ⁻³	3.864 ⁻⁴
0.178	1.046	-7.196 ⁻⁴	4.857 ⁻⁴	-6.668 ⁻⁵	0.788	1.029	2.806 ⁻³	1.206 ⁻³	3.616 ⁻⁴
0.188	1.024	-4.152 ⁻⁴	7.425 ⁻⁴	-1.610 ⁻⁴	0.801	1.008	3.238 ⁻³	1.454 ⁻³	4.238 ⁻⁴
0.201	1.042	-1.170 ⁻³	5.879 ⁻⁴	-4.968 ⁻⁵	0.811	1.007	4.017 ⁻³	1.358 ⁻³	4.409 ⁻⁴
0.215	1.047	1.608 ⁻³	5.026 ⁻⁴	-5.784 ⁻⁵	0.821	0.997	3.136 ⁻³	1.762 ⁻³	5.527 ⁻⁴
0.228	1.060	9.424 ⁻⁴	2.423 ⁻⁴	-3.502 ⁻⁵	0.831	0.997	2.094 ⁻³	1.818 ⁻³	5.433 ⁻⁴
0.241	1.061	7.782 ⁻⁴	2.305 ⁻⁴	-3.629 ⁻⁶	0.841	0.986	2.225 ⁻³	1.759 ⁻³	6.630 ⁻⁴
0.255	1.063	1.272 ⁻³	1.874 ⁻⁴	-2.182 ⁻⁶	0.851	0.974	3.587 ⁻³	1.929 ⁻³	5.941 ⁻⁴
0.268	1.063	8.073 ⁻⁴	1.994 ⁻⁴	-1.705 ⁻⁷	0.861	0.946	1.538 ⁻³	1.890 ⁻³	6.168 ⁻⁴
0.281	1.063	2.288 ⁻³	2.395 ⁻⁴	-2.382 ⁻⁶	0.871	0.953	1.805 ⁻³	2.073 ⁻³	6.946 ⁻⁴
0.308	1.068	2.171 ⁻³	1.145 ⁻⁴	1.360 ⁻⁵	0.881	0.942	2.491 ⁻³	2.041 ⁻³	6.146 ⁻⁴
0.321	1.068	2.964 ⁻³	1.101 ⁻⁴	8.031 ⁻⁶	0.891	0.924	8.564 ⁻⁴	2.029 ⁻³	6.940 ⁻⁴
0.361	1.069	8.505 ⁻⁴	1.067 ⁻⁴	9.917 ⁻⁶	0.901	0.929	2.560 ⁻³	2.035 ⁻³	6.392 ⁻⁴
0.381	1.068	3.350 ⁻³	1.120 ⁻⁴	1.847 ⁻⁵	0.908	0.897	5.232 ⁻⁴	1.990 ⁻³	6.991 ⁻⁴
0.388	1.079	4.760 ⁻³	1.317 ⁻⁴	1.184 ⁻⁵	0.915	0.886	-4.748 ⁻⁴	2.139 ⁻³	6.875 ⁻⁴
0.401	1.070	3.115 ⁻⁴	9.779 ⁻⁵	2.219 ⁻⁵	0.921	0.880	9.382 ⁻⁵	2.167 ⁻³	6.563 ⁻⁴
0.415	1.081	5.140 ⁻³	1.212 ⁻⁴	2.117 ⁻⁵	0.928	0.864	-1.592 ⁻³	2.243 ⁻³	7.261 ⁻⁴
0.468	1.081	6.188 ⁻³	1.250 ⁻⁴	1.155 ⁻⁵	0.935	0.853	-7.411 ⁻⁴	2.194 ⁻³	6.421 ⁻⁴
0.481	1.070	2.542 ⁻³	1.138 ⁻⁴	4.421 ⁻⁵	0.941	0.852	4.594 ⁻⁴	2.197 ⁻³	6.830 ⁻⁴
0.488	1.081	3.613 ⁻³	1.210 ⁻⁴	1.967 ⁻⁵	0.948	0.834	-2.539 ⁻⁴	2.174 ⁻³	6.588 ⁻⁴
0.501	1.071	4.386 ⁻⁴	1.219 ⁻⁴	4.528 ⁻⁵	0.955	0.811	1.627 ⁻³	2.435 ⁻³	7.954 ⁻⁴
0.508	1.081	6.114 ⁻³	1.321 ⁻⁴	1.448 ⁻⁵	0.968	0.792	-1.173 ⁻⁴	3.392 ⁻³	8.872 ⁻⁴

Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)

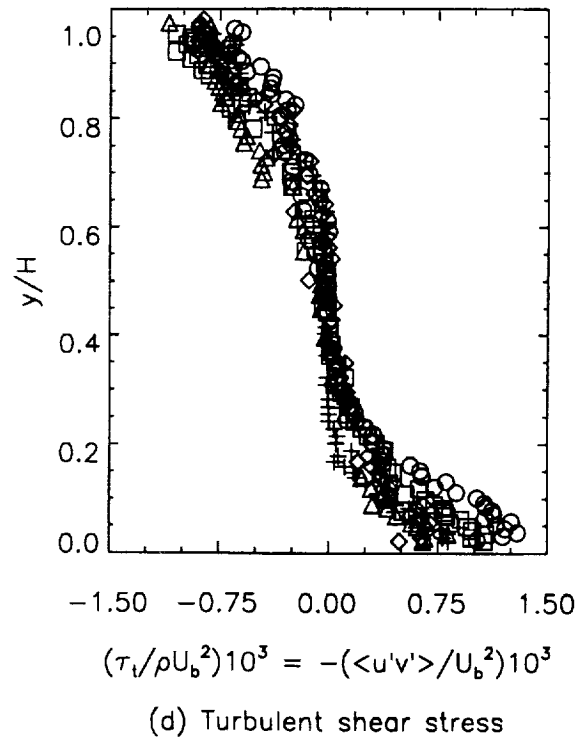
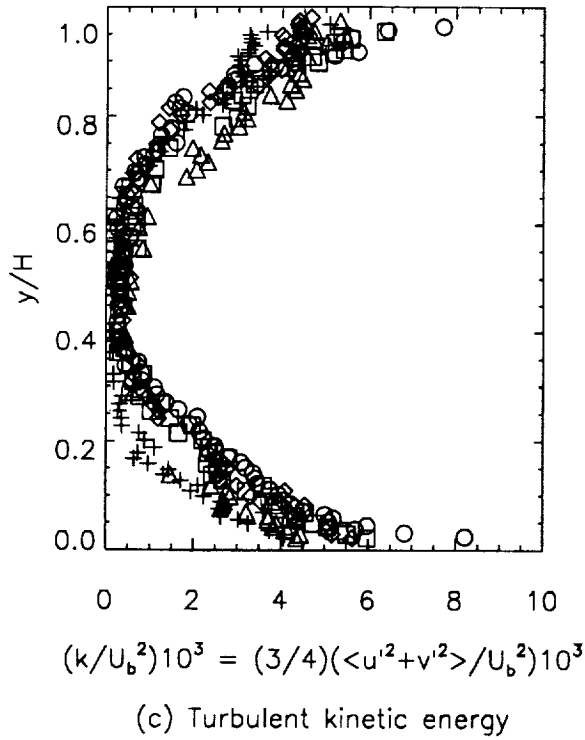
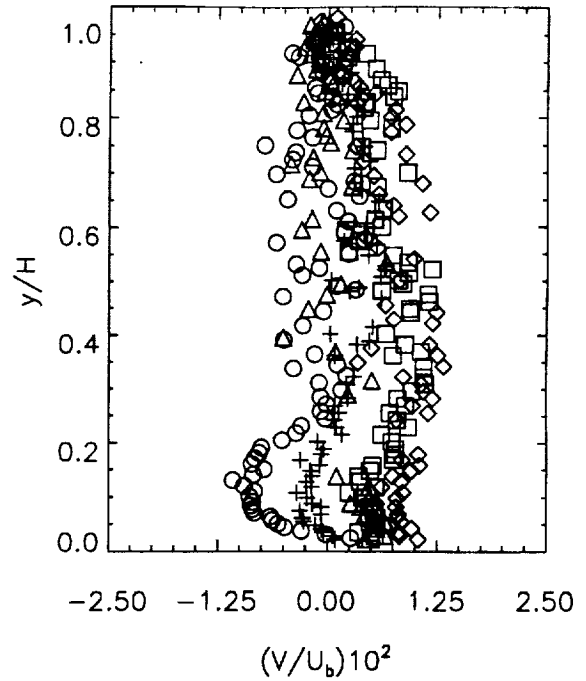
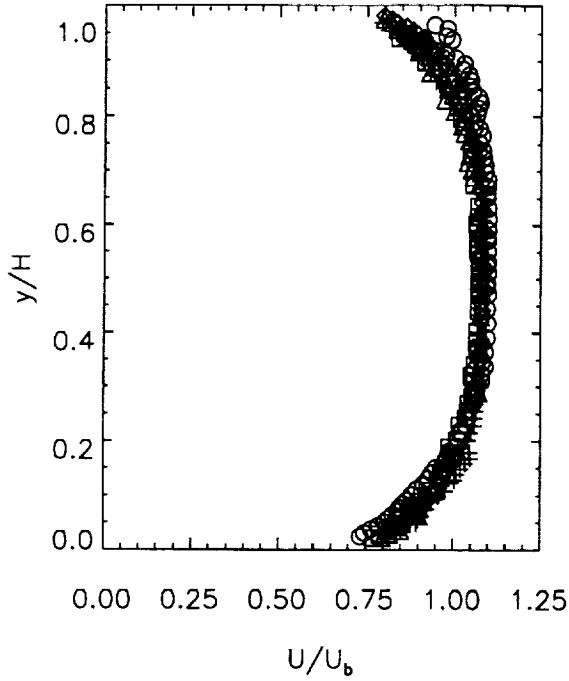


Figure 4. Summary of Table 4 ($x/H = -2$).

Table 5. LDV flowfield data in TAD ($x/H = -1$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

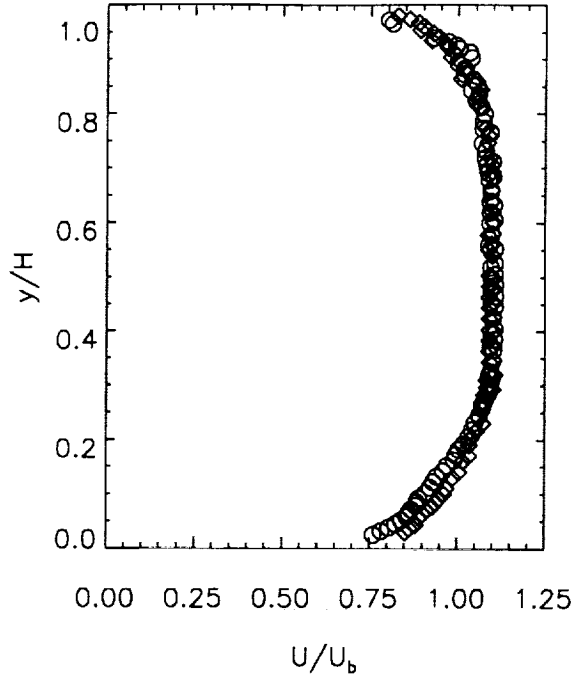
y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.025	0.761	-7.085 ⁻³	4.326 ⁻³	-1.564 ⁻³	0.479	1.096	-1.890 ⁻²	1.509 ⁻⁴	-3.896 ⁻⁸
0.032	0.784	-1.163 ⁻²	3.698 ⁻³	-1.543 ⁻³	0.485	1.108	-1.859 ⁻²	2.605 ⁻⁴	3.864 ⁻⁵
0.039	0.805	-1.176 ⁻²	3.277 ⁻³	-1.367 ⁻³	0.499	1.096	-1.866 ⁻²	1.472 ⁻⁴	6.998 ⁻⁷
0.045	0.825	-1.229 ⁻²	3.089 ⁻³	-1.014 ⁻³	0.505	1.107	-2.120 ⁻²	2.823 ⁻⁴	7.076 ⁻⁵
0.052	0.841	-1.438 ⁻²	3.018 ⁻³	-1.087 ⁻³	0.519	1.095	-1.624 ⁻²	1.424 ⁻⁴	3.108 ⁻⁸
0.059	0.856	-1.482 ⁻²	2.961 ⁻³	-1.058 ⁻³	0.525	1.107	-1.671 ⁻²	2.324 ⁻⁴	3.950 ⁻⁵
0.065	0.862	-1.475 ⁻²	3.080 ⁻³	-1.065 ⁻³	0.552	1.107	-1.447 ⁻²	2.289 ⁻⁴	5.118 ⁻⁵
0.072	0.869	-1.627 ⁻²	2.721 ⁻³	-1.023 ⁻³	0.559	1.088	-1.919 ⁻²	2.130 ⁻⁴	5.432 ⁻⁵
0.079	0.882	-1.679 ⁻²	2.607 ⁻³	-9.201 ⁻⁴	0.579	1.097	-1.883 ⁻²	2.517 ⁻⁴	6.184 ⁻⁵
0.085	0.884	-1.574 ⁻²	2.381 ⁻³	-9.081 ⁻⁴	0.599	1.092	-1.671 ⁻²	1.594 ⁻⁴	1.650 ⁻⁵
0.092	0.890	-1.571 ⁻²	2.466 ⁻³	-9.266 ⁻⁴	0.605	1.105	-1.540 ⁻²	2.663 ⁻⁴	6.767 ⁻⁵
0.102	0.910	-1.627 ⁻²	2.381 ⁻³	-8.409 ⁻⁴	0.619	1.092	-1.686 ⁻²	1.235 ⁻⁴	8.688 ⁻⁸
0.112	0.922	-1.659 ⁻²	2.257 ⁻³	-7.859 ⁻⁴	0.632	1.103	-1.305 ⁻²	2.441 ⁻⁴	5.371 ⁻⁵
0.122	0.932	-1.764 ⁻²	2.192 ⁻³	-8.076 ⁻⁴	0.639	1.092	-1.365 ⁻²	1.257 ⁻⁴	7.943 ⁻⁸
0.132	0.941	-1.765 ⁻²	2.164 ⁻³	-7.419 ⁻⁴	0.659	1.095	-1.619 ⁻²	2.786 ⁻⁴	9.606 ⁻⁵
0.142	0.960	-1.792 ⁻²	1.991 ⁻³	-6.343 ⁻⁴	0.679	1.088	-1.485 ⁻²	1.373 ⁻⁴	1.716 ⁻⁵
0.152	0.970	-1.998 ⁻²	1.915 ⁻³	-5.581 ⁻⁴	0.685	1.101	-1.342 ⁻²	3.231 ⁻⁴	1.057 ⁻⁴
0.162	0.991	-1.991 ⁻²	1.796 ⁻³	-4.889 ⁻⁴	0.692	1.085	-1.547 ⁻²	2.359 ⁻⁴	6.232 ⁻⁸
0.172	0.995	-1.962 ⁻²	1.679 ⁻³	-4.578 ⁻⁴	0.705	1.081	-1.545 ⁻²	3.472 ⁻⁴	1.119 ⁻⁴
0.182	1.004	-1.964 ⁻²	1.551 ⁻³	-3.832 ⁻⁴	0.712	1.099	-1.104 ⁻²	4.905 ⁻⁴	2.352 ⁻⁴
0.192	1.017	-1.913 ⁻²	1.442 ⁻³	-3.429 ⁻⁴	0.719	1.077	-1.650 ⁻²	5.187 ⁻⁴	1.804 ⁻⁴
0.205	1.033	-1.785 ⁻²	1.646 ⁻³	-3.834 ⁻⁴	0.732	1.079	-1.517 ⁻²	3.891 ⁻⁴	9.231 ⁻⁵
0.219	1.042	-1.853 ⁻²	1.322 ⁻³	-2.848 ⁻⁴	0.745	1.068	-1.714 ⁻²	6.288 ⁻⁴	2.053 ⁻⁴
0.232	1.050	-1.752 ⁻²	1.169 ⁻³	-2.379 ⁻⁴	0.765	1.092	-1.011 ⁻²	6.776 ⁻⁴	2.941 ⁻⁴
0.245	1.062	-1.823 ⁻²	1.153 ⁻³	-1.949 ⁻⁴	0.772	1.069	-1.305 ⁻²	5.398 ⁻⁴	1.414 ⁻⁴
0.259	1.071	-1.868 ⁻²	9.445 ⁻⁴	-1.444 ⁻⁴	0.785	1.071	-1.311 ⁻²	5.051 ⁻⁴	1.195 ⁻⁴
0.265	1.071	-1.476 ⁻²	7.171 ⁻⁴	-9.122 ⁻⁵	0.799	1.075	-1.100 ⁻²	4.339 ⁻⁴	1.041 ⁻⁴
0.272	1.079	-1.793 ⁻²	8.060 ⁻⁴	-9.875 ⁻⁵	0.812	1.065	-9.859 ⁻³	7.689 ⁻⁴	1.625 ⁻⁴
0.285	1.089	-1.783 ⁻²	7.242 ⁻⁴	-1.000 ⁻⁴	0.822	1.051	-1.207 ⁻²	1.080 ⁻³	2.909 ⁻⁴
0.292	1.088	-1.684 ⁻²	4.773 ⁻⁴	-6.947 ⁻⁵	0.832	1.057	-1.042 ⁻²	1.035 ⁻³	2.534 ⁻⁴
0.299	1.091	-1.760 ⁻²	6.589 ⁻⁴	-6.200 ⁻⁵	0.842	1.036	-1.116 ⁻²	1.562 ⁻³	3.717 ⁻⁴
0.312	1.099	-1.939 ⁻²	5.023 ⁻⁴	-6.930 ⁻⁵	0.852	1.054	-8.121 ⁻³	9.033 ⁻⁴	1.716 ⁻⁴
0.319	1.089	-1.580 ⁻²	3.818 ⁻⁴	-3.164 ⁻⁵	0.862	1.042	-8.555 ⁻³	1.329 ⁻³	2.382 ⁻⁴
0.325	1.094	-1.605 ⁻²	5.430 ⁻⁴	-7.847 ⁻⁵	0.872	1.016	-8.323 ⁻³	1.893 ⁻³	4.000 ⁻⁴
0.345	1.100	-1.698 ⁻²	3.442 ⁻⁴	-4.034 ⁻⁵	0.882	1.017	-8.298 ⁻³	1.956 ⁻³	4.141 ⁻⁴
0.365	1.103	-1.519 ⁻²	3.869 ⁻⁴	-3.713 ⁻⁵	0.892	0.998	-8.043 ⁻³	2.381 ⁻³	4.794 ⁻⁴
0.372	1.094	-1.668 ⁻²	2.342 ⁻⁴	-1.409 ⁻⁵	0.902	1.037	-7.075 ⁻³	1.747 ⁻³	2.467 ⁻⁴
0.385	1.106	-1.678 ⁻²	3.512 ⁻⁴	-2.569 ⁻⁵	0.912	1.032	-3.844 ⁻³	1.937 ⁻³	3.373 ⁻⁴
0.399	1.095	-1.854 ⁻²	2.231 ⁻⁴	-1.604 ⁻⁵	0.919	1.002	-7.826 ⁻³	2.360 ⁻³	3.763 ⁻⁴
0.405	1.106	-1.563 ⁻²	3.726 ⁻⁴	8.821 ⁻⁶	0.925	0.994	-6.442 ⁻³	3.047 ⁻³	4.436 ⁻⁴
0.425	1.101	-1.688 ⁻²	2.173 ⁻⁴	7.296 ⁻⁶	0.932	0.970	-4.811 ⁻³	3.623 ⁻³	5.441 ⁻⁴
0.445	1.107	-1.496 ⁻²	2.445 ⁻⁴	-5.899 ⁻⁶	0.939	0.930	-4.026 ⁻³	3.784 ⁻³	7.014 ⁻⁴
0.452	1.095	-1.894 ⁻²	1.436 ⁻⁴	-8.233 ⁻⁶	0.965	0.812	2.171 ⁻³	4.551 ⁻³	4.854 ⁻⁴
0.465	1.108	-1.736 ⁻²	2.511 ⁻⁴	1.156 ⁻⁵	0.972	0.801	3.498 ⁻³	7.396 ⁻³	6.769 ⁻⁴

Table 5. Concluded ($x/H = -1$)

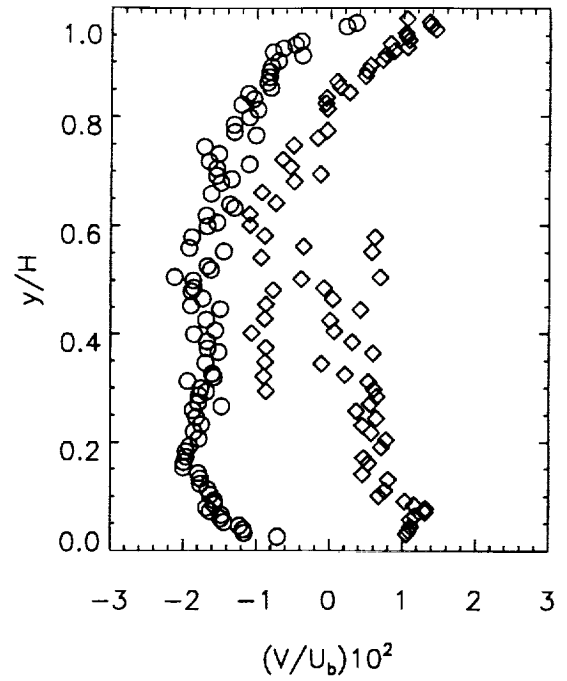
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.030	0.851	1.055 ⁻²	2.695 ⁻³	-8.000 ⁻⁴	0.483	1.091	-8.366 ⁻⁴	2.308 ⁻⁴	-2.631 ⁻⁵
0.037	0.864	1.085 ⁻²	2.631 ⁻³	-7.768 ⁻⁴	0.500	1.099	-3.906 ⁻³	1.329 ⁻⁴	-1.863 ⁻⁵
0.043	0.881	1.112 ⁻²	2.453 ⁻³	-7.999 ⁻⁴	0.503	1.089	6.888 ⁻³	1.702 ⁻⁴	-3.408 ⁻⁵
0.057	0.892	1.111 ⁻²	2.454 ⁻³	-5.958 ⁻⁴	0.540	1.099	-9.382 ⁻³	1.236 ⁻⁴	-1.222 ⁻⁵
0.063	0.902	1.174 ⁻²	2.565 ⁻³	-6.772 ⁻⁴	0.550	1.088	5.761 ⁻³	2.208 ⁻⁴	8.105 ⁻⁶
0.070	0.913	1.312 ⁻²	2.532 ⁻³	-5.521 ⁻⁴	0.560	1.097	-3.612 ⁻³	1.442 ⁻⁴	-2.442 ⁻⁵
0.077	0.929	1.319 ⁻²	2.470 ⁻³	-4.670 ⁻⁴	0.577	1.087	6.149 ⁻³	1.495 ⁻⁴	7.436 ⁻⁶
0.083	0.937	1.159 ⁻²	2.156 ⁻³	-5.035 ⁻⁴	0.580	1.100	-8.881 ⁻³	1.912 ⁻⁴	-1.115 ⁻⁵
0.090	0.947	1.033 ⁻²	2.364 ⁻³	-6.838 ⁻⁴	0.600	1.102	-1.091 ⁻²	1.461 ⁻⁴	-2.137 ⁻⁵
0.100	0.962	6.762 ⁻³	2.355 ⁻³	-6.221 ⁻⁴	0.620	1.098	-1.096 ⁻²	2.326 ⁻⁴	6.153 ⁻⁷
0.110	0.968	7.556 ⁻³	2.136 ⁻³	-6.227 ⁻⁴	0.640	1.098	-7.385 ⁻³	1.700 ⁻⁴	4.128 ⁻⁷
0.130	0.987	8.029 ⁻³	1.774 ⁻³	-4.748 ⁻⁴	0.660	1.097	-9.297 ⁻³	2.754 ⁻⁴	5.915 ⁻⁵
0.140	1.004	4.524 ⁻³	1.795 ⁻³	-5.456 ⁻⁴	0.680	1.099	-4.888 ⁻³	1.931 ⁻⁴	-1.123 ⁻⁶
0.160	1.016	5.325 ⁻³	1.404 ⁻³	-3.927 ⁻⁴	0.693	1.098	-1.312 ⁻³	1.779 ⁻⁴	5.066 ⁻⁶
0.170	1.033	4.658 ⁻³	1.459 ⁻³	-3.717 ⁻⁴	0.707	1.096	-5.390 ⁻³	1.973 ⁻⁴	3.074 ⁻⁵
0.190	1.034	7.095 ⁻³	1.204 ⁻³	-3.172 ⁻⁴	0.720	1.091	-6.449 ⁻³	3.923 ⁻⁴	1.192 ⁻⁴
0.203	1.040	7.727 ⁻³	1.096 ⁻³	-3.400 ⁻⁴	0.747	1.085	-4.969 ⁻³	4.346 ⁻⁴	1.195 ⁻⁴
0.217	1.055	5.717 ⁻³	9.226 ⁻⁴	-2.575 ⁻⁴	0.760	1.087	-1.692 ⁻³	3.866 ⁻⁴	9.464 ⁻⁵
0.230	1.073	4.521 ⁻³	6.750 ⁻⁴	-1.920 ⁻⁴	0.773	1.078	-3.943 ⁻⁴	8.026 ⁻⁴	1.597 ⁻⁴
0.243	1.060	6.385 ⁻³	6.806 ⁻⁴	-1.542 ⁻⁴	0.813	1.064	-3.904 ⁻⁴	8.485 ⁻⁴	2.303 ⁻⁴
0.257	1.072	3.663 ⁻³	6.479 ⁻⁴	-1.763 ⁻⁴	0.823	1.049	-5.996 ⁻⁴	1.380 ⁻³	2.509 ⁻⁴
0.270	1.073	5.583 ⁻³	5.098 ⁻⁴	-1.064 ⁻⁴	0.833	1.058	-5.335 ⁻⁴	1.133 ⁻³	2.426 ⁻⁴
0.283	1.076	6.432 ⁻³	4.372 ⁻⁴	-9.519 ⁻⁵	0.843	1.064	2.611 ⁻³	1.144 ⁻³	1.834 ⁻⁴
0.293	1.101	-8.685 ⁻³	2.427 ⁻⁴	-5.733 ⁻⁵	0.853	1.046	1.333 ⁻³	1.291 ⁻³	2.722 ⁻⁴
0.297	1.084	6.046 ⁻³	3.455 ⁻⁴	-6.620 ⁻⁵	0.863	1.008	9.231 ⁻⁴	1.914 ⁻³	3.626 ⁻⁴
0.310	1.084	5.282 ⁻³	2.679 ⁻⁴	-2.299 ⁻⁵	0.873	1.027	4.808 ⁻³	1.663 ⁻³	2.736 ⁻⁴
0.320	1.106	-9.032 ⁻³	1.671 ⁻⁴	-3.030 ⁻⁵	0.883	1.021	5.012 ⁻³	2.031 ⁻³	3.372 ⁻⁴
0.323	1.091	2.088 ⁻³	2.212 ⁻⁴	-2.356 ⁻⁵	0.893	1.004	5.446 ⁻³	2.095 ⁻³	3.903 ⁻⁴
0.343	1.092	-1.132 ⁻³	2.889 ⁻⁴	-6.156 ⁻⁵	0.903	0.979	7.146 ⁻³	2.200 ⁻³	3.978 ⁻⁴
0.347	1.104	-8.843 ⁻³	1.333 ⁻⁴	-2.213 ⁻⁵	0.913	0.984	7.561 ⁻³	2.204 ⁻³	4.666 ⁻⁴
0.363	1.091	5.927 ⁻³	2.012 ⁻⁴	-3.031 ⁻⁵	0.920	0.970	8.658 ⁻³	2.845 ⁻³	5.435 ⁻⁴
0.373	1.104	-8.731 ⁻³	1.401 ⁻⁴	-1.904 ⁻⁵	0.927	0.965	1.052 ⁻²	2.561 ⁻³	5.866 ⁻⁴
0.383	1.091	3.062 ⁻³	2.043 ⁻⁴	-3.822 ⁻⁵	0.933	0.923	8.224 ⁻³	2.780 ⁻³	6.150 ⁻⁴
0.400	1.105	-1.069 ⁻²	1.282 ⁻⁴	-2.032 ⁻⁵	0.940	0.944	1.071 ⁻²	3.002 ⁻³	8.878 ⁻⁴
0.403	1.091	5.962 ⁻⁴	2.210 ⁻⁴	-4.811 ⁻⁵	0.947	0.929	1.042 ⁻²	2.885 ⁻³	7.965 ⁻⁴
0.423	1.091	3.511 ⁻⁵	1.599 ⁻⁴	-2.706 ⁻⁵	0.953	0.891	1.032 ⁻²	3.120 ⁻³	8.065 ⁻⁴
0.427	1.103	-8.903 ⁻³	1.850 ⁻⁴	-3.576 ⁻⁵	0.960	0.901	1.443 ⁻²	3.423 ⁻³	8.793 ⁻⁴
0.443	1.092	4.172 ⁻³	2.258 ⁻⁴	-1.448 ⁻⁵	0.967	0.886	1.374 ⁻²	3.511 ⁻³	7.123 ⁻⁴
0.453	1.104	-8.741 ⁻³	1.723 ⁻⁴	-2.215 ⁻⁵	0.973	0.860	1.358 ⁻²	4.201 ⁻³	1.186 ⁻³
0.463	1.090	3.774 ⁻⁴	1.602 ⁻⁴	-2.244 ⁻⁵	0.980	0.828	1.048 ⁻²	4.639 ⁻³	1.404 ⁻³
0.480	1.102	-7.759 ⁻³	1.887 ⁻⁴	-2.956 ⁻⁵					

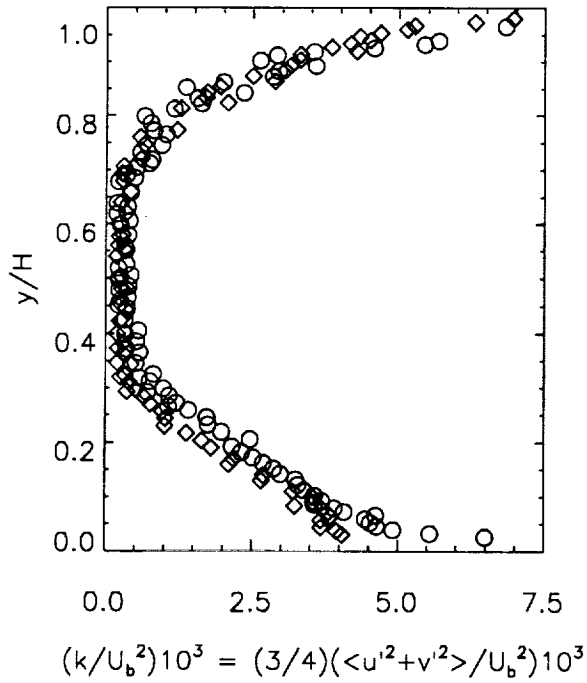
Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)



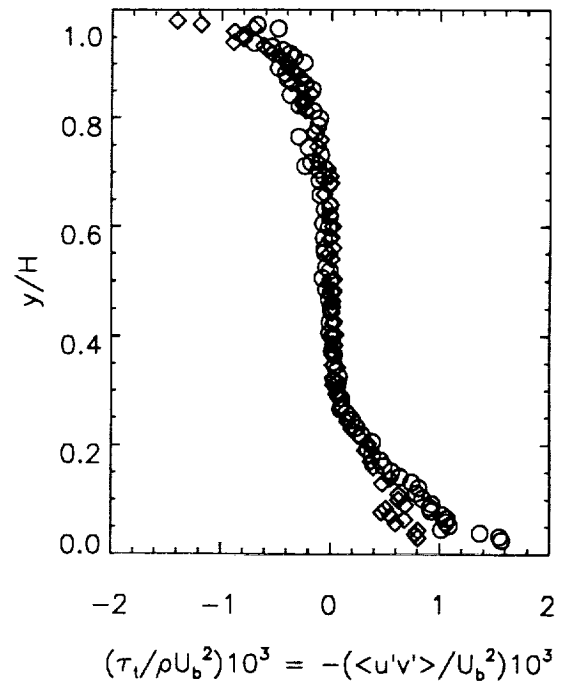
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 5. Summary of Table 5 ($x/H = -1$).

Table 6. LDV flowfield in TAD ($\theta = 0$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.023	1.180	-6.091 ⁻²	1.927 ⁻³	-5.593 ⁻⁴	0.443	1.099	-2.347 ⁻¹	2.428 ⁻⁴	5.246 ⁻⁵
0.029	1.190	-7.114 ⁻²	2.017 ⁻³	-6.244 ⁻⁴	0.453	1.082	-2.346 ⁻¹	3.442 ⁻⁴	1.088 ⁻⁴
0.036	1.195	-8.341 ⁻²	2.035 ⁻³	-5.975 ⁻⁴	0.463	1.083	-2.353 ⁻¹	3.960 ⁻⁴	1.587 ⁻⁴
0.043	1.190	-9.351 ⁻²	1.936 ⁻³	-6.034 ⁻⁴	0.480	1.073	-2.293 ⁻¹	2.425 ⁻⁴	4.131 ⁻⁵
0.049	1.190	-1.032 ⁻¹	1.913 ⁻³	-6.334 ⁻⁴	0.483	1.076	-2.306 ⁻¹	3.735 ⁻⁴	1.597 ⁻⁴
0.056	1.196	-1.133 ⁻¹	1.925 ⁻³	-6.173 ⁻⁴	0.500	1.061	-2.250 ⁻¹	3.170 ⁻⁴	1.027 ⁻⁴
0.063	1.195	-1.218 ⁻¹	1.902 ⁻³	-6.173 ⁻⁴	0.503	1.063	-2.291 ⁻¹	4.777 ⁻⁴	2.143 ⁻⁴
0.069	1.199	-1.309 ⁻¹	1.796 ⁻³	-6.195 ⁻⁴	0.520	1.051	-2.215 ⁻¹	4.162 ⁻⁴	1.590 ⁻⁴
0.076	1.206	-1.410 ⁻¹	1.721 ⁻³	-5.372 ⁻⁴	0.523	1.050	-2.263 ⁻¹	5.219 ⁻⁴	2.236 ⁻⁴
0.083	1.209	-1.491 ⁻¹	1.877 ⁻³	-6.269 ⁻⁴	0.540	1.040	-2.171 ⁻¹	5.379 ⁻⁴	2.313 ⁻⁴
0.109	1.214	-1.744 ⁻¹	1.528 ⁻³	-5.116 ⁻⁴	0.549	1.043	-2.164 ⁻¹	5.114 ⁻⁴	2.090 ⁻⁴
0.119	1.214	-1.827 ⁻¹	1.529 ⁻³	-4.713 ⁻⁴	0.560	1.036	-2.108 ⁻¹	3.768 ⁻⁴	1.173 ⁻⁴
0.129	1.221	-1.922 ⁻¹	1.510 ⁻³	-4.764 ⁻⁴	0.576	1.025	-2.111 ⁻¹	6.984 ⁻⁴	2.547 ⁻⁴
0.139	1.223	-1.987 ⁻¹	1.372 ⁻³	-4.115 ⁻⁴	0.580	1.023	-2.076 ⁻¹	5.208 ⁻⁴	2.155 ⁻⁴
0.149	1.222	-2.043 ⁻¹	1.344 ⁻³	-3.937 ⁻⁴	0.600	1.006	-1.977 ⁻¹	6.120 ⁻⁴	2.034 ⁻⁴
0.159	1.222	-2.108 ⁻¹	1.213 ⁻³	-3.758 ⁻⁴	0.603	1.028	-1.992 ⁻¹	4.672 ⁻⁴	1.759 ⁻⁴
0.169	1.223	-2.151 ⁻¹	1.147 ⁻³	-2.995 ⁻⁴	0.620	1.012	-1.955 ⁻¹	4.207 ⁻⁴	1.522 ⁻⁴
0.179	1.224	-2.176 ⁻¹	9.131 ⁻⁴	-2.351 ⁻⁴	0.629	1.017	-1.904 ⁻¹	5.875 ⁻⁴	1.583 ⁻⁴
0.189	1.221	-2.217 ⁻¹	9.587 ⁻⁴	-2.423 ⁻⁴	0.660	0.983	-1.861 ⁻¹	1.092 ⁻³	3.302 ⁻⁴
0.203	1.220	-2.288 ⁻¹	7.830 ⁻⁴	-1.513 ⁻⁴	0.680	0.971	-1.819 ⁻¹	1.193 ⁻³	3.537 ⁻⁴
0.216	1.214	-2.294 ⁻¹	6.989 ⁻⁴	-1.169 ⁻⁴	0.683	0.986	-1.743 ⁻¹	1.073 ⁻³	3.277 ⁻⁴
0.229	1.210	-2.330 ⁻¹	5.918 ⁻⁴	-1.161 ⁻⁴	0.693	0.964	-1.789 ⁻¹	1.440 ⁻³	4.407 ⁻⁴
0.240	1.200	-2.406 ⁻¹	5.285 ⁻⁴	-1.126 ⁻⁴	0.720	0.946	-1.674 ⁻¹	1.779 ⁻³	4.532 ⁻⁴
0.243	1.208	-2.395 ⁻¹	4.065 ⁻⁴	-4.707 ⁻⁵	0.733	0.937	-1.627 ⁻¹	2.005 ⁻³	4.687 ⁻⁴
0.256	1.197	-2.396 ⁻¹	4.563 ⁻⁴	-6.774 ⁻⁵	0.760	0.913	-1.521 ⁻¹	2.796 ⁻³	6.172 ⁻⁴
0.267	1.186	-2.446 ⁻¹	4.015 ⁻⁴	-4.956 ⁻⁵	0.773	0.892	-1.475 ⁻¹	3.057 ⁻³	6.339 ⁻⁴
0.269	1.192	-2.415 ⁻¹	3.661 ⁻⁴	-4.653 ⁻⁵	0.787	0.894	-1.429 ⁻¹	3.071 ⁻³	6.496 ⁻⁴
0.283	1.187	-2.482 ⁻¹	2.862 ⁻⁴	-1.442 ⁻⁶	0.800	0.889	-1.356 ⁻¹	2.988 ⁻³	6.521 ⁻⁴
0.293	1.170	-2.459 ⁻¹	3.852 ⁻⁴	-3.930 ⁻⁵	0.813	0.862	-1.288 ⁻¹	3.322 ⁻³	7.222 ⁻⁴
0.296	1.178	-2.481 ⁻¹	3.297 ⁻⁴	-4.856 ⁻⁶	0.823	0.853	-1.233 ⁻¹	3.836 ⁻³	7.772 ⁻⁴
0.309	1.169	-2.481 ⁻¹	2.630 ⁻⁴	2.609 ⁻⁵	0.833	0.834	-1.223 ⁻¹	3.721 ⁻³	8.324 ⁻⁴
0.320	1.156	-2.471 ⁻¹	2.899 ⁻⁴	-6.760 ⁻⁶	0.843	0.828	-1.148 ⁻¹	3.878 ⁻³	7.468 ⁻⁴
0.323	1.164	-2.474 ⁻¹	2.887 ⁻⁴	2.312 ⁻⁵	0.853	0.812	-1.102 ⁻¹	4.093 ⁻³	9.168 ⁻⁴
0.343	1.154	-2.408 ⁻¹	2.783 ⁻⁴	2.987 ⁻⁵	0.863	0.792	-1.053 ⁻¹	4.438 ⁻³	8.123 ⁻⁴
0.347	1.142	-2.452 ⁻¹	2.632 ⁻⁴	-1.814 ⁻⁶	0.873	0.767	-1.011 ⁻¹	4.664 ⁻³	9.691 ⁻⁴
0.363	1.143	-2.367 ⁻¹	2.182 ⁻⁴	9.050 ⁻⁶	0.883	0.753	-9.311 ⁻²	4.609 ⁻³	9.312 ⁻⁴
0.373	1.127	-2.434 ⁻¹	2.722 ⁻⁴	3.571 ⁻⁵	0.903	0.715	-8.288 ⁻²	4.751 ⁻³	9.555 ⁻⁴
0.383	1.131	-2.391 ⁻¹	2.183 ⁻⁴	3.094 ⁻⁵	0.913	0.692	-7.693 ⁻²	4.872 ⁻³	9.301 ⁻⁴
0.400	1.111	-2.418 ⁻¹	3.057 ⁻⁴	8.876 ⁻⁵	0.920	0.670	-7.389 ⁻²	5.294 ⁻³	7.078 ⁻⁴
0.403	1.120	-2.404 ⁻¹	2.370 ⁻⁴	4.812 ⁻⁵	0.927	0.641	-6.572 ⁻²	5.315 ⁻³	8.238 ⁻⁴
0.423	1.111	-2.354 ⁻¹	2.442 ⁻⁴	6.144 ⁻⁵	0.933	0.615	-6.076 ⁻²	6.190 ⁻³	6.824 ⁻⁴
0.427	1.101	-2.350 ⁻¹	2.226 ⁻⁴	1.575 ⁻⁵					

Table 6. Continued ($\theta = 0$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.033	1.228	-7.237 ⁻²	1.892 ⁻³	-2.908 ⁻⁴	0.560	1.023	-1.938 ⁻¹	2.316 ⁻⁴	6.349 ⁻⁵
0.040	1.237	-8.381 ⁻²	1.863 ⁻³	-2.286 ⁻⁴	0.573	1.035	-1.824 ⁻¹	2.260 ⁻⁴	6.937 ⁻⁵
0.047	1.243	-9.738 ⁻²	1.514 ⁻³	-3.922 ⁻⁴	0.580	1.011	-1.952 ⁻¹	2.678 ⁻⁴	8.983 ⁻⁵
0.053	1.247	-9.990 ⁻²	1.966 ⁻³	-1.776 ⁻⁴	0.600	1.010	-1.865 ⁻¹	2.799 ⁻⁴	9.414 ⁻⁵
0.060	1.245	-1.104 ⁻¹	2.045 ⁻³	-1.772 ⁻⁴	0.620	0.992	-1.844 ⁻¹	4.109 ⁻⁴	1.603 ⁻⁴
0.073	1.257	-1.204 ⁻¹	1.932 ⁻³	-3.111 ⁻⁴	0.640	0.977	-1.805 ⁻¹	6.042 ⁻⁴	2.374 ⁻⁴
0.097	1.262	-1.482 ⁻¹	1.360 ⁻³	-2.962 ⁻⁴	0.660	0.973	-1.694 ⁻¹	5.730 ⁻⁴	2.241 ⁻⁴
0.117	1.261	-1.635 ⁻¹	1.298 ⁻³	-1.505 ⁻⁴	0.680	0.968	-1.636 ⁻¹	7.103 ⁻⁴	2.481 ⁻⁴
0.137	1.254	-1.786 ⁻¹	1.082 ⁻³	-1.290 ⁻⁴	0.693	0.950	-1.620 ⁻¹	8.888 ⁻⁴	3.034 ⁻⁴
0.147	1.245	-1.810 ⁻¹	1.053 ⁻³	-7.599 ⁻⁵	0.707	0.952	-1.542 ⁻¹	8.966 ⁻⁴	3.118 ⁻⁴
0.157	1.253	-1.891 ⁻¹	8.739 ⁻⁴	-1.218 ⁻⁴	0.720	0.926	-1.548 ⁻¹	1.269 ⁻³	4.069 ⁻⁴
0.177	1.245	-2.039 ⁻¹	6.811 ⁻⁴	-7.980 ⁻⁵	0.733	0.928	-1.455 ⁻¹	1.382 ⁻³	3.990 ⁻⁴
0.187	1.243	-2.068 ⁻¹	5.349 ⁻⁴	-1.125 ⁻⁴	0.747	0.911	-1.448 ⁻¹	1.397 ⁻³	3.794 ⁻⁴
0.200	1.244	-2.138 ⁻¹	4.063 ⁻⁴	-4.087 ⁻⁵	0.760	0.900	-1.356 ⁻¹	1.765 ⁻³	4.755 ⁻⁴
0.213	1.238	-2.167 ⁻¹	3.225 ⁻⁴	-7.512 ⁻⁵	0.773	0.867	-1.353 ⁻¹	2.216 ⁻³	6.170 ⁻⁴
0.227	1.231	-2.223 ⁻¹	2.721 ⁻⁴	-1.282 ⁻⁵	0.787	0.874	-1.284 ⁻¹	2.262 ⁻³	5.928 ⁻⁴
0.240	1.209	-2.281 ⁻¹	2.024 ⁻⁴	-1.271 ⁻⁵	0.800	0.864	-1.220 ⁻¹	2.570 ⁻³	6.869 ⁻⁴
0.253	1.209	-2.226 ⁻¹	2.388 ⁻⁴	2.918 ⁻⁵	0.813	0.828	-1.195 ⁻¹	2.591 ⁻³	6.846 ⁻⁴
0.267	1.186	-2.335 ⁻¹	1.851 ⁻⁴	-5.613 ⁻⁶	0.823	0.841	-1.133 ⁻¹	2.267 ⁻³	6.620 ⁻⁴
0.280	1.186	-2.272 ⁻¹	1.559 ⁻⁴	4.542 ⁻⁶	0.833	0.828	-1.084 ⁻¹	2.642 ⁻³	6.991 ⁻⁴
0.293	1.171	-2.338 ⁻¹	1.922 ⁻⁴	-4.679 ⁻⁷	0.843	0.821	-1.030 ⁻¹	2.840 ⁻³	8.514 ⁻⁴
0.307	1.170	-2.250 ⁻¹	1.457 ⁻⁴	-5.032 ⁻⁶	0.853	0.804	-9.947 ⁻²	2.889 ⁻³	8.492 ⁻⁴
0.320	1.152	-2.327 ⁻¹	1.516 ⁻⁴	4.143 ⁻⁶	0.863	0.792	-9.181 ⁻²	3.207 ⁻³	8.959 ⁻⁴
0.340	1.145	-2.216 ⁻¹	1.648 ⁻⁴	-1.403 ⁻⁵	0.873	0.775	-8.950 ⁻²	3.761 ⁻³	9.383 ⁻⁴
0.347	1.131	-2.355 ⁻¹	1.486 ⁻⁴	1.613 ⁻⁵	0.883	0.761	-8.355 ⁻²	3.767 ⁻³	9.781 ⁻⁴
0.360	1.139	-2.212 ⁻¹	1.571 ⁻⁴	-2.305 ⁻⁶	0.893	0.746	-7.915 ⁻²	3.804 ⁻³	9.285 ⁻⁴
0.373	1.115	-2.310 ⁻¹	1.772 ⁻⁴	3.118 ⁻⁵	0.903	0.726	-7.258 ⁻²	3.899 ⁻³	1.069 ⁻³
0.380	1.124	-2.217 ⁻¹	1.279 ⁻⁴	-1.034 ⁻⁶	0.913	0.721	-6.655 ⁻²	3.950 ⁻³	1.044 ⁻³
0.400	1.104	-2.259 ⁻¹	1.654 ⁻⁴	2.363 ⁻⁵	0.920	0.701	-6.367 ⁻²	4.377 ⁻³	1.054 ⁻³
0.420	1.107	-2.122 ⁻¹	1.427 ⁻⁴	1.216 ⁻⁵	0.927	0.692	-5.779 ⁻²	4.297 ⁻³	9.911 ⁻⁴
0.427	1.086	-2.223 ⁻¹	1.750 ⁻⁴	3.371 ⁻⁵	0.933	0.686	-5.451 ⁻²	4.379 ⁻³	1.007 ⁻³
0.440	1.097	-2.107 ⁻¹	2.080 ⁻⁴	2.586 ⁻⁵	0.940	0.661	-5.068 ⁻²	4.804 ⁻³	1.048 ⁻³
0.453	1.074	-2.167 ⁻¹	1.929 ⁻⁴	4.862 ⁻⁵	0.947	0.653	-4.520 ⁻²	4.989 ⁻³	9.966 ⁻⁴
0.460	1.090	-2.024 ⁻¹	1.545 ⁻⁴	1.131 ⁻⁵	0.953	0.646	-4.069 ⁻²	5.228 ⁻³	1.041 ⁻³
0.480	1.066	-2.097 ⁻¹	1.808 ⁻⁴	3.756 ⁻⁵	0.960	0.629	-3.633 ⁻²	5.631 ⁻³	1.062 ⁻³
0.500	1.054	-2.068 ⁻¹	1.846 ⁻⁴	4.186 ⁻⁵	0.967	0.606	-3.187 ⁻²	5.857 ⁻³	1.069 ⁻³
0.520	1.043	-2.012 ⁻¹	2.267 ⁻⁴	7.012 ⁻⁵	0.973	0.575	-2.719 ⁻²	6.847 ⁻³	1.058 ⁻³
0.540	1.030	-2.038 ⁻¹	1.853 ⁻⁴	4.754 ⁻⁵	0.980	0.557	-2.135 ⁻²	7.258 ⁻³	1.212 ⁻³
0.547	1.047	-1.910 ⁻¹	1.947 ⁻⁴	4.038 ⁻⁵					

Table 6. Continued ($\theta = 0$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.040	1.239	-8.900 ⁻²	1.890 ⁻³	-4.272 ⁻⁴	0.480	1.077	-2.191 ⁻¹	3.111 ⁻⁴	1.009 ⁻⁴
0.047	1.245	-1.000 ⁻¹	2.028 ⁻³	-2.193 ⁻⁴	0.500	1.070	-2.152 ⁻¹	2.963 ⁻⁴	1.039 ⁻⁴
0.053	1.241	-1.147 ⁻¹	1.810 ⁻³	-5.328 ⁻⁴	0.520	1.059	-2.080 ⁻¹	2.932 ⁻⁴	9.657 ⁻⁵
0.067	1.253	-1.339 ⁻¹	1.547 ⁻³	-5.476 ⁻⁴	0.540	1.060	-2.058 ⁻¹	2.872 ⁻⁴	9.356 ⁻⁵
0.073	1.266	-1.413 ⁻¹	1.506 ⁻³	-3.769 ⁻⁴	0.560	1.047	-1.995 ⁻¹	4.423 ⁻⁴	1.486 ⁻⁴
0.080	1.250	-1.447 ⁻¹	1.532 ⁻³	-5.081 ⁻⁴	0.580	1.035	-1.969 ⁻¹	6.229 ⁻⁴	2.346 ⁻⁴
0.087	1.246	-1.516 ⁻¹	1.270 ⁻³	-4.773 ⁻⁴	0.600	1.025	-1.865 ⁻¹	3.936 ⁻⁴	1.263 ⁻⁴
0.097	1.243	-1.587 ⁻¹	1.217 ⁻³	-4.219 ⁻⁴	0.640	1.002	-1.826 ⁻¹	1.044 ⁻³	3.071 ⁻⁴
0.107	1.247	-1.666 ⁻¹	1.175 ⁻³	-4.165 ⁻⁴	0.660	0.985	-1.770 ⁻¹	1.409 ⁻³	4.360 ⁻⁴
0.117	1.248	-1.750 ⁻¹	1.062 ⁻³	-3.590 ⁻⁴	0.680	0.962	-1.662 ⁻¹	1.473 ⁻³	4.212 ⁻⁴
0.127	1.262	-1.843 ⁻¹	9.757 ⁻⁴	-3.296 ⁻⁴	0.693	0.961	-1.651 ⁻¹	1.706 ⁻³	4.677 ⁻⁴
0.137	1.239	-1.886 ⁻¹	8.495 ⁻⁴	-2.704 ⁻⁴	0.720	0.939	-1.571 ⁻¹	2.076 ⁻³	5.742 ⁻⁴
0.147	1.247	-1.942 ⁻¹	7.967 ⁻⁴	-2.687 ⁻⁴	0.733	0.928	-1.446 ⁻¹	2.190 ⁻³	5.530 ⁻⁴
0.157	1.244	-2.030 ⁻¹	6.905 ⁻⁴	-2.216 ⁻⁴	0.747	0.917	-1.452 ⁻¹	2.318 ⁻³	5.998 ⁻⁴
0.167	1.248	-2.070 ⁻¹	5.415 ⁻⁴	-1.628 ⁻⁴	0.773	0.912	-1.336 ⁻¹	2.329 ⁻³	6.129 ⁻⁴
0.177	1.230	-2.078 ⁻¹	6.356 ⁻⁴	-1.908 ⁻⁴	0.787	0.879	-1.281 ⁻¹	2.800 ⁻³	6.973 ⁻⁴
0.187	1.240	-2.129 ⁻¹	3.798 ⁻⁴	-7.731 ⁻⁵	0.800	0.873	-1.235 ⁻¹	3.079 ⁻³	7.321 ⁻⁴
0.200	1.236	-2.210 ⁻¹	2.941 ⁻⁴	-5.813 ⁻⁵	0.813	0.856	-1.173 ⁻¹	3.150 ⁻³	7.907 ⁻⁴
0.213	1.227	-2.169 ⁻¹	3.504 ⁻⁴	-7.260 ⁻⁵	0.823	0.840	-1.134 ⁻¹	3.613 ⁻³	9.324 ⁻⁴
0.227	1.227	-2.171 ⁻¹	2.805 ⁻⁴	-5.801 ⁻⁵	0.833	0.827	-1.093 ⁻¹	3.035 ⁻³	7.602 ⁻⁴
0.240	1.225	-2.342 ⁻¹	2.354 ⁻⁴	-1.715 ⁻⁵	0.843	0.821	-1.050 ⁻¹	3.564 ⁻³	8.749 ⁻⁴
0.253	1.195	-2.285 ⁻¹	2.067 ⁻⁴	7.503 ⁻⁶	0.853	0.803	-1.006 ⁻¹	3.520 ⁻³	9.115 ⁻⁴
0.267	1.207	-2.356 ⁻¹	2.036 ⁻⁴	-1.427 ⁻⁶	0.863	0.780	-9.613 ⁻²	3.852 ⁻³	9.738 ⁻⁴
0.280	1.177	-2.286 ⁻¹	1.619 ⁻⁴	-5.927 ⁻⁶	0.873	0.781	-8.945 ⁻²	3.763 ⁻³	9.140 ⁻⁴
0.293	1.189	-2.402 ⁻¹	2.057 ⁻⁴	1.266 ⁻⁶	0.883	0.769	-8.448 ⁻²	3.793 ⁻³	8.724 ⁻⁴
0.307	1.160	-2.295 ⁻¹	1.721 ⁻⁴	1.354 ⁻⁶	0.893	0.739	-7.871 ⁻²	3.966 ⁻³	9.448 ⁻⁴
0.320	1.171	-2.393 ⁻¹	1.740 ⁻⁴	1.830 ⁻⁶	0.903	0.715	-7.539 ⁻²	4.227 ⁻³	8.590 ⁻⁴
0.340	1.139	-2.253 ⁻¹	1.667 ⁻⁴	-7.001 ⁻⁶	0.913	0.698	-7.010 ⁻²	4.473 ⁻³	8.502 ⁻⁴
0.347	1.159	-2.450 ⁻¹	2.816 ⁻⁴	7.893 ⁻⁶	0.920	0.685	-6.492 ⁻²	4.775 ⁻³	8.556 ⁻⁴
0.360	1.126	-2.251 ⁻¹	1.439 ⁻⁴	1.510 ⁻⁶	0.927	0.696	-6.063 ⁻²	4.730 ⁻³	9.434 ⁻⁴
0.373	1.144	-2.436 ⁻¹	2.719 ⁻⁴	7.219 ⁻⁶	0.933	0.674	-5.662 ⁻²	5.169 ⁻³	9.253 ⁻⁴
0.380	1.115	-2.282 ⁻¹	1.978 ⁻⁴	2.289 ⁻⁶	0.947	0.647	-4.773 ⁻²	5.815 ⁻³	9.443 ⁻⁴
0.400	1.121	-2.321 ⁻¹	2.248 ⁻⁴	5.674 ⁻⁶	0.953	0.625	-4.240 ⁻²	6.625 ⁻³	1.032 ⁻³
0.420	1.100	-2.123 ⁻¹	1.473 ⁻⁴	-5.364 ⁻⁶	0.960	0.590	-3.900 ⁻²	6.977 ⁻³	9.174 ⁻⁴
0.427	1.118	-2.299 ⁻¹	1.948 ⁻⁴	4.772 ⁻⁶	0.967	0.593	-3.303 ⁻²	6.364 ⁻³	9.304 ⁻⁴
0.440	1.077	-2.211 ⁻¹	3.151 ⁻⁴	7.427 ⁻⁶	0.973	0.546	-2.657 ⁻²	7.097 ⁻³	8.618 ⁻⁴
0.453	1.102	-2.276 ⁻¹	2.693 ⁻⁴	8.636 ⁻⁶	0.980	0.529	-2.083 ⁻²	7.355 ⁻³	7.955 ⁻⁴
0.460	1.074	-2.113 ⁻¹	1.644 ⁻⁴	-1.709 ⁻⁷					

Table 6. Continued ($\theta = 0$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.040	1.252	-1.107 ⁻¹	2.732 ⁻³	-2.364 ⁻⁴	0.660	0.964	-1.682 ⁻¹	8.099 ⁻⁴	3.062 ⁻⁴
0.087	1.252	-1.744 ⁻¹	1.627 ⁻³	-4.376 ⁻⁴	0.680	0.944	-1.642 ⁻¹	1.062 ⁻³	2.952 ⁻⁴
0.097	1.259	-1.820 ⁻¹	1.471 ⁻³	-4.265 ⁻⁴	0.693	0.925	-1.518 ⁻¹	1.634 ⁻³	4.406 ⁻⁴
0.107	1.259	-1.869 ⁻¹	1.158 ⁻³	-3.026 ⁻⁴	0.707	0.925	-1.532 ⁻¹	1.466 ⁻³	3.938 ⁻⁴
0.117	1.260	-1.947 ⁻¹	1.196 ⁻³	-3.327 ⁻⁴	0.720	0.934	-1.437 ⁻¹	1.229 ⁻³	2.801 ⁻⁴
0.127	1.243	-1.988 ⁻¹	1.398 ⁻³	-4.056 ⁻⁴	0.733	0.922	-1.414 ⁻¹	1.533 ⁻³	3.667 ⁻⁴
0.137	1.265	-2.079 ⁻¹	9.304 ⁻⁴	-2.521 ⁻⁴	0.747	0.914	-1.346 ⁻¹	1.690 ⁻³	4.213 ⁻⁴
0.147	1.266	-2.096 ⁻¹	7.744 ⁻⁴	-1.779 ⁻⁴	0.760	0.896	-1.314 ⁻¹	2.156 ⁻³	5.359 ⁻⁴
0.157	1.239	-2.190 ⁻¹	7.072 ⁻⁴	-1.573 ⁻⁴	0.773	0.893	-1.256 ⁻¹	2.261 ⁻³	5.026 ⁻⁴
0.167	1.242	-2.214 ⁻¹	6.642 ⁻⁴	-1.177 ⁻⁴	0.787	0.890	-1.201 ⁻¹	2.060 ⁻³	4.099 ⁻⁴
0.177	1.237	-2.235 ⁻¹	6.097 ⁻⁴	-1.389 ⁻⁴	0.800	0.858	-1.153 ⁻¹	2.739 ⁻³	5.622 ⁻⁴
0.187	1.234	-2.271 ⁻¹	4.611 ⁻⁴	-3.201 ⁻⁵	0.813	0.842	-1.110 ⁻¹	3.053 ⁻³	6.173 ⁻⁴
0.200	1.230	-2.302 ⁻¹	3.383 ⁻⁴	-1.122 ⁻⁵	0.823	0.860	-1.038 ⁻¹	2.594 ⁻³	5.836 ⁻⁴
0.293	1.162	-2.307 ⁻¹	2.494 ⁻⁴	6.310 ⁻⁵	0.833	0.833	-9.914 ⁻²	3.427 ⁻³	6.567 ⁻⁴
0.320	1.139	-2.359 ⁻¹	2.613 ⁻⁴	6.215 ⁻⁵	0.843	0.810	-9.697 ⁻²	3.675 ⁻³	7.842 ⁻⁴
0.340	1.135	-2.336 ⁻¹	2.295 ⁻⁴	5.942 ⁻⁵	0.853	0.815	-8.973 ⁻²	3.302 ⁻³	7.319 ⁻⁴
0.347	1.123	-2.298 ⁻¹	1.950 ⁻⁴	4.160 ⁻⁵	0.863	0.804	-8.548 ⁻²	3.566 ⁻³	7.741 ⁻⁴
0.373	1.105	-2.246 ⁻¹	2.322 ⁻⁴	6.523 ⁻⁵	0.873	0.774	-8.203 ⁻²	4.159 ⁻³	1.028 ⁻³
0.400	1.087	-2.257 ⁻¹	3.838 ⁻⁴	1.146 ⁻⁴	0.883	0.779	-7.565 ⁻²	3.848 ⁻³	8.419 ⁻⁴
0.420	1.086	-2.177 ⁻¹	2.913 ⁻⁴	1.164 ⁻⁴	0.893	0.766	-7.121 ⁻²	3.734 ⁻³	9.659 ⁻⁴
0.427	1.077	-2.163 ⁻¹	2.435 ⁻⁴	8.025 ⁻⁵	0.903	0.726	-6.661 ⁻²	4.285 ⁻³	1.114 ⁻³
0.453	1.062	-2.123 ⁻¹	2.768 ⁻⁴	9.313 ⁻⁵	0.913	0.712	-6.357 ⁻²	4.907 ⁻³	1.147 ⁻³
0.480	1.043	-2.120 ⁻¹	5.372 ⁻⁴	1.463 ⁻⁴	0.920	0.702	-5.717 ⁻²	4.652 ⁻³	1.055 ⁻³
0.500	1.041	-2.059 ⁻¹	3.793 ⁻⁴	1.444 ⁻⁴	0.927	0.692	-5.531 ⁻²	5.079 ⁻³	1.130 ⁻³
0.520	1.033	-1.993 ⁻¹	3.147 ⁻⁴	9.943 ⁻⁵	0.933	0.676	-5.210 ⁻²	5.207 ⁻³	1.216 ⁻³
0.540	1.021	-1.961 ⁻¹	3.226 ⁻⁴	1.104 ⁻⁴	0.940	0.661	-4.908 ⁻²	4.819 ⁻³	1.189 ⁻³
0.547	1.029	-1.914 ⁻¹	4.414 ⁻⁴	1.891 ⁻⁴	0.947	0.631	-4.566 ⁻²	5.445 ⁻³	1.079 ⁻³
0.560	1.012	-1.926 ⁻¹	3.361 ⁻⁴	1.211 ⁻⁴	0.953	0.643	-4.156 ⁻²	5.685 ⁻³	1.271 ⁻³
0.580	1.004	-1.845 ⁻¹	4.250 ⁻⁴	1.412 ⁻⁴	0.960	0.609	-3.579 ⁻²	6.499 ⁻³	1.323 ⁻³
0.620	0.982	-1.767 ⁻¹	6.317 ⁻⁴	2.153 ⁻⁴	0.967	0.588	-3.308 ⁻²	6.272 ⁻³	1.347 ⁻³
0.640	0.979	-1.710 ⁻¹	5.102 ⁻⁴	1.762 ⁻⁴	0.973	0.561	-2.979 ⁻²	6.577 ⁻³	1.221 ⁻³
0.653	0.981	-1.627 ⁻¹	6.560 ⁻⁴	2.311 ⁻⁴	0.980	0.562	-3.017 ⁻²	6.747 ⁻³	1.376 ⁻³

Table 6. Concluded ($\theta = 0$ deg)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.033	1.260	-1.033 ⁻¹	1.766 ⁻³	-1.968 ⁻⁴	0.440	1.075	-2.248 ⁻¹	2.025 ⁻⁴	6.188 ⁻⁵
0.040	1.261	-1.179 ⁻¹	1.345 ⁻³	-4.567 ⁻⁴	0.547	1.021	-2.049 ⁻¹	3.630 ⁻⁴	1.319 ⁻⁴
0.047	1.269	-1.215 ⁻¹	1.786 ⁻³	-2.271 ⁻⁴	0.573	1.011	-2.022 ⁻¹	4.960 ⁻⁴	2.008 ⁻⁴
0.053	1.269	-1.322 ⁻¹	1.501 ⁻³	-4.429 ⁻⁴	0.660	0.990	-1.763 ⁻¹	7.616 ⁻⁴	3.136 ⁻⁴
0.060	1.270	-1.444 ⁻¹	1.489 ⁻³	-4.597 ⁻⁴	0.693	0.959	-1.666 ⁻¹	1.084 ⁻³	3.032 ⁻⁴
0.067	1.281	-1.578 ⁻¹	1.341 ⁻³	-4.748 ⁻⁴	0.707	0.958	-1.612 ⁻¹	9.991 ⁻⁴	2.459 ⁻⁴
0.073	1.283	-1.628 ⁻¹	1.327 ⁻³	-4.886 ⁻⁴	0.720	0.949	-1.555 ⁻¹	9.803 ⁻⁴	2.503 ⁻⁴
0.080	1.272	-1.687 ⁻¹	1.227 ⁻³	-3.767 ⁻⁴	0.733	0.933	-1.513 ⁻¹	1.479 ⁻³	3.644 ⁻⁴
0.087	1.272	-1.762 ⁻¹	1.257 ⁻³	-3.886 ⁻⁴	0.747	0.938	-1.450 ⁻¹	1.469 ⁻³	3.752 ⁻⁴
0.097	1.267	-1.858 ⁻¹	1.306 ⁻³	-3.379 ⁻⁴	0.760	0.907	-1.392 ⁻¹	1.705 ⁻³	3.408 ⁻⁴
0.107	1.273	-1.943 ⁻¹	1.137 ⁻³	-3.080 ⁻⁴	0.773	0.891	-1.333 ⁻¹	1.777 ⁻³	3.987 ⁻⁴
0.117	1.272	-1.985 ⁻¹	9.428 ⁻⁴	-2.383 ⁻⁴	0.787	0.873	-1.246 ⁻¹	2.157 ⁻³	5.442 ⁻⁴
0.127	1.247	-2.005 ⁻¹	1.109 ⁻³	-3.055 ⁻⁴	0.800	0.841	-1.192 ⁻¹	2.945 ⁻³	7.629 ⁻⁴
0.137	1.260	-2.090 ⁻¹	8.099 ⁻⁴	-1.164 ⁻⁴	0.813	0.847	-1.139 ⁻¹	2.749 ⁻³	7.431 ⁻⁴
0.147	1.265	-2.154 ⁻¹	7.377 ⁻⁴	-1.264 ⁻⁴	0.823	0.836	-1.088 ⁻¹	2.998 ⁻³	7.601 ⁻⁴
0.157	1.267	-2.210 ⁻¹	5.308 ⁻⁴	-9.303 ⁻⁵	0.833	0.810	-1.039 ⁻¹	2.855 ⁻³	8.665 ⁻⁴
0.167	1.248	-2.244 ⁻¹	6.655 ⁻⁴	-1.477 ⁻⁴	0.843	0.798	-9.893 ⁻²	3.158 ⁻³	9.312 ⁻⁴
0.177	1.254	-2.290 ⁻¹	5.076 ⁻⁴	-4.011 ⁻⁵	0.853	0.804	-9.171 ⁻²	3.486 ⁻³	9.737 ⁻⁴
0.187	1.243	-2.323 ⁻¹	4.332 ⁻⁴	-8.034 ⁻⁵	0.863	0.778	-8.809 ⁻²	3.499 ⁻³	8.866 ⁻⁴
0.200	1.238	-2.369 ⁻¹	2.339 ⁻⁴	-2.958 ⁻⁵	0.873	0.750	-8.314 ⁻²	3.698 ⁻³	1.019 ⁻³
0.213	1.231	-2.352 ⁻¹	3.267 ⁻⁴	-3.763 ⁻⁵	0.883	0.737	-7.707 ⁻²	3.795 ⁻³	9.805 ⁻⁴
0.227	1.201	-2.484 ⁻¹	3.518 ⁻⁴	-6.042 ⁻⁵	0.893	0.732	-7.231 ⁻²	3.299 ⁻³	9.785 ⁻⁴
0.240	1.199	-2.466 ⁻¹	2.335 ⁻⁴	-1.545 ⁻⁵	0.903	0.724	-6.636 ⁻²	4.005 ⁻³	1.217 ⁻³
0.253	1.194	-2.447 ⁻¹	2.135 ⁻⁴	-3.720 ⁻⁵	0.913	0.692	-6.216 ⁻²	4.244 ⁻³	1.245 ⁻³
0.267	1.185	-2.437 ⁻¹	1.713 ⁻⁴	-1.340 ⁻⁵	0.920	0.665	-6.035 ⁻²	4.041 ⁻³	1.164 ⁻³
0.280	1.170	-2.419 ⁻¹	2.796 ⁻⁴	-2.068 ⁻⁵	0.927	0.661	-5.391 ⁻²	4.365 ⁻³	1.025 ⁻³
0.293	1.168	-2.393 ⁻¹	1.878 ⁻⁴	-7.531 ⁻⁶	0.933	0.662	-5.053 ⁻²	4.516 ⁻³	1.116 ⁻³
0.307	1.155	-2.428 ⁻¹	1.731 ⁻⁴	-1.723 ⁻⁵	0.940	0.638	-4.525 ⁻²	4.786 ⁻³	1.058 ⁻³
0.340	1.134	-2.428 ⁻¹	1.436 ⁻⁴	1.785 ⁻⁶	0.947	0.607	-4.117 ⁻²	4.778 ⁻³	8.195 ⁻⁴
0.360	1.126	-2.366 ⁻¹	2.049 ⁻⁴	4.812 ⁻⁵	0.953	0.586	-4.004 ⁻²	4.736 ⁻³	1.096 ⁻³
0.380	1.112	-2.317 ⁻¹	1.736 ⁻⁴	3.390 ⁻⁵	0.960	0.522	-3.551 ⁻²	5.054 ⁻³	8.267 ⁻⁴
0.420	1.086	-2.290 ⁻¹	1.362 ⁻⁴	1.071 ⁻⁵	0.973	0.492	-2.196 ⁻²	5.788 ⁻³	8.513 ⁻⁴

Legend: $Re=1 \times 10^5$; $z/H=0$ (\odot); $Re=1 \times 10^6$; $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)

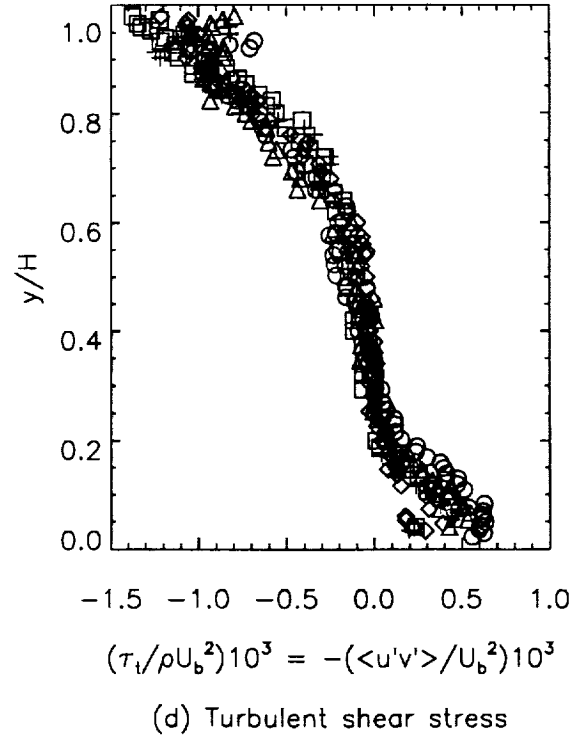
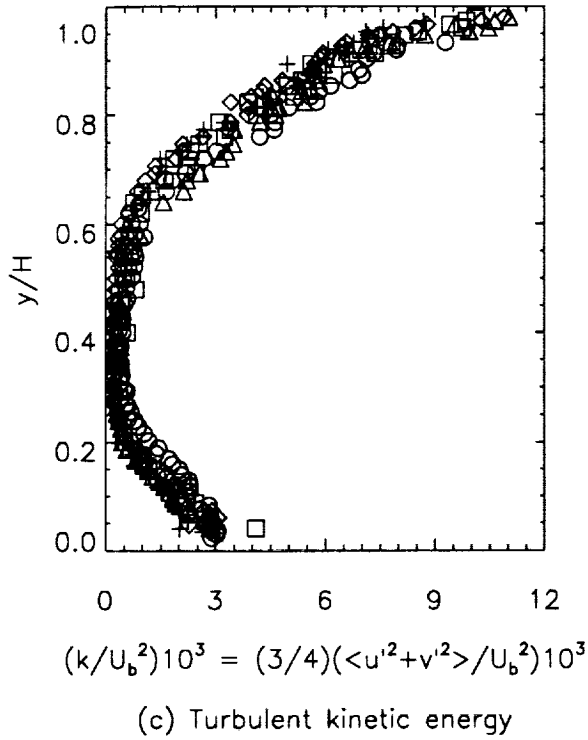
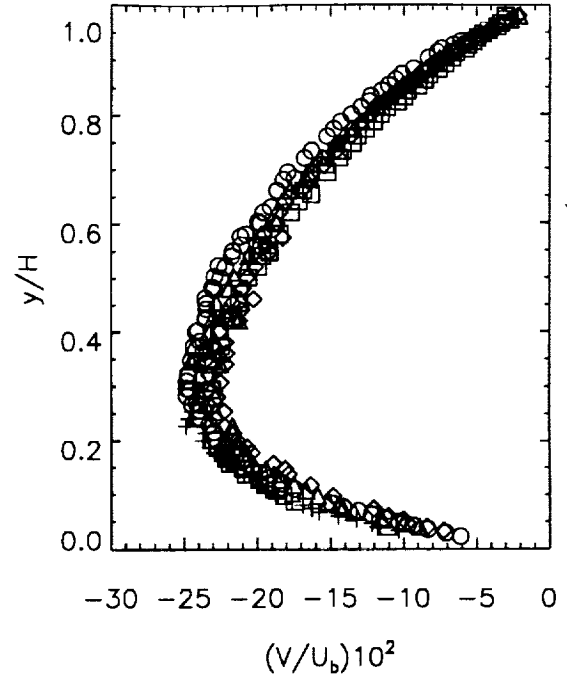
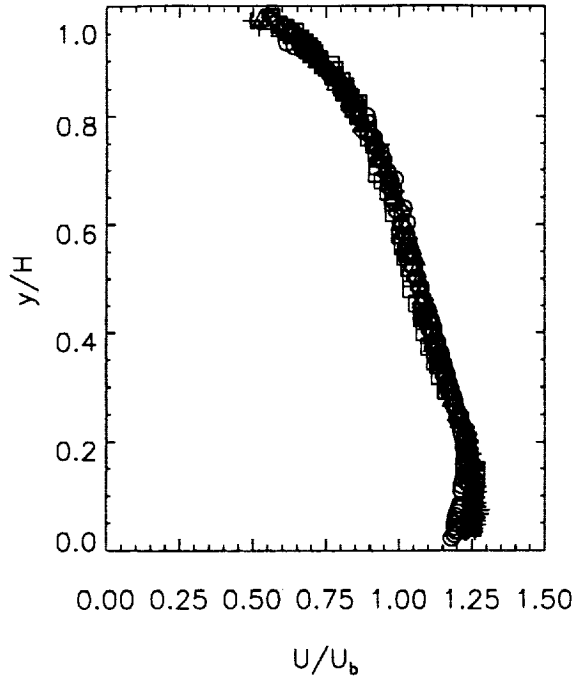


Figure 6. Summary of Table 6 ($\theta = 0$ deg).

Table 7. LDV flowfield data in TAD ($\theta = 30$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

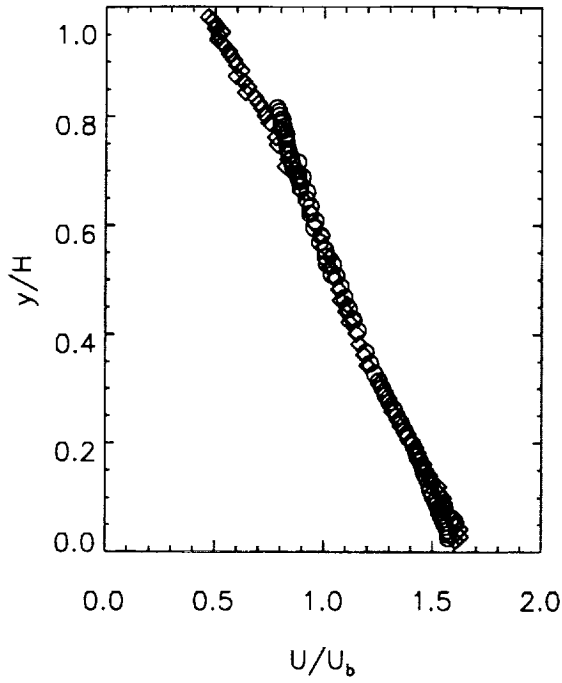
y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.025	1.572	9.592 ⁻²	2.532 ⁻³	1.447 ⁻⁵	0.467	1.095	-2.927 ⁻²	2.882 ⁻⁴	5.782 ⁻⁵
0.032	1.573	8.771 ⁻²	2.402 ⁻³	-3.451 ⁻⁵	0.487	1.078	-2.534 ⁻²	3.767 ⁻⁴	1.245 ⁻⁴
0.039	1.569	7.500 ⁻²	2.293 ⁻³	-4.273 ⁻⁶	0.507	1.056	-2.511 ⁻²	6.792 ⁻⁴	3.180 ⁻⁴
0.046	1.562	6.764 ⁻²	2.228 ⁻³	8.044 ⁻⁵	0.510	1.034	-3.200 ⁻²	8.535 ⁻⁴	2.157 ⁻⁴
0.053	1.553	5.585 ⁻²	2.048 ⁻³	4.464 ⁻⁵	0.527	1.042	-2.368 ⁻²	4.309 ⁻⁴	1.852 ⁻⁴
0.060	1.546	5.496 ⁻²	2.140 ⁻³	7.203 ⁻⁵	0.530	1.011	-3.010 ⁻²	1.226 ⁻³	4.468 ⁻⁴
0.066	1.538	4.617 ⁻²	1.921 ⁻³	4.174 ⁻⁵	0.543	1.006	-2.362 ⁻²	1.085 ⁻³	3.480 ⁻⁴
0.073	1.530	4.216 ⁻²	1.811 ⁻³	6.301 ⁻⁵	0.555	1.005	-2.615 ⁻²	7.701 ⁻⁴	2.805 ⁻⁴
0.080	1.526	3.130 ⁻²	1.783 ⁻³	8.128 ⁻⁵	0.569	0.980	-2.529 ⁻²	1.553 ⁻³	5.442 ⁻⁴
0.087	1.519	3.307 ⁻²	1.641 ⁻³	1.517 ⁻⁴	0.582	0.986	-1.505 ⁻²	8.512 ⁻⁴	2.540 ⁻⁴
0.094	1.513	2.448 ⁻²	1.560 ⁻³	8.695 ⁻⁵	0.596	0.954	-2.003 ⁻²	1.546 ⁻³	6.461 ⁻⁴
0.104	1.499	1.734 ⁻²	1.454 ⁻³	8.118 ⁻⁵	0.608	0.961	-7.839 ⁻³	1.406 ⁻³	6.559 ⁻⁴
0.114	1.489	1.101 ⁻²	1.313 ⁻³	1.238 ⁻⁴	0.622	0.934	-1.088 ⁻²	1.750 ⁻³	7.636 ⁻⁴
0.124	1.483	8.702 ⁻³	1.135 ⁻³	1.325 ⁻⁴	0.635	0.938	-7.521 ⁻³	1.502 ⁻³	6.565 ⁻⁴
0.135	1.474	3.842 ⁻⁴	1.053 ⁻³	1.348 ⁻⁴	0.648	0.918	-4.600 ⁻⁵	2.171 ⁻³	8.565 ⁻⁴
0.145	1.460	-3.304 ⁻³	1.069 ⁻³	1.803 ⁻⁴	0.662	0.922	-2.061 ⁻³	1.552 ⁻³	6.086 ⁻⁴
0.155	1.453	-1.071 ⁻³	9.876 ⁻⁴	1.595 ⁻⁴	0.671	0.890	2.636 ⁻³	2.564 ⁻³	1.103 ⁻³
0.165	1.444	-6.916 ⁻³	7.323 ⁻⁴	8.359 ⁻⁵	0.681	0.884	5.926 ⁻³	2.635 ⁻³	1.146 ⁻³
0.175	1.428	-1.071 ⁻²	7.003 ⁻⁴	1.264 ⁻⁴	0.689	0.902	8.512 ⁻³	2.267 ⁻³	1.037 ⁻³
0.185	1.422	-1.264 ⁻²	5.755 ⁻⁴	7.930 ⁻⁵	0.691	0.880	6.810 ⁻³	2.850 ⁻³	1.197 ⁻³
0.196	1.410	-1.533 ⁻²	5.285 ⁻⁴	7.731 ⁻⁵	0.701	0.867	1.625 ⁻²	3.137 ⁻³	1.359 ⁻³
0.209	1.389	-1.765 ⁻²	5.283 ⁻⁴	1.135 ⁻⁴	0.711	0.852	1.442 ⁻²	3.466 ⁻³	1.508 ⁻³
0.222	1.372	-1.779 ⁻²	4.424 ⁻⁴	8.202 ⁻⁵	0.716	0.881	1.448 ⁻²	2.724 ⁻³	1.130 ⁻³
0.235	1.356	-2.164 ⁻²	3.617 ⁻⁴	6.143 ⁻⁵	0.720	0.849	2.672 ⁻²	3.899 ⁻³	1.544 ⁻³
0.248	1.336	-2.424 ⁻²	3.823 ⁻⁴	7.419 ⁻⁵	0.730	0.840	2.020 ⁻²	3.453 ⁻³	1.355 ⁻³
0.261	1.322	-2.432 ⁻²	3.157 ⁻⁴	4.882 ⁻⁵	0.740	0.833	2.632 ⁻²	3.470 ⁻³	1.338 ⁻³
0.275	1.301	-2.621 ⁻²	3.559 ⁻⁴	8.909 ⁻⁵	0.750	0.828	2.725 ⁻²	3.044 ⁻³	1.142 ⁻³
0.288	1.283	-2.556 ⁻²	2.656 ⁻⁴	4.366 ⁻⁵	0.760	0.823	4.058 ⁻²	3.931 ⁻³	1.436 ⁻³
0.301	1.268	-2.849 ⁻²	2.627 ⁻⁴	4.692 ⁻⁵	0.767	0.825	4.895 ⁻²	5.465 ⁻³	1.630 ⁻³
0.314	1.252	-3.095 ⁻²	2.918 ⁻⁴	7.090 ⁻⁵	0.774	0.808	5.255 ⁻²	6.134 ⁻³	1.819 ⁻³
0.327	1.234	-3.364 ⁻²	2.439 ⁻⁴	5.929 ⁻⁵	0.780	0.814	4.507 ⁻²	4.807 ⁻³	1.224 ⁻³
0.347	1.213	-3.482 ⁻²	2.477 ⁻⁴	5.528 ⁻⁵	0.787	0.802	5.462 ⁻²	5.424 ⁻³	1.458 ⁻³
0.367	1.193	-3.471 ⁻²	3.173 ⁻⁴	7.190 ⁻⁵	0.794	0.806	5.668 ⁻²	5.331 ⁻³	1.348 ⁻³
0.407	1.155	-2.847 ⁻²	2.763 ⁻⁴	6.096 ⁻⁵	0.801	0.795	5.239 ⁻²	5.644 ⁻³	1.467 ⁻³
0.427	1.135	-2.539 ⁻²	2.757 ⁻⁴	6.101 ⁻⁵	0.808	0.793	5.053 ⁻²	5.322 ⁻³	1.418 ⁻³
0.447	1.115	-2.609 ⁻²	4.314 ⁻⁴	1.659 ⁻⁴	0.815	0.784	6.554 ⁻²	7.055 ⁻³	1.684 ⁻³

Table 7. Concluded ($\theta = 30$ deg)

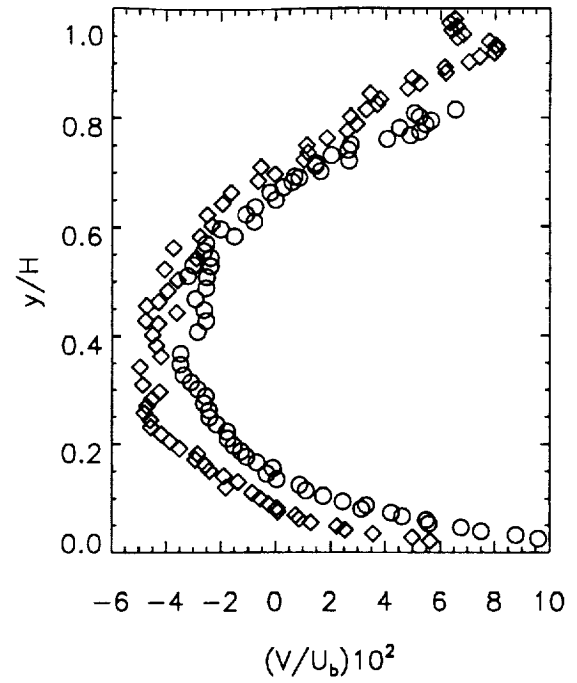
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.021	1.607	5.631^{-2}	2.963^{-3}	3.809^{-4}	0.502	1.048	-3.575^{-2}	1.342^{-3}	8.159^{-4}
0.027	1.628	4.982^{-2}	3.238^{-3}	4.183^{-4}	0.523	1.026	-4.052^{-2}	1.585^{-3}	1.028^{-3}
0.034	1.612	3.552^{-2}	2.085^{-3}	-7.559^{-5}	0.542	1.027	-2.889^{-2}	9.789^{-4}	5.360^{-4}
0.041	1.627	2.530^{-2}	2.315^{-3}	-4.582^{-5}	0.562	1.000	-3.724^{-2}	1.250^{-3}	7.831^{-4}
0.048	1.610	2.234^{-2}	2.184^{-3}	1.269^{-4}	0.582	0.990	-2.751^{-2}	1.034^{-3}	5.556^{-4}
0.055	1.608	1.281^{-2}	2.116^{-3}	7.059^{-5}	0.603	0.954	-2.318^{-2}	2.098^{-3}	1.321^{-3}
0.062	1.602	8.597^{-3}	2.103^{-3}	9.071^{-5}	0.622	0.941	-2.494^{-2}	1.490^{-3}	7.852^{-4}
0.069	1.581	7.321^{-3}	1.904^{-3}	3.141^{-5}	0.642	0.918	-1.935^{-2}	1.987^{-3}	1.086^{-3}
0.076	1.553	7.211^{-4}	1.819^{-3}	1.224^{-4}	0.662	0.892	-1.622^{-2}	2.270^{-3}	1.250^{-3}
0.082	1.558	3.920^{-4}	1.711^{-3}	6.597^{-5}	0.683	0.878	-6.412^{-3}	3.984^{-3}	2.431^{-3}
0.089	1.556	-2.524^{-3}	1.857^{-3}	2.102^{-5}	0.696	0.857	-3.248^{-4}	3.966^{-3}	2.034^{-3}
0.099	1.549	-5.703^{-3}	1.698^{-3}	-1.004^{-5}	0.709	0.822	-5.411^{-3}	4.448^{-3}	2.387^{-3}
0.110	1.527	-8.536^{-3}	1.501^{-3}	9.342^{-5}	0.722	0.833	1.024^{-2}	5.317^{-3}	2.838^{-3}
0.120	1.527	-1.815^{-2}	1.578^{-3}	1.432^{-4}	0.735	0.827	1.166^{-2}	4.807^{-3}	2.442^{-3}
0.130	1.498	-1.373^{-2}	1.232^{-3}	1.052^{-4}	0.748	0.784	1.120^{-2}	5.543^{-3}	2.544^{-3}
0.140	1.486	-1.895^{-2}	1.072^{-3}	3.359^{-5}	0.761	0.777	1.857^{-2}	5.036^{-3}	2.514^{-3}
0.150	1.468	-2.417^{-2}	1.055^{-3}	8.522^{-5}	0.774	0.796	2.594^{-2}	5.485^{-3}	2.408^{-3}
0.160	1.458	-2.572^{-2}	8.883^{-4}	2.526^{-5}	0.788	0.748	2.937^{-2}	6.095^{-3}	2.598^{-3}
0.171	1.436	-2.933^{-2}	1.056^{-3}	8.461^{-5}	0.801	0.728	2.718^{-2}	5.585^{-3}	2.564^{-3}
0.181	1.433	-2.853^{-2}	1.027^{-3}	3.585^{-5}	0.814	0.713	3.290^{-2}	7.045^{-3}	3.097^{-3}
0.191	1.417	-3.515^{-2}	6.555^{-4}	1.295^{-5}	0.824	0.699	3.697^{-2}	6.177^{-3}	2.737^{-3}
0.204	1.400	-3.867^{-2}	5.406^{-4}	9.911^{-5}	0.834	0.682	3.789^{-2}	8.152^{-3}	3.413^{-3}
0.217	1.376	-4.177^{-2}	6.975^{-4}	7.930^{-5}	0.843	0.639	3.428^{-2}	7.538^{-3}	2.916^{-3}
0.230	1.353	-4.559^{-2}	6.373^{-4}	3.799^{-5}	0.853	0.648	4.804^{-2}	7.988^{-3}	3.134^{-3}
0.244	1.342	-4.584^{-2}	5.344^{-4}	4.294^{-5}	0.863	0.630	5.236^{-2}	9.047^{-3}	3.773^{-3}
0.257	1.315	-4.800^{-2}	7.145^{-4}	9.660^{-5}	0.873	0.596	4.964^{-2}	1.021^{-2}	4.745^{-3}
0.270	1.304	-4.709^{-2}	5.259^{-4}	1.185^{-4}	0.883	0.618	6.192^{-2}	1.089^{-2}	4.709^{-3}
0.283	1.285	-4.511^{-2}	5.991^{-4}	8.514^{-5}	0.893	0.597	6.161^{-2}	9.108^{-3}	3.754^{-3}
0.296	1.270	-4.243^{-2}	4.834^{-4}	9.371^{-5}	0.903	0.586	7.050^{-2}	1.200^{-2}	4.984^{-3}
0.309	1.252	-4.858^{-2}	4.102^{-4}	1.009^{-4}	0.912	0.566	7.438^{-2}	1.313^{-2}	5.552^{-3}
0.343	1.199	-4.957^{-2}	8.675^{-4}	3.572^{-4}	0.919	0.560	7.969^{-2}	1.413^{-2}	6.067^{-3}
0.363	1.185	-4.192^{-2}	6.516^{-4}	2.027^{-4}	0.926	0.545	8.079^{-2}	1.333^{-2}	5.641^{-3}
0.383	1.161	-4.364^{-2}	1.031^{-3}	5.429^{-4}	0.933	0.531	8.036^{-2}	1.341^{-2}	5.386^{-3}
0.402	1.149	-4.497^{-2}	1.174^{-3}	4.611^{-4}	0.940	0.510	7.787^{-2}	1.484^{-2}	5.730^{-3}
0.423	1.116	-4.288^{-2}	1.094^{-3}	6.770^{-4}	0.947	0.517	6.616^{-2}	1.187^{-2}	4.215^{-3}
0.428	1.136	-4.745^{-2}	8.840^{-4}	2.478^{-4}	0.954	0.530	6.832^{-2}	1.214^{-2}	4.215^{-3}
0.443	1.100	-3.615^{-2}	7.105^{-4}	3.445^{-4}	0.960	0.499	6.407^{-2}	1.217^{-2}	3.595^{-3}
0.455	1.107	-4.712^{-2}	6.168^{-4}	2.335^{-4}	0.967	0.501	6.615^{-2}	1.048^{-2}	3.545^{-3}
0.463	1.075	-4.274^{-2}	1.202^{-3}	7.452^{-4}	0.974	0.488	6.329^{-2}	1.073^{-2}	3.555^{-3}
0.482	1.068	-3.941^{-2}	1.362^{-3}	8.126^{-4}	0.981	0.468	6.523^{-2}	1.170^{-2}	3.849^{-3}

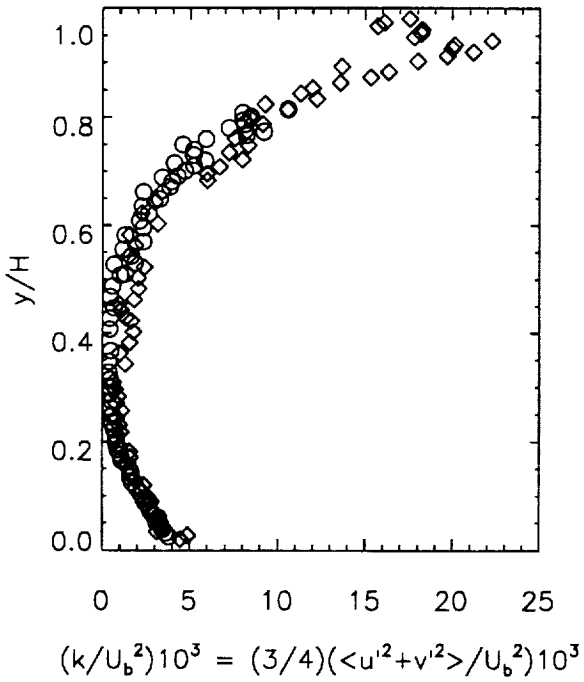
Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)



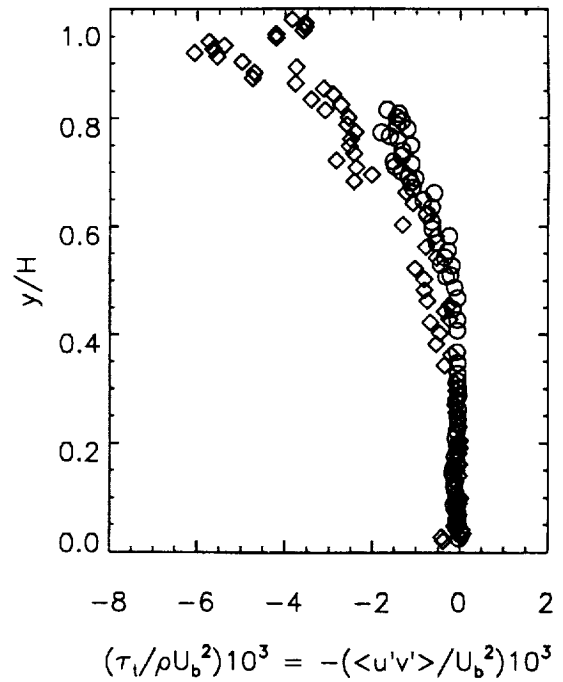
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 7. Summary of Table 7 ($\theta = 30$ deg).

Table 8. LDV flowfield data in TAD ($\theta = 60$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.026	1.699	1.137 ⁻¹	2.156 ⁻³	3.073 ⁻⁴	0.485	1.059	5.392 ⁻²	1.370 ⁻³	4.918 ⁻⁴
0.033	1.700	1.164 ⁻¹	2.015 ⁻³	4.441 ⁻⁴	0.505	1.038	5.631 ⁻²	1.979 ⁻³	7.672 ⁻⁴
0.040	1.690	1.219 ⁻¹	2.028 ⁻³	4.344 ⁻⁴	0.525	1.007	6.036 ⁻²	3.352 ⁻³	1.788 ⁻³
0.047	1.677	1.180 ⁻¹	2.115 ⁻³	5.357 ⁻⁴	0.552	0.986	6.139 ⁻²	2.790 ⁻³	1.201 ⁻³
0.053	1.668	1.079 ⁻¹	2.015 ⁻³	4.767 ⁻⁴	0.579	0.942	6.154 ⁻²	3.683 ⁻³	1.686 ⁻³
0.060	1.657	9.822 ⁻²	2.041 ⁻³	5.682 ⁻⁴	0.599	0.904	6.302 ⁻²	4.831 ⁻³	2.076 ⁻³
0.067	1.651	9.940 ⁻²	2.025 ⁻³	4.865 ⁻⁴	0.606	0.929	6.249 ⁻²	4.394 ⁻³	2.230 ⁻³
0.074	1.636	1.021 ⁻¹	2.113 ⁻³	4.899 ⁻⁴	0.613	0.891	5.886 ⁻²	4.999 ⁻³	2.272 ⁻³
0.081	1.625	9.891 ⁻²	2.175 ⁻³	5.031 ⁻⁴	0.626	0.879	6.452 ⁻²	5.560 ⁻³	2.428 ⁻³
0.088	1.618	9.439 ⁻²	1.928 ⁻³	5.446 ⁻⁴	0.632	0.912	7.426 ⁻²	4.235 ⁻³	1.820 ⁻³
0.095	1.606	9.162 ⁻²	1.794 ⁻³	5.562 ⁻⁴	0.652	0.858	7.143 ⁻²	6.279 ⁻³	3.200 ⁻³
0.104	1.586	9.002 ⁻²	1.765 ⁻³	5.699 ⁻⁴	0.659	0.884	7.033 ⁻²	4.823 ⁻³	2.209 ⁻³
0.114	1.573	8.583 ⁻²	1.709 ⁻³	5.007 ⁻⁴	0.665	0.854	6.691 ⁻²	5.928 ⁻³	2.742 ⁻³
0.124	1.561	8.274 ⁻²	1.473 ⁻³	4.394 ⁻⁴	0.678	0.841	7.824 ⁻²	5.992 ⁻³	2.583 ⁻³
0.134	1.542	7.705 ⁻²	1.518 ⁻³	4.201 ⁻⁴	0.686	0.856	8.191 ⁻²	6.588 ⁻³	3.618 ⁻³
0.144	1.530	7.605 ⁻²	1.337 ⁻³	3.785 ⁻⁴	0.692	0.825	8.288 ⁻²	6.665 ⁻³	3.117 ⁻³
0.154	1.515	7.575 ⁻²	1.142 ⁻³	3.331 ⁻⁴	0.705	0.821	8.180 ⁻²	6.418 ⁻³	2.881 ⁻³
0.164	1.497	7.190 ⁻²	1.242 ⁻³	3.408 ⁻⁴	0.713	0.835	9.442 ⁻²	7.796 ⁻³	4.333 ⁻³
0.173	1.484	6.514 ⁻²	9.882 ⁻⁴	2.841 ⁻⁴	0.718	0.808	8.157 ⁻²	6.676 ⁻³	3.019 ⁻³
0.183	1.471	6.696 ⁻²	9.471 ⁻⁴	2.575 ⁻⁴	0.731	0.787	7.885 ⁻²	8.548 ⁻³	4.555 ⁻³
0.193	1.457	5.963 ⁻²	8.094 ⁻⁴	2.206 ⁻⁴	0.740	0.789	9.465 ⁻²	9.839 ⁻³	5.140 ⁻³
0.206	1.436	6.406 ⁻²	8.723 ⁻⁴	1.222 ⁻⁴	0.761	0.758	8.536 ⁻²	1.050 ⁻²	5.638 ⁻³
0.219	1.417	5.897 ⁻²	7.025 ⁻⁴	6.347 ⁻⁵	0.790	0.733	9.774 ⁻²	1.092 ⁻²	5.923 ⁻³
0.233	1.391	5.705 ⁻²	6.281 ⁻⁴	8.602 ⁻⁵	0.800	0.706	8.325 ⁻²	1.291 ⁻²	7.530 ⁻³
0.246	1.368	5.774 ⁻²	6.010 ⁻⁴	1.440 ⁻⁴	0.810	0.713	9.292 ⁻²	1.168 ⁻²	6.459 ⁻³
0.259	1.349	5.348 ⁻²	5.167 ⁻⁴	9.588 ⁻⁵	0.820	0.698	8.209 ⁻²	1.196 ⁻²	6.836 ⁻³
0.272	1.325	5.386 ⁻²	5.449 ⁻⁴	1.462 ⁻⁴	0.829	0.679	7.325 ⁻²	1.294 ⁻²	7.827 ⁻³
0.285	1.306	5.302 ⁻²	5.457 ⁻⁴	1.346 ⁻⁴	0.836	0.653	6.689 ⁻²	1.440 ⁻²	9.090 ⁻³
0.298	1.285	5.891 ⁻²	5.353 ⁻⁴	1.237 ⁻⁴	0.843	0.653	6.738 ⁻²	1.478 ⁻²	9.088 ⁻³
0.311	1.269	5.671 ⁻²	4.814 ⁻⁴	9.875 ⁻⁵	0.850	0.631	5.492 ⁻²	1.581 ⁻²	9.724 ⁻³
0.325	1.253	5.327 ⁻²	4.315 ⁻⁴	9.057 ⁻⁵	0.857	0.627	5.123 ⁻²	1.533 ⁻²	9.271 ⁻³
0.345	1.224	5.672 ⁻²	4.790 ⁻⁴	1.038 ⁻⁴	0.864	0.623	4.802 ⁻²	1.457 ⁻²	8.665 ⁻³
0.365	1.202	6.337 ⁻²	5.959 ⁻⁴	1.482 ⁻⁴	0.871	0.614	4.712 ⁻²	1.459 ⁻²	8.434 ⁻³
0.385	1.176	5.520 ⁻²	6.554 ⁻⁴	1.860 ⁻⁴	0.877	0.596	3.965 ⁻²	1.597 ⁻²	9.059 ⁻³
0.405	1.149	4.940 ⁻²	4.641 ⁻⁴	1.058 ⁻⁴	0.884	0.580	4.079 ⁻²	1.764 ⁻²	9.531 ⁻³
0.425	1.126	5.999 ⁻²	1.051 ⁻³	3.361 ⁻⁴	0.891	0.566	2.722 ⁻²	1.967 ⁻²	1.098 ⁻²
0.445	1.102	5.607 ⁻²	1.136 ⁻³	3.056 ⁻⁴	0.898	0.576	3.607 ⁻²	2.004 ⁻²	9.674 ⁻³
0.465	1.076	6.434 ⁻²	2.288 ⁻³	1.070 ⁻³					

Table 8. Concluded ($\theta = 60$ deg)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.034	1.670	7.580 ⁻²	5.159 ⁻³	-9.448 ⁻⁴	0.459	1.041	4.138 ⁻²	5.090 ⁻³	1.772 ⁻³
0.041	1.670	6.913 ⁻²	4.675 ⁻³	-9.068 ⁻⁴	0.479	1.030	5.370 ⁻²	3.848 ⁻³	7.081 ⁻⁴
0.048	1.660	6.470 ⁻²	5.194 ⁻³	-1.149 ⁻³	0.519	0.969	4.848 ⁻²	6.142 ⁻³	2.917 ⁻³
0.055	1.642	6.722 ⁻²	5.680 ⁻³	-1.341 ⁻³	0.546	0.945	5.205 ⁻²	6.014 ⁻³	2.604 ⁻³
0.062	1.635	5.094 ⁻²	2.915 ⁻³	-6.740 ⁻⁵	0.573	0.939	6.224 ⁻²	4.383 ⁻³	1.863 ⁻³
0.069	1.626	6.095 ⁻²	3.944 ⁻³	-5.416 ⁻⁴	0.602	0.913	5.566 ⁻²	4.448 ⁻³	1.705 ⁻³
0.076	1.612	4.919 ⁻²	2.909 ⁻³	-2.250 ⁻⁴	0.627	0.893	7.572 ⁻²	5.878 ⁻³	3.304 ⁻³
0.082	1.602	5.304 ⁻²	2.985 ⁻³	-3.449 ⁻⁴	0.654	0.856	6.333 ⁻²	8.053 ⁻³	5.160 ⁻³
0.089	1.597	4.983 ⁻²	3.044 ⁻³	-6.629 ⁻⁴	0.662	0.867	7.086 ⁻²	5.142 ⁻³	2.938 ⁻³
0.099	1.568	4.508 ⁻²	3.062 ⁻³	-2.981 ⁻⁴	0.682	0.821	6.644 ⁻²	8.731 ⁻³	5.829 ⁻³
0.109	1.553	4.698 ⁻²	2.929 ⁻³	-4.050 ⁻⁴	0.708	0.811	7.132 ⁻²	8.183 ⁻³	5.163 ⁻³
0.119	1.545	4.920 ⁻²	3.318 ⁻³	-6.133 ⁻⁴	0.722	0.777	6.422 ⁻²	7.530 ⁻³	4.703 ⁻³
0.129	1.527	4.185 ⁻²	2.209 ⁻³	-2.203 ⁻⁴	0.735	0.780	7.396 ⁻²	8.106 ⁻³	5.629 ⁻³
0.138	1.514	5.014 ⁻²	3.053 ⁻³	-6.367 ⁻⁴	0.748	0.787	7.740 ⁻²	6.158 ⁻³	3.988 ⁻³
0.148	1.496	4.216 ⁻²	2.791 ⁻³	-5.447 ⁻⁴	0.761	0.739	7.200 ⁻²	9.063 ⁻³	6.239 ⁻³
0.158	1.476	4.360 ⁻²	2.556 ⁻³	-5.169 ⁻⁴	0.774	0.750	7.957 ⁻²	7.440 ⁻³	4.441 ⁻³
0.168	1.466	4.766 ⁻²	2.813 ⁻³	-6.239 ⁻⁴	0.788	0.734	7.638 ⁻²	9.040 ⁻³	5.804 ⁻³
0.178	1.438	3.779 ⁻²	2.547 ⁻³	-3.102 ⁻⁴	0.814	0.694	6.684 ⁻²	1.064 ⁻²	6.921 ⁻³
0.188	1.435	4.311 ⁻²	2.513 ⁻³	-6.305 ⁻⁴	0.824	0.638	6.545 ⁻²	1.143 ⁻²	6.711 ⁻³
0.201	1.408	3.334 ⁻²	2.500 ⁻³	-3.929 ⁻⁴	0.834	0.666	5.729 ⁻²	1.081 ⁻²	6.165 ⁻³
0.214	1.387	4.936 ⁻²	2.614 ⁻³	-6.054 ⁻⁴	0.843	0.634	5.301 ⁻²	1.177 ⁻²	6.933 ⁻³
0.227	1.373	4.768 ⁻²	1.981 ⁻³	-4.380 ⁻⁴	0.853	0.574	2.923 ⁻²	1.193 ⁻²	7.039 ⁻³
0.240	1.348	5.195 ⁻²	2.930 ⁻³	-4.131 ⁻⁴	0.863	0.591	4.109 ⁻²	1.218 ⁻²	7.157 ⁻³
0.253	1.323	4.554 ⁻²	2.716 ⁻³	-2.932 ⁻⁴	0.883	0.547	1.609 ⁻²	1.352 ⁻²	7.534 ⁻³
0.267	1.302	4.160 ⁻²	2.141 ⁻³	-2.334 ⁻⁴	0.903	0.542	3.853 ⁻²	1.343 ⁻²	5.997 ⁻³
0.280	1.282	4.906 ⁻²	2.421 ⁻³	-3.655 ⁻⁴	0.912	0.532	2.500 ⁻²	1.357 ⁻²	5.986 ⁻³
0.293	1.266	5.329 ⁻²	2.290 ⁻³	-4.347 ⁻⁴	0.919	0.542	1.359 ⁻²	1.104 ⁻²	5.640 ⁻³
0.306	1.242	4.521 ⁻²	2.646 ⁻³	-3.516 ⁻⁴	0.926	0.533	1.214 ⁻²	1.028 ⁻²	4.875 ⁻³
0.319	1.235	5.320 ⁻²	1.973 ⁻³	-1.466 ⁻⁴	0.933	0.543	1.993 ⁻²	9.442 ⁻³	4.485 ⁻³
0.339	1.209	5.195 ⁻²	2.033 ⁻³	3.593 ⁻⁵	0.940	0.548	3.036 ⁻²	8.115 ⁻³	3.570 ⁻³
0.359	1.179	5.638 ⁻²	2.485 ⁻³	8.662 ⁻⁵	0.954	0.494	1.513 ⁻²	1.192 ⁻²	3.691 ⁻³
0.379	1.144	3.882 ⁻²	2.773 ⁻³	4.148 ⁻⁴	0.960	0.528	3.034 ⁻²	9.681 ⁻³	2.873 ⁻³
0.419	1.098	4.720 ⁻²	2.733 ⁻³	5.799 ⁻⁴	0.967	0.526	3.061 ⁻²	8.762 ⁻³	2.310 ⁻³
0.439	1.072	4.069 ⁻²	3.472 ⁻³	9.031 ⁻⁴	0.981	0.518	3.659 ⁻²	9.053 ⁻³	1.706 ⁻³

Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)

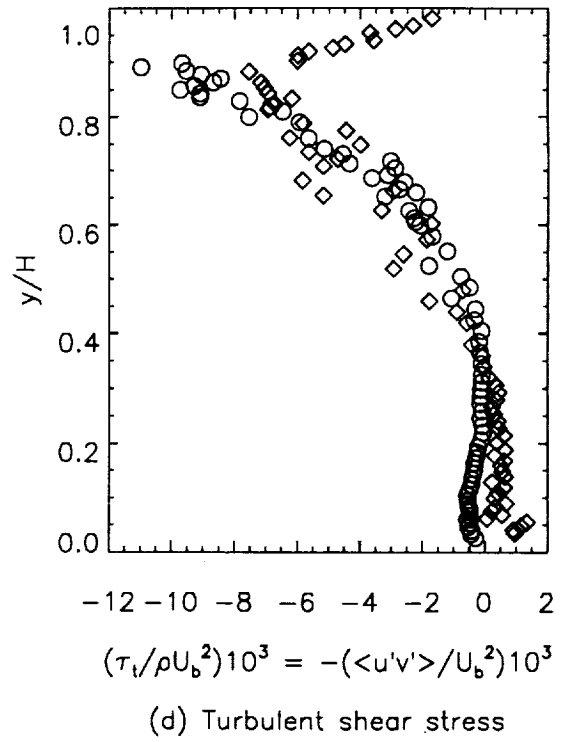
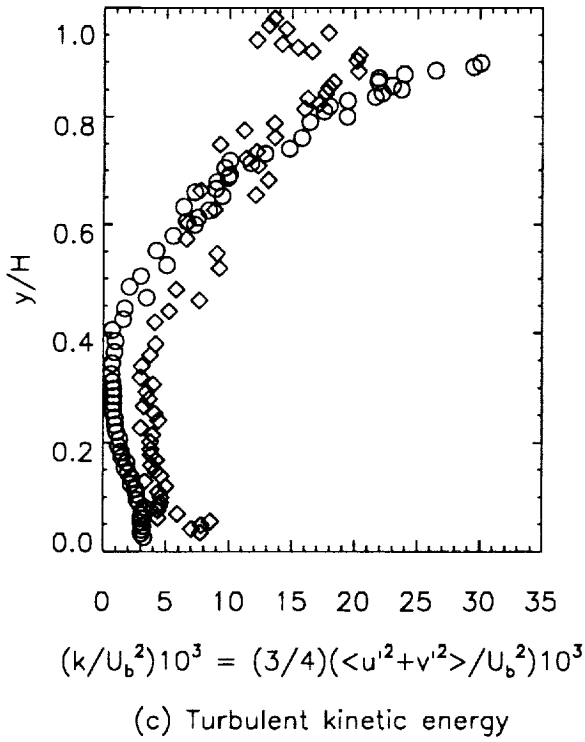
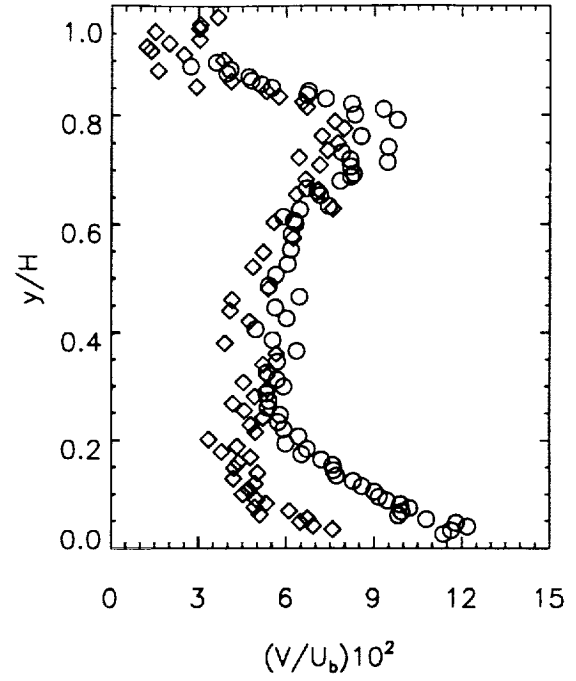
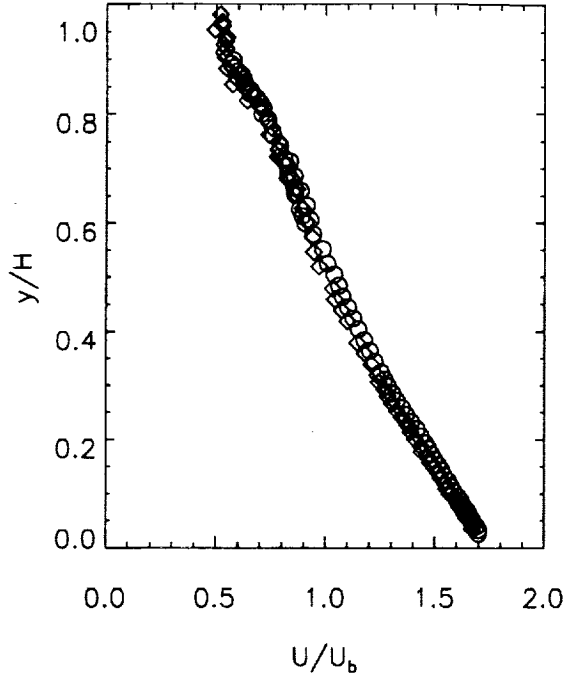


Figure 8. Summary of Table 8 ($\theta = 60$ deg).

Table 9. LDV flowfield in TAD ($\theta = 90$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.025	1.664	8.480^{-2}	3.554^{-3}	-8.794^{-4}	0.518	0.976	7.327^{-2}	3.197^{-3}	1.212^{-3}
0.031	1.665	9.266^{-2}	3.245^{-3}	-7.576^{-4}	0.538	0.962	8.798^{-2}	3.089^{-3}	1.003^{-3}
0.038	1.666	1.005^{-1}	3.129^{-3}	-5.865^{-4}	0.551	0.977	1.122^{-1}	4.851^{-3}	1.867^{-3}
0.045	1.660	1.087^{-1}	3.253^{-3}	-5.618^{-4}	0.558	0.940	1.150^{-1}	5.262^{-3}	2.432^{-3}
0.051	1.655	1.123^{-1}	2.868^{-3}	3.410^{-5}	0.578	0.936	1.178^{-1}	5.151^{-3}	2.121^{-3}
0.058	1.652	1.173^{-1}	2.645^{-3}	2.028^{-4}	0.598	0.902	1.037^{-1}	5.932^{-3}	3.022^{-3}
0.065	1.643	1.201^{-1}	2.730^{-3}	2.077^{-4}	0.605	0.924	1.218^{-1}	6.732^{-3}	3.223^{-3}
0.071	1.636	1.228^{-1}	2.365^{-3}	5.361^{-4}	0.618	0.888	1.060^{-1}	6.255^{-3}	3.362^{-3}
0.078	1.624	1.214^{-1}	2.326^{-3}	5.929^{-4}	0.631	0.899	1.195^{-1}	7.150^{-3}	3.625^{-3}
0.085	1.616	1.202^{-1}	2.292^{-3}	7.011^{-4}	0.638	0.869	1.020^{-1}	6.595^{-3}	3.567^{-3}
0.091	1.608	1.255^{-1}	2.156^{-3}	6.262^{-4}	0.658	0.856	1.169^{-1}	1.021^{-2}	5.910^{-3}
0.101	1.590	1.221^{-1}	2.381^{-3}	5.883^{-4}	0.691	0.818	1.080^{-1}	9.480^{-3}	5.996^{-3}
0.111	1.579	1.193^{-1}	2.193^{-3}	6.442^{-4}	0.705	0.806	1.080^{-1}	9.482^{-3}	6.022^{-3}
0.121	1.567	1.206^{-1}	1.948^{-3}	6.749^{-4}	0.711	0.818	1.264^{-1}	1.467^{-2}	8.064^{-3}
0.131	1.552	1.145^{-1}	2.055^{-3}	7.016^{-4}	0.718	0.797	1.073^{-1}	1.035^{-2}	6.583^{-3}
0.141	1.531	1.085^{-1}	1.855^{-3}	6.404^{-4}	0.731	0.784	1.047^{-1}	1.004^{-2}	6.251^{-3}
0.151	1.518	1.057^{-1}	1.988^{-3}	3.527^{-4}	0.745	0.754	8.399^{-2}	1.479^{-2}	9.573^{-3}
0.161	1.502	1.103^{-1}	1.726^{-3}	5.016^{-4}	0.758	0.756	9.536^{-2}	1.378^{-2}	9.002^{-3}
0.171	1.489	1.056^{-1}	1.431^{-3}	4.282^{-4}	0.765	0.770	1.270^{-1}	1.514^{-2}	9.323^{-3}
0.181	1.469	1.001^{-1}	1.379^{-3}	4.957^{-4}	0.811	0.705	7.902^{-2}	1.539^{-2}	1.011^{-2}
0.191	1.451	1.048^{-1}	1.482^{-3}	4.431^{-4}	0.841	0.671	8.696^{-2}	1.824^{-2}	8.542^{-3}
0.205	1.433	9.795^{-2}	1.105^{-3}	3.090^{-4}	0.851	0.667	4.048^{-2}	1.491^{-2}	8.999^{-3}
0.218	1.408	1.038^{-1}	1.318^{-3}	3.745^{-4}	0.861	0.649	4.730^{-2}	1.587^{-2}	9.747^{-3}
0.231	1.390	9.381^{-2}	9.530^{-4}	2.330^{-4}	0.871	0.651	5.057^{-2}	1.551^{-2}	9.373^{-3}
0.245	1.363	8.385^{-2}	1.209^{-3}	2.996^{-4}	0.881	0.633	3.925^{-2}	1.371^{-2}	7.967^{-3}
0.258	1.346	9.487^{-2}	9.968^{-4}	2.431^{-4}	0.891	0.624	2.390^{-2}	1.272^{-2}	6.987^{-3}
0.271	1.321	9.801^{-2}	1.321^{-3}	1.642^{-4}	0.901	0.631	4.391^{-2}	1.131^{-2}	6.401^{-3}
0.285	1.305	9.232^{-2}	9.270^{-4}	1.784^{-4}	0.911	0.617	3.779^{-2}	1.155^{-2}	6.722^{-3}
0.298	1.283	9.551^{-2}	9.748^{-4}	1.048^{-4}	0.918	0.605	3.317^{-2}	1.055^{-2}	6.060^{-3}
0.311	1.262	9.214^{-2}	1.100^{-3}	2.173^{-4}	0.925	0.599	2.654^{-2}	1.047^{-2}	5.493^{-3}
0.405	1.141	1.049^{-1}	8.433^{-4}	7.407^{-5}	0.931	0.612	2.392^{-2}	9.624^{-3}	4.796^{-3}
0.425	1.097	7.402^{-2}	1.560^{-3}	2.897^{-4}	0.938	0.599	1.676^{-2}	9.624^{-3}	4.290^{-3}
0.445	1.089	1.127^{-1}	2.521^{-3}	3.701^{-4}	0.945	0.585	3.736^{-3}	9.515^{-3}	4.148^{-3}
0.451	1.047	5.763^{-2}	2.118^{-3}	4.464^{-4}	0.951	0.589	1.545^{-2}	9.203^{-3}	3.928^{-3}
0.465	1.070	1.180^{-1}	2.504^{-3}	4.089^{-4}	0.958	0.573	1.031^{-2}	9.352^{-3}	3.597^{-3}
0.478	1.019	7.386^{-2}	2.898^{-3}	7.986^{-4}	0.965	0.558	3.507^{-3}	8.988^{-3}	3.395^{-3}
0.498	0.989	6.766^{-2}	4.204^{-3}	1.860^{-3}	0.971	0.546	2.508^{-4}	8.658^{-3}	3.258^{-3}
0.505	1.019	1.084^{-1}	4.618^{-3}	1.522^{-3}	0.978	0.513	-6.853^{-3}	9.166^{-3}	3.030^{-3}

Table 9. Continued ($\theta = 90$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	1.676	5.713^{-2}	3.806^{-3}	-6.821^{-4}	0.500	0.953	2.509^{-2}	1.469^{-2}	1.094^{-2}
0.027	1.659	5.697^{-2}	3.600^{-3}	-8.488^{-4}	0.520	0.943	4.958^{-2}	1.103^{-2}	7.267^{-3}
0.033	1.655	5.673^{-2}	3.317^{-3}	-4.947^{-4}	0.540	0.929	5.402^{-2}	1.240^{-2}	8.153^{-3}
0.040	1.644	5.690^{-2}	3.562^{-3}	-5.808^{-4}	0.547	0.854	-8.499^{-3}	2.125^{-2}	1.509^{-2}
0.047	1.627	5.513^{-2}	3.506^{-3}	-6.536^{-4}	0.560	0.886	3.056^{-2}	1.730^{-2}	1.203^{-2}
0.053	1.609	6.559^{-2}	4.666^{-3}	-1.864^{-3}	0.573	0.869	3.190^{-2}	1.584^{-2}	1.074^{-2}
0.060	1.615	6.013^{-2}	4.657^{-3}	-1.745^{-3}	0.580	0.886	6.018^{-2}	1.387^{-2}	9.075^{-3}
0.067	1.595	6.151^{-2}	4.333^{-3}	-1.593^{-3}	0.600	0.846	2.250^{-2}	1.826^{-2}	1.235^{-2}
0.073	1.593	5.935^{-2}	3.397^{-3}	-8.274^{-4}	0.620	0.859	6.229^{-2}	1.397^{-2}	8.949^{-3}
0.080	1.587	5.486^{-2}	2.575^{-3}	9.504^{-6}	0.627	0.791	5.692^{-3}	2.356^{-2}	1.576^{-2}
0.087	1.569	5.263^{-2}	2.640^{-3}	-1.929^{-4}	0.653	0.803	5.411^{-2}	1.641^{-2}	1.086^{-2}
0.097	1.548	5.223^{-2}	1.856^{-3}	2.786^{-4}	0.660	0.826	5.387^{-2}	1.430^{-2}	8.631^{-3}
0.107	1.538	5.305^{-2}	1.748^{-3}	3.174^{-4}	0.680	0.788	4.398^{-2}	1.542^{-2}	1.020^{-2}
0.117	1.518	5.423^{-2}	2.342^{-3}	-2.781^{-4}	0.693	0.761	6.689^{-3}	2.471^{-2}	1.550^{-2}
0.127	1.510	6.191^{-2}	1.971^{-3}	-1.513^{-4}	0.707	0.758	2.879^{-2}	2.014^{-2}	1.285^{-2}
0.137	1.492	5.984^{-2}	1.933^{-3}	-2.819^{-4}	0.720	0.728	-1.151^{-2}	2.439^{-2}	1.452^{-2}
0.147	1.470	6.341^{-2}	1.292^{-3}	2.739^{-4}	0.733	0.727	2.723^{-2}	1.924^{-2}	1.140^{-2}
0.157	1.467	6.366^{-2}	1.344^{-3}	1.327^{-4}	0.747	0.727	1.848^{-2}	1.804^{-2}	9.817^{-3}
0.167	1.444	5.927^{-2}	1.697^{-3}	-4.873^{-5}	0.760	0.677	-1.930^{-3}	2.006^{-2}	1.174^{-2}
0.177	1.430	6.673^{-2}	9.668^{-4}	1.247^{-4}	0.773	0.683	-1.145^{-2}	2.258^{-2}	1.376^{-2}
0.187	1.415	6.790^{-2}	9.076^{-4}	1.126^{-4}	0.787	0.680	5.054^{-3}	1.769^{-2}	9.785^{-3}
0.200	1.390	5.817^{-2}	7.993^{-4}	1.013^{-4}	0.800	0.696	4.357^{-2}	1.372^{-2}	8.133^{-3}
0.213	1.365	5.064^{-2}	1.260^{-3}	1.888^{-4}	0.813	0.684	3.790^{-2}	1.452^{-2}	8.269^{-3}
0.227	1.347	6.674^{-2}	1.251^{-3}	3.180^{-5}	0.823	0.653	-2.040^{-3}	1.851^{-2}	1.054^{-2}
0.240	1.331	6.430^{-2}	1.235^{-3}	2.627^{-4}	0.833	0.644	-3.831^{-3}	1.697^{-2}	9.183^{-3}
0.253	1.305	6.083^{-2}	1.202^{-3}	2.734^{-4}	0.843	0.662	1.956^{-2}	1.575^{-2}	8.191^{-3}
0.267	1.286	6.336^{-2}	1.862^{-3}	4.351^{-4}	0.853	0.653	2.663^{-2}	1.432^{-2}	7.755^{-3}
0.280	1.267	5.544^{-2}	1.102^{-3}	2.317^{-4}	0.863	0.621	-5.176^{-3}	1.875^{-2}	9.356^{-3}
0.293	1.245	5.612^{-2}	3.275^{-3}	1.658^{-3}	0.873	0.646	1.719^{-2}	1.459^{-2}	7.129^{-3}
0.307	1.211	3.054^{-2}	5.158^{-3}	2.976^{-3}	0.883	0.644	2.894^{-2}	1.264^{-2}	5.935^{-3}
0.320	1.206	6.001^{-2}	3.392^{-3}	1.623^{-3}	0.893	0.631	1.409^{-2}	1.294^{-2}	5.873^{-3}
0.340	1.170	5.012^{-2}	3.376^{-3}	1.519^{-3}	0.903	0.632	2.985^{-2}	1.130^{-2}	5.094^{-3}
0.347	1.174	5.940^{-2}	3.837^{-3}	2.204^{-3}	0.913	0.596	2.461^{-2}	1.504^{-2}	4.528^{-3}
0.360	1.125	2.609^{-2}	9.560^{-3}	6.567^{-3}	0.933	0.602	1.583^{-2}	1.089^{-2}	4.359^{-3}
0.373	1.133	4.543^{-2}	5.575^{-3}	3.344^{-3}	0.940	0.593	1.369^{-2}	9.798^{-3}	3.893^{-3}
0.400	1.075	3.498^{-2}	9.033^{-3}	6.208^{-3}	0.947	0.593	1.189^{-2}	9.592^{-3}	3.705^{-3}
0.427	1.042	2.259^{-2}	1.391^{-2}	1.059^{-2}	0.953	0.581	1.237^{-2}	1.041^{-2}	3.421^{-3}
0.440	1.019	2.235^{-2}	1.145^{-2}	8.432^{-3}	0.960	0.572	6.476^{-3}	9.083^{-3}	2.941^{-3}
0.453	0.999	2.581^{-2}	1.516^{-2}	1.006^{-2}	0.967	0.569	1.257^{-2}	8.498^{-3}	2.886^{-3}
0.460	1.011	3.898^{-2}	8.990^{-3}	6.515^{-3}	0.973	0.558	1.155^{-2}	8.415^{-3}	2.392^{-3}
0.480	0.983	3.809^{-2}	1.187^{-2}	8.597^{-3}	0.980	0.546	4.758^{-3}	9.327^{-3}	2.939^{-3}

Table 9. Continued ($\theta = 90$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.027	1.632	4.612^{-2}	2.894^{-3}	-6.292^{-4}	0.493	0.934	3.909^{-2}	1.759^{-2}	1.178^{-2}
0.033	1.628	4.653^{-2}	2.110^{-3}	5.127^{-5}	0.500	0.913	1.531^{-2}	1.919^{-2}	1.346^{-2}
0.040	1.621	5.159^{-2}	2.438^{-3}	-5.220^{-4}	0.513	0.901	1.828^{-2}	2.001^{-2}	1.332^{-2}
0.047	1.624	5.174^{-2}	2.921^{-3}	-6.341^{-4}	0.533	0.893	2.383^{-2}	2.006^{-2}	1.277^{-2}
0.053	1.616	5.219^{-2}	3.141^{-3}	-8.624^{-4}	0.547	0.820	-2.677^{-2}	2.456^{-2}	1.620^{-2}
0.060	1.607	4.681^{-2}	2.247^{-3}	-1.173^{-4}	0.553	0.884	5.586^{-2}	2.393^{-2}	1.405^{-2}
0.067	1.602	4.832^{-2}	2.126^{-3}	1.633^{-4}	0.573	0.826	7.414^{-3}	2.397^{-2}	1.489^{-2}
0.073	1.581	5.394^{-2}	2.045^{-3}	2.121^{-5}	0.593	0.788	-4.240^{-2}	2.880^{-2}	1.760^{-2}
0.080	1.577	5.511^{-2}	1.706^{-3}	2.405^{-4}	0.600	0.791	-1.277^{-2}	1.993^{-2}	1.276^{-2}
0.087	1.564	6.126^{-2}	2.381^{-3}	-6.068^{-4}	0.613	0.813	7.406^{-3}	2.794^{-2}	1.665^{-2}
0.097	1.559	5.978^{-2}	1.614^{-3}	-2.447^{-5}	0.627	0.762	-6.000^{-3}	2.207^{-2}	1.387^{-2}
0.107	1.533	6.024^{-2}	1.985^{-3}	-3.283^{-4}	0.653	0.775	2.258^{-2}	2.331^{-2}	1.416^{-2}
0.117	1.520	6.096^{-2}	1.458^{-3}	5.614^{-5}	0.673	0.771	2.309^{-2}	2.636^{-2}	1.650^{-2}
0.127	1.503	6.801^{-2}	2.127^{-3}	-6.414^{-4}	0.680	0.733	4.189^{-4}	2.098^{-2}	1.178^{-2}
0.137	1.494	6.341^{-2}	1.411^{-3}	-1.605^{-4}	0.687	0.774	4.165^{-2}	2.139^{-2}	1.265^{-2}
0.147	1.475	6.390^{-2}	1.255^{-3}	1.570^{-4}	0.700	0.735	-4.395^{-2}	2.981^{-2}	1.613^{-2}
0.157	1.454	7.603^{-2}	2.131^{-3}	-8.021^{-4}	0.707	0.708	-3.946^{-2}	2.860^{-2}	1.733^{-2}
0.167	1.445	7.231^{-2}	9.817^{-4}	-2.678^{-5}	0.713	0.742	1.541^{-2}	2.353^{-2}	1.444^{-2}
0.177	1.429	6.764^{-2}	1.010^{-3}	5.506^{-5}	0.740	0.714	-2.391^{-3}	2.265^{-2}	1.371^{-2}
0.187	1.407	6.162^{-2}	9.944^{-4}	7.176^{-5}	0.753	0.686	-4.832^{-2}	2.168^{-2}	1.126^{-2}
0.200	1.385	6.073^{-2}	1.154^{-3}	3.963^{-5}	0.767	0.719	3.858^{-2}	2.102^{-2}	1.270^{-2}
0.213	1.361	6.514^{-2}	1.200^{-3}	-2.079^{-4}	0.780	0.666	-2.027^{-2}	2.246^{-2}	1.267^{-2}
0.227	1.340	6.640^{-2}	1.803^{-3}	1.729^{-4}	0.793	0.672	-6.238^{-3}	2.052^{-2}	1.173^{-2}
0.233	1.328	3.731^{-2}	1.170^{-3}	3.342^{-4}	0.807	0.670	5.822^{-3}	1.824^{-2}	1.076^{-2}
0.240	1.314	6.293^{-2}	1.642^{-3}	-3.936^{-5}	0.817	0.678	1.753^{-2}	1.706^{-2}	9.938^{-3}
0.253	1.297	6.712^{-2}	2.347^{-3}	3.604^{-4}	0.827	0.646	-2.806^{-2}	1.834^{-2}	1.052^{-2}
0.267	1.270	4.742^{-2}	3.259^{-3}	1.335^{-3}	0.847	0.627	-3.008^{-2}	1.704^{-2}	9.728^{-3}
0.280	1.252	5.717^{-2}	2.753^{-3}	7.123^{-4}	0.857	0.605	-4.635^{-2}	1.678^{-2}	8.754^{-3}
0.287	1.218	1.609^{-2}	3.121^{-3}	1.397^{-3}	0.867	0.623	-2.357^{-2}	1.504^{-2}	8.702^{-3}
0.307	1.210	5.953^{-2}	3.562^{-3}	1.452^{-3}	0.877	0.624	-1.108^{-2}	1.358^{-2}	7.241^{-3}
0.313	1.170	1.703^{-2}	5.222^{-3}	2.660^{-3}	0.887	0.613	7.177^{-3}	1.396^{-2}	7.645^{-3}
0.320	1.186	4.630^{-2}	4.027^{-3}	1.755^{-3}	0.897	0.578	-3.929^{-2}	1.349^{-2}	6.652^{-3}
0.340	1.137	1.843^{-2}	6.044^{-3}	3.314^{-3}	0.907	0.583	-3.619^{-2}	1.249^{-2}	6.289^{-3}
0.360	1.120	4.221^{-2}	8.149^{-3}	5.004^{-3}	0.913	0.582	-1.504^{-2}	1.188^{-2}	6.033^{-3}
0.367	1.112	4.028^{-2}	4.685^{-3}	2.236^{-3}	0.920	0.572	-4.036^{-2}	1.127^{-2}	5.726^{-3}
0.380	1.082	2.455^{-2}	1.040^{-2}	6.645^{-3}	0.927	0.570	-3.272^{-2}	1.052^{-2}	5.068^{-3}
0.393	1.073	3.446^{-2}	7.021^{-3}	4.167^{-3}	0.933	0.551	-3.780^{-2}	1.031^{-2}	4.697^{-3}
0.420	1.003	-2.214^{-3}	1.759^{-2}	1.171^{-2}	0.940	0.560	-2.505^{-2}	9.493^{-3}	4.122^{-3}
0.440	0.984	1.133^{-2}	1.691^{-2}	1.147^{-2}	0.947	0.540	-3.645^{-2}	9.199^{-3}	3.914^{-3}
0.447	0.963	9.399^{-3}	1.866^{-2}	1.134^{-2}	0.953	0.552	-1.798^{-2}	9.046^{-3}	4.154^{-3}
0.460	0.968	3.910^{-3}	1.712^{-2}	1.226^{-2}	0.960	0.531	-2.603^{-2}	8.318^{-3}	3.387^{-3}
0.473	0.941	5.604^{-3}	2.071^{-2}	1.370^{-2}	0.967	0.540	-1.988^{-2}	8.144^{-3}	3.350^{-3}
0.480	0.936	2.284^{-2}	1.617^{-2}	1.038^{-2}	0.973	0.522	-1.842^{-2}	7.713^{-3}	2.940^{-3}

Table 9. Continued ($\theta = 90$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

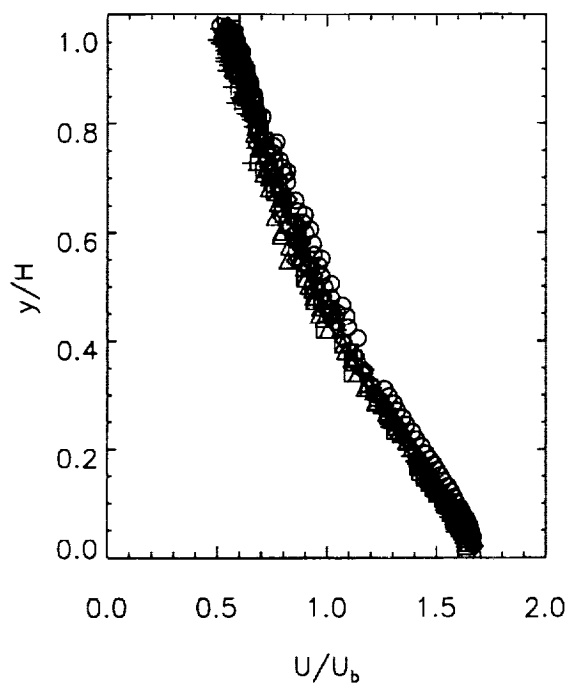
$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	1.633	5.900^{-2}	3.180^{-3}	-6.418^{-4}	0.613	0.827	3.753^{-2}	1.788^{-2}	1.098^{-2}
0.027	1.651	5.973^{-2}	3.625^{-3}	-7.753^{-4}	0.633	0.799	1.284^{-2}	2.115^{-2}	1.301^{-2}
0.033	1.637	5.445^{-2}	3.974^{-3}	-1.194^{-3}	0.653	0.799	3.807^{-2}	1.906^{-2}	1.113^{-2}
0.040	1.631	5.308^{-2}	3.535^{-3}	-7.920^{-4}	0.673	0.762	3.576^{-2}	1.937^{-2}	1.233^{-2}
0.047	1.632	5.385^{-2}	4.278^{-3}	-1.495^{-3}	0.687	0.779	6.350^{-2}	1.800^{-2}	1.130^{-2}
0.053	1.604	5.440^{-2}	3.832^{-3}	-9.898^{-4}	0.700	0.761	4.558^{-2}	1.803^{-2}	1.069^{-2}
0.060	1.595	5.447^{-2}	3.819^{-3}	-1.287^{-3}	0.713	0.738	3.534^{-2}	1.816^{-2}	1.120^{-2}
0.067	1.582	6.569^{-2}	3.087^{-3}	-3.855^{-4}	0.727	0.757	7.086^{-2}	1.401^{-2}	8.598^{-3}
0.073	1.588	5.928^{-2}	2.744^{-3}	-6.317^{-4}	0.740	0.727	4.926^{-2}	1.769^{-2}	1.146^{-2}
0.080	1.566	3.921^{-2}	2.940^{-3}	-5.139^{-4}	0.753	0.717	3.909^{-2}	1.657^{-2}	1.011^{-2}
0.087	1.578	4.971^{-2}	2.756^{-3}	-6.150^{-4}	0.767	0.708	4.512^{-2}	1.659^{-2}	1.025^{-2}
0.097	1.540	6.760^{-2}	3.296^{-3}	-1.147^{-3}	0.780	0.694	3.498^{-2}	1.680^{-2}	9.862^{-3}
0.107	1.530	4.597^{-2}	3.287^{-3}	-8.380^{-4}	0.793	0.681	3.522^{-2}	1.694^{-2}	9.952^{-3}
0.117	1.502	7.804^{-2}	3.696^{-3}	-1.156^{-3}	0.807	0.684	4.021^{-2}	1.637^{-2}	9.704^{-3}
0.127	1.486	4.683^{-2}	3.552^{-3}	-8.881^{-4}	0.817	0.672	4.632^{-2}	1.515^{-2}	9.173^{-3}
0.137	1.467	5.440^{-2}	4.052^{-3}	-5.982^{-4}	0.827	0.654	7.851^{-3}	1.706^{-2}	9.363^{-3}
0.147	1.446	6.076^{-2}	4.805^{-3}	-1.138^{-3}	0.837	0.666	3.652^{-2}	1.414^{-2}	7.647^{-3}
0.157	1.426	7.018^{-2}	3.695^{-3}	-3.853^{-4}	0.847	0.660	4.279^{-2}	1.369^{-2}	7.682^{-3}
0.167	1.416	7.621^{-2}	4.165^{-3}	-1.568^{-3}	0.857	0.627	2.638^{-2}	1.390^{-2}	7.845^{-3}
0.233	1.312	2.315^{-2}	1.749^{-3}	6.750^{-4}	0.867	0.632	3.033^{-2}	1.423^{-2}	8.059^{-3}
0.260	1.280	4.867^{-2}	1.907^{-3}	5.578^{-4}	0.877	0.635	3.227^{-2}	1.294^{-2}	6.720^{-3}
0.287	1.232	2.329^{-2}	1.890^{-3}	6.845^{-4}	0.887	0.620	2.133^{-2}	1.337^{-2}	6.979^{-3}
0.313	1.193	5.982^{-2}	2.816^{-3}	1.276^{-3}	0.897	0.624	2.834^{-2}	1.235^{-2}	5.770^{-3}
0.340	1.116	1.049^{-2}	1.015^{-2}	6.141^{-3}	0.907	0.608	1.753^{-2}	1.203^{-2}	5.954^{-3}
0.367	1.120	4.606^{-2}	4.721^{-3}	2.669^{-3}	0.913	0.599	8.824^{-3}	1.147^{-2}	5.514^{-3}
0.393	1.072	3.821^{-2}	6.998^{-3}	4.152^{-3}	0.920	0.600	1.016^{-2}	1.143^{-2}	5.509^{-3}
0.420	0.990	-1.185^{-2}	1.535^{-2}	1.015^{-2}	0.927	0.593	1.518^{-2}	1.073^{-2}	5.063^{-3}
0.447	1.019	6.430^{-2}	7.693^{-3}	4.725^{-3}	0.933	0.588	9.851^{-3}	1.007^{-2}	4.565^{-3}
0.473	0.979	5.371^{-2}	1.019^{-2}	6.754^{-3}	0.940	0.577	6.564^{-3}	9.599^{-3}	4.465^{-3}
0.493	0.939	4.211^{-2}	1.494^{-2}	9.628^{-3}	0.947	0.578	6.451^{-3}	9.371^{-3}	4.157^{-3}
0.513	0.901	5.017^{-3}	1.945^{-2}	1.267^{-2}	0.953	0.572	2.095^{-3}	9.070^{-3}	4.048^{-3}
0.533	0.918	4.777^{-2}	1.171^{-2}	7.236^{-3}	0.960	0.577	4.987^{-3}	8.563^{-3}	3.579^{-3}
0.553	0.887	5.307^{-2}	1.633^{-2}	1.013^{-2}	0.967	0.565	1.585^{-3}	7.926^{-3}	3.179^{-3}
0.573	0.860	3.331^{-2}	1.599^{-2}	9.381^{-3}	0.973	0.564	7.642^{-4}	7.727^{-3}	2.879^{-3}
0.593	0.866	6.860^{-2}	1.410^{-2}	9.162^{-3}					

Table 9. Concluded ($\theta = 90$ deg)

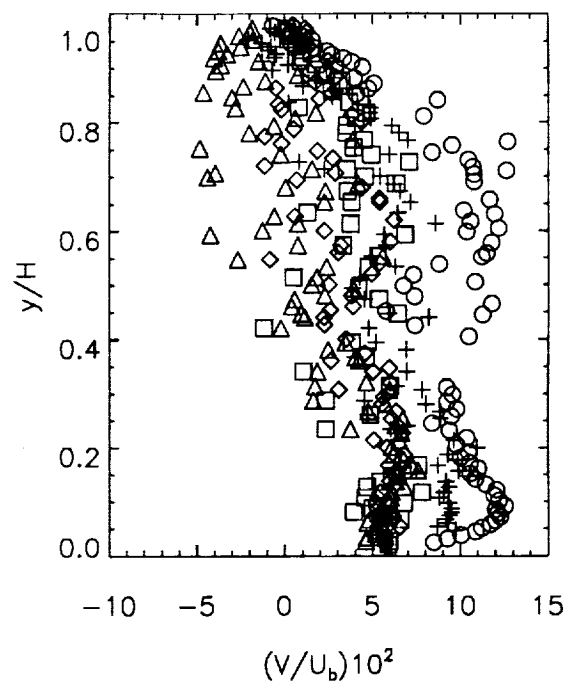
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.047	1.580	9.734^{-2}	4.947^{-3}	-2.163^{-3}	0.533	0.940	6.328^{-2}	5.722^{-3}	3.186^{-3}
0.053	1.575	8.675^{-2}	3.550^{-3}	-1.089^{-3}	0.553	0.894	4.970^{-2}	9.807^{-3}	6.156^{-3}
0.060	1.574	9.289^{-2}	3.086^{-3}	-6.102^{-4}	0.573	0.872	5.754^{-2}	1.140^{-2}	7.346^{-3}
0.067	1.562	9.194^{-2}	3.381^{-3}	-9.389^{-4}	0.593	0.858	5.674^{-2}	9.256^{-3}	5.970^{-3}
0.073	1.551	9.372^{-2}	2.709^{-3}	-5.123^{-4}	0.613	0.848	8.577^{-2}	1.032^{-2}	6.440^{-3}
0.080	1.547	9.496^{-2}	2.676^{-3}	-4.396^{-4}	0.633	0.827	6.443^{-2}	1.322^{-2}	8.241^{-3}
0.087	1.528	9.471^{-2}	2.579^{-3}	-4.557^{-4}	0.653	0.798	7.164^{-2}	1.155^{-2}	7.340^{-3}
0.097	1.524	9.330^{-2}	2.580^{-3}	-4.828^{-4}	0.673	0.761	6.569^{-2}	1.323^{-2}	8.781^{-3}
0.107	1.504	8.799^{-2}	2.410^{-3}	-3.911^{-4}	0.687	0.741	6.222^{-2}	1.595^{-2}	1.067^{-2}
0.117	1.488	9.049^{-2}	2.539^{-3}	-6.104^{-4}	0.700	0.722	5.438^{-2}	1.473^{-2}	9.680^{-3}
0.127	1.474	9.343^{-2}	2.182^{-3}	-4.276^{-4}	0.713	0.675	2.256^{-2}	1.597^{-2}	1.050^{-2}
0.137	1.455	9.188^{-2}	2.171^{-3}	-4.362^{-4}	0.727	0.650	8.015^{-3}	1.618^{-2}	1.041^{-2}
0.147	1.459	1.051^{-1}	2.376^{-3}	-6.010^{-4}	0.740	0.687	5.959^{-2}	1.558^{-2}	1.019^{-2}
0.157	1.423	9.916^{-2}	2.539^{-3}	-9.145^{-4}	0.753	0.667	4.024^{-2}	1.516^{-2}	9.906^{-3}
0.167	1.409	8.714^{-2}	2.090^{-3}	-8.858^{-4}	0.767	0.686	6.995^{-2}	1.566^{-2}	9.880^{-3}
0.177	1.395	9.874^{-2}	2.367^{-3}	-1.415^{-3}	0.780	0.678	6.484^{-2}	1.532^{-2}	9.650^{-3}
0.187	1.375	9.295^{-2}	3.148^{-3}	-1.724^{-3}	0.793	0.654	6.080^{-2}	1.602^{-2}	1.028^{-2}
0.200	1.356	1.095^{-1}	2.645^{-3}	-1.450^{-3}	0.807	0.646	4.878^{-2}	1.476^{-2}	8.892^{-3}
0.213	1.333	9.631^{-2}	2.726^{-3}	-1.672^{-3}	0.817	0.625	4.826^{-2}	1.602^{-2}	1.010^{-2}
0.233	1.334	6.031^{-2}	8.234^{-4}	2.663^{-4}	0.827	0.622	4.842^{-2}	1.526^{-2}	9.589^{-3}
0.240	1.283	6.984^{-2}	3.077^{-3}	-1.125^{-3}	0.837	0.578	2.099^{-3}	1.489^{-2}	8.239^{-3}
0.253	1.272	8.878^{-2}	2.268^{-3}	-1.017^{-3}	0.847	0.593	2.698^{-2}	1.545^{-2}	9.022^{-3}
0.260	1.288	4.717^{-2}	6.176^{-4}	1.051^{-4}	0.857	0.607	2.856^{-2}	1.486^{-2}	8.452^{-3}
0.267	1.246	8.854^{-2}	3.180^{-3}	-1.871^{-3}	0.867	0.561	1.028^{-2}	1.398^{-2}	7.877^{-3}
0.280	1.224	8.045^{-2}	3.380^{-3}	-2.249^{-3}	0.877	0.588	1.759^{-2}	1.350^{-2}	7.076^{-3}
0.287	1.245	4.514^{-2}	5.238^{-4}	8.419^{-5}	0.887	0.566	9.505^{-3}	1.289^{-2}	6.428^{-3}
0.307	1.182	7.803^{-2}	4.310^{-3}	-9.640^{-4}	0.897	0.536	-7.243^{-3}	1.188^{-2}	5.551^{-3}
0.313	1.211	6.342^{-2}	5.648^{-4}	7.090^{-5}	0.907	0.547	1.928^{-3}	1.178^{-2}	5.765^{-3}
0.340	1.163	6.937^{-2}	2.369^{-3}	4.615^{-5}	0.913	0.530	-1.276^{-2}	1.087^{-2}	5.004^{-3}
0.367	1.136	3.984^{-2}	9.336^{-4}	1.355^{-4}	0.920	0.527	-5.893^{-3}	1.057^{-2}	4.573^{-3}
0.380	1.092	6.909^{-2}	4.053^{-3}	-2.832^{-4}	0.927	0.538	-4.954^{-3}	1.070^{-2}	4.686^{-3}
0.393	1.105	5.174^{-2}	1.970^{-3}	5.566^{-4}	0.933	0.529	-9.721^{-3}	1.000^{-2}	3.992^{-3}
0.420	1.053	4.786^{-2}	3.268^{-3}	1.038^{-3}	0.940	0.535	-7.696^{-3}	9.802^{-3}	3.858^{-3}
0.440	1.027	8.194^{-2}	6.530^{-3}	2.443^{-3}	0.947	0.507	-1.310^{-2}	9.243^{-3}	3.080^{-3}
0.447	1.044	5.902^{-2}	2.062^{-3}	5.535^{-4}	0.953	0.495	-2.043^{-2}	8.363^{-3}	2.378^{-3}
0.473	1.003	4.557^{-2}	3.744^{-3}	1.723^{-3}	0.960	0.530	-1.958^{-3}	8.780^{-3}	2.959^{-3}
0.493	0.955	3.848^{-2}	6.016^{-3}	3.226^{-3}	0.967	0.520	-5.593^{-3}	8.031^{-3}	2.567^{-3}
0.513	0.942	4.264^{-2}	7.429^{-3}	4.430^{-3}	0.973	0.502	-8.333^{-3}	7.567^{-3}	2.194^{-3}

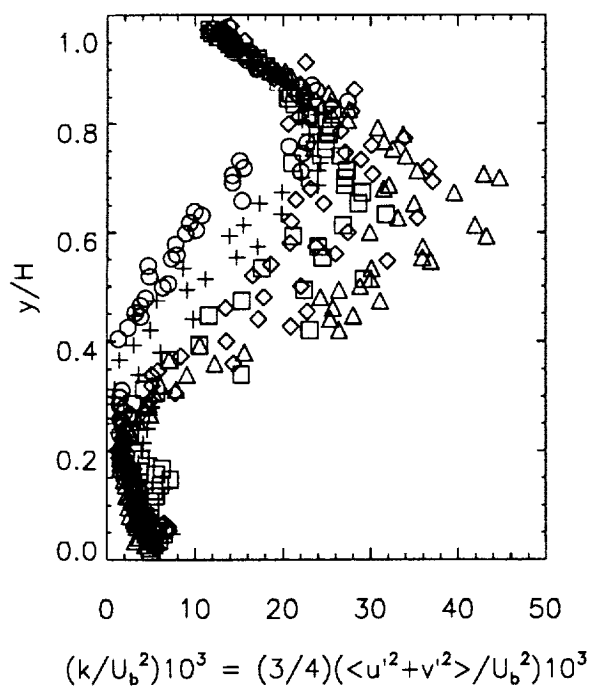
Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)



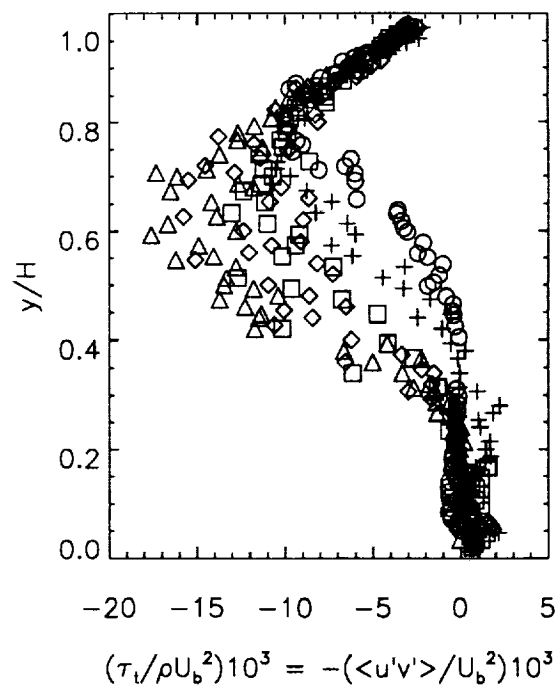
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 9. Summary of Table 9 ($\theta = 90$ deg).

Table 10. LDV flowfield data in TAD ($\theta = 120$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.023	1.629	6.011^{-2}	2.905^{-3}	4.855^{-4}	0.481	1.008	1.035^{-1}	8.272^{-3}	4.293^{-3}
0.030	1.632	6.740^{-2}	2.474^{-3}	5.757^{-4}	0.485	1.006	1.232^{-1}	8.832^{-3}	4.182^{-3}
0.036	1.625	7.272^{-2}	2.195^{-3}	6.346^{-4}	0.501	0.980	1.013^{-1}	1.509^{-2}	6.883^{-3}
0.043	1.616	7.976^{-2}	2.022^{-3}	5.776^{-4}	0.505	0.986	1.321^{-1}	1.074^{-2}	5.207^{-3}
0.050	1.606	8.979^{-2}	2.131^{-3}	5.297^{-4}	0.521	0.961	9.878^{-2}	1.321^{-2}	6.473^{-3}
0.057	1.598	9.202^{-2}	2.687^{-3}	6.694^{-4}	0.525	0.970	1.278^{-1}	8.062^{-3}	3.870^{-3}
0.064	1.588	9.428^{-2}	2.287^{-3}	6.632^{-4}	0.545	0.948	1.280^{-1}	9.380^{-3}	4.636^{-3}
0.071	1.576	1.062^{-1}	2.168^{-3}	5.620^{-4}	0.548	0.927	7.879^{-2}	1.491^{-2}	7.875^{-3}
0.078	1.571	1.094^{-1}	2.213^{-3}	6.317^{-4}	0.565	0.920	1.197^{-1}	1.198^{-2}	6.249^{-3}
0.084	1.553	1.141^{-1}	2.551^{-3}	6.536^{-4}	0.585	0.907	1.105^{-1}	1.360^{-2}	6.279^{-3}
0.091	1.546	1.114^{-1}	2.401^{-3}	5.682^{-4}	0.602	0.890	9.166^{-2}	1.564^{-2}	7.110^{-3}
0.101	1.532	1.142^{-1}	2.233^{-3}	4.615^{-4}	0.605	0.902	1.325^{-1}	1.331^{-2}	6.316^{-3}
0.111	1.520	1.146^{-1}	2.187^{-3}	5.109^{-4}	0.619	0.878	1.068^{-1}	1.421^{-2}	6.870^{-3}
0.121	1.506	1.059^{-1}	2.384^{-3}	5.048^{-4}	0.632	0.878	1.360^{-1}	1.104^{-2}	5.526^{-3}
0.131	1.499	1.103^{-1}	2.488^{-3}	5.845^{-4}	0.645	0.866	1.273^{-1}	1.247^{-2}	6.109^{-3}
0.141	1.481	0.87^{-1}	2.401^{-3}	4.312^{-4}	0.655	0.830	7.402^{-2}	1.833^{-2}	7.783^{-3}
0.150	1.470	9.938^{-2}	2.359^{-3}	5.624^{-4}	0.658	0.856	1.251^{-1}	1.209^{-2}	5.706^{-3}
0.160	1.452	1.098^{-1}	2.068^{-3}	4.209^{-4}	0.671	0.843	9.811^{-2}	1.724^{-2}	6.956^{-3}
0.170	1.441	1.092^{-1}	2.096^{-3}	3.468^{-4}	0.683	0.814	8.239^{-2}	1.769^{-2}	7.803^{-3}
0.180	1.426	1.001^{-1}	1.764^{-3}	3.613^{-4}	0.697	0.805	8.242^{-2}	1.586^{-2}	7.398^{-3}
0.190	1.412	1.089^{-1}	1.883^{-3}	4.291^{-4}	0.710	0.806	9.362^{-2}	1.456^{-2}	6.191^{-3}
0.203	1.388	9.510^{-2}	2.097^{-3}	4.867^{-4}	0.724	0.790	8.101^{-2}	1.441^{-2}	5.902^{-3}
0.216	1.373	1.077^{-1}	1.648^{-3}	3.467^{-4}	0.736	0.768	5.961^{-2}	1.722^{-2}	7.161^{-3}
0.229	1.349	1.015^{-1}	1.513^{-3}	3.267^{-4}	0.747	0.763	5.542^{-2}	1.596^{-2}	6.384^{-3}
0.242	1.330	1.053^{-1}	1.603^{-3}	3.902^{-4}	0.756	0.761	7.212^{-2}	1.328^{-2}	5.624^{-3}
0.255	1.306	9.198^{-2}	2.599^{-3}	6.868^{-4}	0.766	0.756	7.294^{-2}	1.387^{-2}	5.327^{-3}
0.269	1.285	8.747^{-2}	2.401^{-3}	6.652^{-4}	0.776	0.750	7.979^{-2}	1.216^{-2}	5.060^{-3}
0.271	1.276	1.189^{-1}	3.288^{-3}	1.051^{-3}	0.786	0.741	7.035^{-2}	1.120^{-2}	4.650^{-3}
0.282	1.267	8.865^{-2}	1.582^{-3}	3.896^{-4}	0.796	0.741	7.882^{-2}	1.003^{-2}	4.345^{-3}
0.295	1.251	9.863^{-2}	2.221^{-3}	6.108^{-4}	0.806	0.724	6.070^{-2}	1.097^{-2}	4.434^{-3}
0.308	1.231	1.029^{-1}	1.965^{-3}	5.969^{-4}	0.815	0.721	4.774^{-2}	1.046^{-2}	3.647^{-3}
0.325	1.197	1.069^{-1}	5.755^{-3}	2.483^{-3}	0.825	0.715	6.030^{-2}	1.029^{-2}	3.709^{-3}
0.341	1.174	9.414^{-2}	4.636^{-3}	2.041^{-3}	0.835	0.707	3.880^{-2}	1.128^{-2}	3.921^{-3}
0.361	1.160	1.271^{-1}	3.639^{-3}	1.413^{-3}	0.842	0.703	4.625^{-2}	1.039^{-2}	3.713^{-3}
0.379	1.134	1.325^{-1}	6.536^{-3}	2.570^{-3}	0.849	0.693	1.747^{-2}	1.075^{-2}	3.302^{-3}
0.381	1.123	8.803^{-2}	5.613^{-3}	2.833^{-3}	0.856	0.695	1.933^{-2}	1.003^{-2}	2.976^{-3}
0.401	1.109	1.125^{-1}	4.390^{-3}	1.671^{-3}	0.863	0.690	3.606^{-2}	9.623^{-3}	3.094^{-3}
0.421	1.071	9.957^{-2}	7.410^{-3}	3.793^{-3}	0.869	0.685	1.255^{-2}	1.074^{-2}	2.732^{-3}
0.425	1.063	1.325^{-1}	6.114^{-3}	2.733^{-3}	0.876	0.674	1.898^{-3}	1.045^{-2}	2.498^{-3}
0.441	1.049	1.221^{-1}	9.842^{-3}	4.989^{-3}	0.883	0.680	9.514^{-3}	9.985^{-3}	2.398^{-3}
0.445	1.059	1.264^{-1}	4.690^{-3}	1.911^{-3}	0.890	0.675	4.040^{-3}	1.010^{-2}	2.267^{-3}
0.461	1.024	9.502^{-2}	8.747^{-3}	4.494^{-3}	0.897	0.668	9.351^{-3}	1.046^{-2}	2.270^{-3}
0.465	1.039	1.269^{-1}	6.051^{-3}	2.523^{-3}	0.904	0.669	1.913^{-2}	1.035^{-2}	2.271^{-3}

Table 10. Concluded ($\theta = 120$ deg)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	1.509	9.386 ⁻²	5.509 ⁻³	-9.768 ⁻⁴	0.463	1.009	1.228 ⁻¹	9.997 ⁻³	4.786 ⁻³
0.027	1.517	1.017 ⁻¹	5.343 ⁻³	-9.030 ⁻⁴	0.483	0.984	9.456 ⁻²	1.332 ⁻²	6.826 ⁻³
0.034	1.524	1.066 ⁻¹	4.772 ⁻³	-8.560 ⁻⁴	0.498	0.969	7.469 ⁻²	1.188 ⁻²	6.373 ⁻³
0.041	1.527	1.155 ⁻¹	4.884 ⁻³	-8.283 ⁻⁴	0.503	0.956	7.739 ⁻²	1.388 ⁻²	7.381 ⁻³
0.047	1.520	1.176 ⁻¹	4.672 ⁻³	-7.838 ⁻⁴	0.518	0.950	7.869 ⁻²	1.179 ⁻²	6.430 ⁻³
0.054	1.510	1.280 ⁻¹	4.793 ⁻³	-8.917 ⁻⁴	0.523	0.925	7.270 ⁻²	1.516 ⁻²	7.909 ⁻³
0.061	1.519	1.247 ⁻¹	4.419 ⁻³	-5.991 ⁻⁴	0.545	0.916	6.712 ⁻²	1.535 ⁻²	8.658 ⁻³
0.068	1.507	1.345 ⁻¹	4.812 ⁻³	-7.575 ⁻⁴	0.563	0.889	7.046 ⁻²	1.671 ⁻²	8.676 ⁻³
0.075	1.505	1.380 ⁻¹	3.937 ⁻³	-6.500 ⁻⁴	0.572	0.883	4.349 ⁻²	1.837 ⁻²	9.255 ⁻³
0.082	1.496	1.313 ⁻¹	4.246 ⁻³	-6.793 ⁻⁴	0.583	0.875	7.785 ⁻²	1.658 ⁻²	8.726 ⁻³
0.089	1.491	1.306 ⁻¹	3.916 ⁻³	-5.918 ⁻⁴	0.599	0.860	4.510 ⁻²	1.878 ⁻²	9.465 ⁻³
0.098	1.482	1.299 ⁻¹	3.209 ⁻³	-4.332 ⁻⁴	0.603	0.851	6.280 ⁻²	1.875 ⁻²	9.025 ⁻³
0.108	1.488	1.254 ⁻¹	2.899 ⁻³	-4.253 ⁻⁴	0.616	0.843	7.695 ⁻²	1.829 ⁻²	9.252 ⁻³
0.118	1.479	1.275 ⁻¹	2.723 ⁻³	-4.589 ⁻⁴	0.629	0.835	7.564 ⁻²	1.721 ⁻²	8.620 ⁻³
0.128	1.466	1.292 ⁻¹	2.808 ⁻³	-4.611 ⁻⁴	0.642	0.822	5.292 ⁻²	1.932 ⁻²	8.484 ⁻³
0.138	1.439	1.425 ⁻¹	2.677 ⁻³	-4.826 ⁻⁴	0.655	0.815	6.196 ⁻²	1.888 ⁻²	8.393 ⁻³
0.148	1.426	1.441 ⁻¹	2.854 ⁻³	-5.285 ⁻⁴	0.668	0.803	6.067 ⁻²	1.910 ⁻²	8.655 ⁻³
0.157	1.410	1.337 ⁻¹	2.838 ⁻³	-5.175 ⁻⁴	0.680	0.791	4.561 ⁻²	1.883 ⁻²	8.419 ⁻³
0.167	1.402	1.318 ⁻¹	2.657 ⁻³	-4.499 ⁻⁴	0.682	0.793	5.515 ⁻²	1.822 ⁻²	8.082 ⁻³
0.177	1.391	1.384 ⁻¹	1.781 ⁻³	-2.857 ⁻⁴	0.695	0.791	7.570 ⁻²	1.787 ⁻²	8.225 ⁻³
0.187	1.382	1.331 ⁻¹	1.749 ⁻³	-2.285 ⁻⁴	0.707	0.772	5.095 ⁻²	1.715 ⁻²	7.431 ⁻³
0.200	1.362	1.482 ⁻¹	1.735 ⁻³	-2.334 ⁻⁴	0.721	0.765	5.223 ⁻²	1.819 ⁻²	7.899 ⁻³
0.213	1.343	1.311 ⁻¹	2.315 ⁻³	-1.987 ⁻⁴	0.734	0.758	5.699 ⁻²	1.655 ⁻²	6.788 ⁻³
0.226	1.323	1.209 ⁻¹	1.847 ⁻³	-8.260 ⁻⁵	0.744	0.743	2.921 ⁻²	1.866 ⁻²	6.888 ⁻³
0.240	1.305	1.334 ⁻¹	1.958 ⁻³	-1.075 ⁻⁵	0.754	0.738	3.139 ⁻²	1.793 ⁻²	6.600 ⁻³
0.253	1.283	1.217 ⁻¹	2.925 ⁻³	1.937 ⁻⁴	0.760	0.735	2.052 ⁻²	1.681 ⁻²	6.638 ⁻³
0.266	1.261	1.176 ⁻¹	2.432 ⁻³	2.892 ⁻⁴	0.764	0.741	3.848 ⁻²	1.707 ⁻²	6.018 ⁻³
0.268	1.248	1.106 ⁻¹	3.239 ⁻³	2.725 ⁻⁴	0.773	0.728	2.834 ⁻²	1.812 ⁻²	6.146 ⁻³
0.279	1.245	1.372 ⁻¹	1.887 ⁻³	9.433 ⁻⁵	0.783	0.739	6.766 ⁻²	1.464 ⁻²	5.218 ⁻³
0.292	1.231	1.228 ⁻¹	1.842 ⁻³	1.298 ⁻⁴	0.793	0.716	4.137 ⁻²	1.646 ⁻²	5.791 ⁻³
0.295	1.220	1.158 ⁻¹	2.519 ⁻³	1.614 ⁻⁴	0.803	0.711	3.774 ⁻²	1.570 ⁻²	5.210 ⁻³
0.305	1.207	1.119 ⁻¹	2.378 ⁻³	3.405 ⁻⁴	0.813	0.703	1.659 ⁻²	1.690 ⁻²	4.895 ⁻³
0.318	1.196	1.265 ⁻¹	1.735 ⁻³	7.541 ⁻⁵	0.823	0.708	3.968 ⁻²	1.471 ⁻²	4.548 ⁻³
0.322	1.186	1.054 ⁻¹	4.272 ⁻³	1.059 ⁻³	0.832	0.691	1.819 ⁻²	1.454 ⁻²	4.258 ⁻³
0.338	1.163	1.149 ⁻¹	3.614 ⁻³	1.187 ⁻³	0.839	0.699	2.595 ⁻²	1.450 ⁻²	4.335 ⁻³
0.349	1.149	8.267 ⁻²	5.952 ⁻³	1.947 ⁻³	0.846	0.690	3.499 ⁻²	1.396 ⁻²	4.150 ⁻³
0.358	1.135	9.773 ⁻²	3.811 ⁻³	1.288 ⁻³	0.853	0.691	2.827 ⁻²	1.243 ⁻²	3.708 ⁻³
0.376	1.114	1.128 ⁻¹	5.919 ⁻³	2.102 ⁻³	0.860	0.681	6.618 ⁻³	1.272 ⁻²	3.928 ⁻³
0.398	1.084	9.395 ⁻²	5.404 ⁻³	2.446 ⁻³	0.867	0.678	1.080 ⁻²	1.212 ⁻²	3.695 ⁻³
0.403	1.081	1.111 ⁻¹	7.868 ⁻³	3.311 ⁻³	0.874	0.678	1.496 ⁻²	1.201 ⁻²	3.113 ⁻³
0.418	1.058	9.133 ⁻²	8.003 ⁻³	4.224 ⁻³	0.880	0.666	2.910 ⁻²	1.248 ⁻²	2.745 ⁻³
0.423	1.053	9.689 ⁻²	1.045 ⁻²	5.160 ⁻³	0.887	0.648	1.701 ⁻²	1.399 ⁻²	2.145 ⁻³
0.443	1.024	9.248 ⁻²	1.220 ⁻²	6.153 ⁻³	0.894	0.647	1.531 ⁻²	1.201 ⁻²	2.233 ⁻³
0.458	1.010	9.183 ⁻²	9.748 ⁻³	5.124 ⁻³	0.901	0.638	1.459 ⁻²	1.149 ⁻²	2.165 ⁻³

Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)

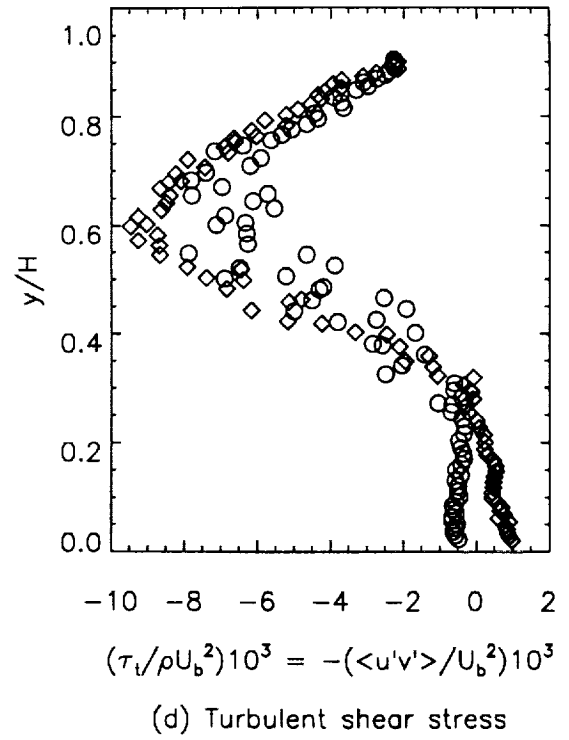
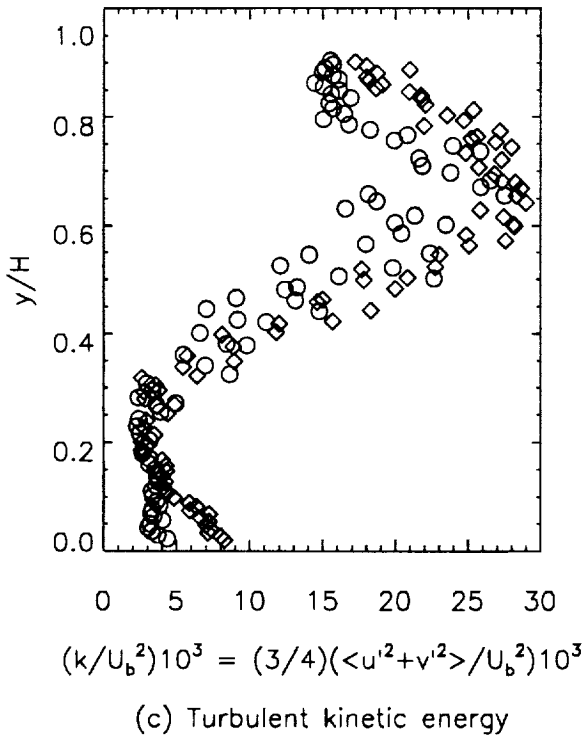
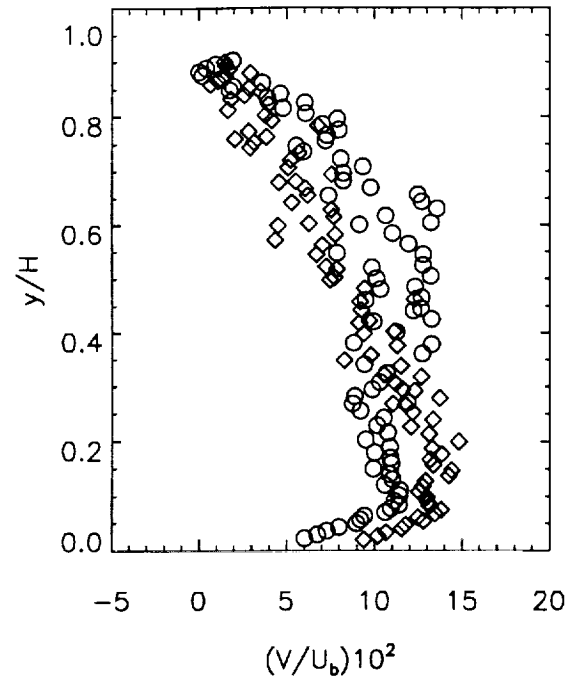
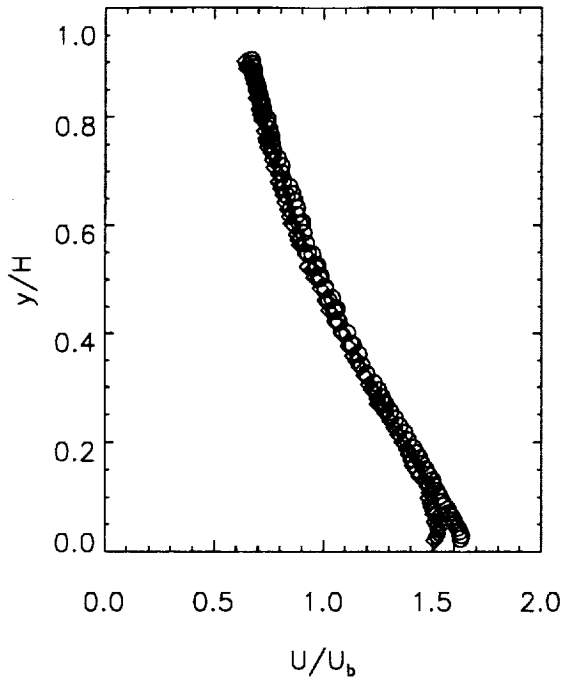


Figure 10. Summary of Table 10 ($\theta = 120$ deg).

Table 11. LDV flowfield data in TAD ($\theta = 150$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

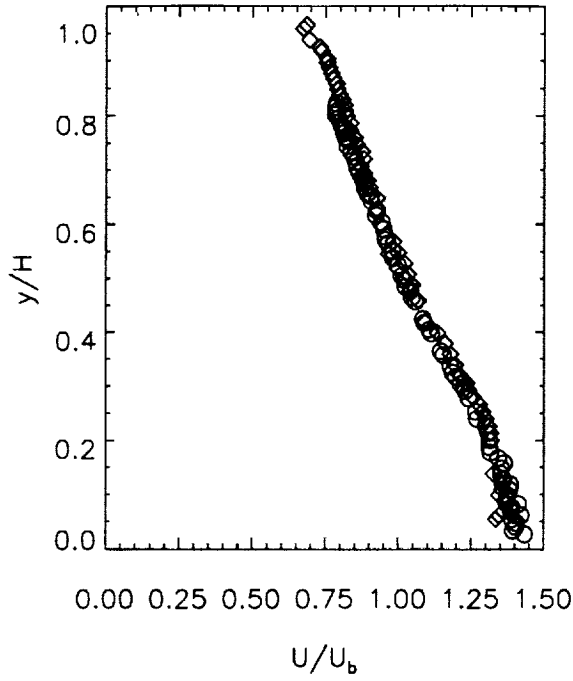
$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.027	1.434	7.940^{-2}	6.506^{-3}	6.787^{-4}	0.477	1.042	2.072^{-1}	6.911^{-3}	2.076^{-3}
0.034	1.394	8.499^{-2}	6.260^{-3}	1.967^{-4}	0.484	1.024	2.010^{-1}	1.018^{-2}	2.784^{-3}
0.041	1.403	9.546^{-2}	5.402^{-3}	-1.832^{-4}	0.497	1.020	2.045^{-1}	9.924^{-3}	3.524^{-3}
0.047	1.405	1.064^{-1}	5.078^{-3}	-2.709^{-4}	0.504	1.010	2.051^{-1}	8.466^{-3}	2.338^{-3}
0.054	1.391	1.172^{-1}	4.511^{-3}	-4.812^{-4}	0.524	0.998	2.226^{-1}	1.228^{-2}	2.709^{-3}
0.061	1.422	1.173^{-1}	4.187^{-3}	-5.052^{-4}	0.537	0.980	2.000^{-1}	1.149^{-2}	2.772^{-3}
0.068	1.387	1.367^{-1}	3.594^{-3}	-7.024^{-4}	0.550	0.979	2.273^{-1}	7.547^{-3}	2.293^{-3}
0.075	1.389	1.429^{-1}	3.259^{-3}	-7.268^{-4}	0.564	0.964	2.112^{-1}	1.102^{-2}	3.194^{-3}
0.082	1.413	1.396^{-1}	4.510^{-3}	-1.114^{-3}	0.570	0.955	2.008^{-1}	1.327^{-2}	3.961^{-3}
0.089	1.374	1.736^{-1}	3.436^{-3}	-9.621^{-4}	0.577	0.955	2.068^{-1}	8.549^{-3}	2.729^{-3}
0.098	1.374	1.732^{-1}	3.244^{-3}	-7.886^{-4}	0.590	0.949	2.140^{-1}	8.665^{-3}	2.778^{-3}
0.108	1.382	1.721^{-1}	4.272^{-3}	-1.417^{-3}	0.603	0.942	2.118^{-1}	7.847^{-3}	2.307^{-3}
0.118	1.385	1.717^{-1}	4.740^{-3}	-1.503^{-3}	0.616	0.920	1.767^{-1}	1.119^{-2}	3.857^{-3}
0.128	1.359	1.904^{-1}	3.434^{-3}	-9.072^{-4}	0.624	0.926	2.174^{-1}	1.138^{-2}	3.476^{-3}
0.138	1.351	2.000^{-1}	3.216^{-3}	-8.466^{-4}	0.642	0.906	1.902^{-1}	1.209^{-2}	3.404^{-3}
0.148	1.353	1.936^{-1}	3.336^{-3}	-8.028^{-4}	0.651	0.905	2.013^{-1}	1.425^{-2}	3.531^{-3}
0.157	1.364	1.844^{-1}	4.857^{-3}	-9.819^{-4}	0.656	0.892	1.769^{-1}	1.080^{-2}	3.305^{-3}
0.167	1.343	1.961^{-1}	4.244^{-3}	-6.985^{-4}	0.665	0.884	1.793^{-1}	1.144^{-2}	4.105^{-3}
0.177	1.316	2.176^{-1}	2.476^{-3}	-5.147^{-4}	0.675	0.883	1.849^{-1}	1.257^{-2}	3.415^{-3}
0.187	1.313	2.157^{-1}	3.367^{-3}	-6.499^{-4}	0.678	0.880	1.904^{-1}	1.171^{-2}	3.595^{-3}
0.200	1.313	2.066^{-1}	3.467^{-3}	-4.804^{-4}	0.685	0.874	1.815^{-1}	1.073^{-2}	3.577^{-3}
0.213	1.309	2.037^{-1}	5.219^{-3}	-1.034^{-4}	0.695	0.865	1.699^{-1}	1.231^{-2}	3.712^{-3}
0.226	1.301	1.900^{-1}	5.233^{-3}	4.076^{-4}	0.705	0.856	1.607^{-1}	1.462^{-2}	3.760^{-3}
0.240	1.269	2.247^{-1}	2.607^{-3}	-2.844^{-4}	0.714	0.852	1.742^{-1}	1.225^{-2}	3.430^{-3}
0.253	1.266	2.019^{-1}	4.840^{-3}	3.526^{-4}	0.724	0.846	1.592^{-1}	1.180^{-2}	3.256^{-3}
0.277	1.242	2.035^{-1}	3.729^{-3}	2.948^{-4}	0.732	0.838	1.359^{-1}	1.705^{-2}	4.292^{-3}
0.290	1.229	2.167^{-1}	3.673^{-3}	4.728^{-4}	0.734	0.837	1.383^{-1}	1.372^{-2}	3.696^{-3}
0.297	1.224	2.409^{-1}	3.670^{-3}	5.822^{-4}	0.744	0.823	1.131^{-1}	1.482^{-2}	4.312^{-3}
0.304	1.213	2.134^{-1}	4.777^{-3}	8.940^{-4}	0.754	0.828	1.241^{-1}	1.260^{-2}	3.068^{-3}
0.317	1.197	2.020^{-1}	5.839^{-3}	1.496^{-3}	0.758	0.818	1.421^{-1}	1.493^{-2}	4.176^{-3}
0.324	1.186	2.273^{-1}	4.283^{-3}	8.137^{-4}	0.761	0.818	1.033^{-1}	1.335^{-2}	3.775^{-3}
0.337	1.178	2.039^{-1}	4.912^{-3}	1.157^{-3}	0.768	0.811	9.013^{-2}	1.358^{-2}	4.047^{-3}
0.357	1.153	2.259^{-1}	6.978^{-3}	1.421^{-3}	0.774	0.812	9.694^{-2}	1.229^{-2}	3.481^{-3}
0.364	1.144	2.074^{-1}	6.478^{-3}	1.839^{-3}	0.781	0.804	7.193^{-2}	1.387^{-2}	3.689^{-3}
0.397	1.112	2.081^{-1}	8.238^{-3}	2.478^{-3}	0.788	0.798	3.353^{-2}	1.596^{-2}	3.330^{-3}
0.404	1.105	2.246^{-1}	6.808^{-3}	1.733^{-3}	0.795	0.793	4.764^{-2}	1.567^{-2}	3.253^{-3}
0.417	1.088	1.985^{-1}	1.104^{-2}	3.316^{-3}	0.802	0.782	3.297^{-2}	1.665^{-2}	3.453^{-3}
0.424	1.083	2.313^{-1}	6.597^{-3}	1.397^{-3}	0.809	0.789	5.859^{-2}	1.551^{-2}	3.084^{-3}
0.457	1.058	2.097^{-1}	1.002^{-2}	3.016^{-3}	0.816	0.784	4.762^{-2}	1.527^{-2}	3.433^{-3}
0.464	1.045	2.245^{-1}	1.040^{-2}	2.771^{-3}	0.822	0.786	4.972^{-2}	1.685^{-2}	3.427^{-3}

Table 11. Concluded ($\theta = 150$ deg)

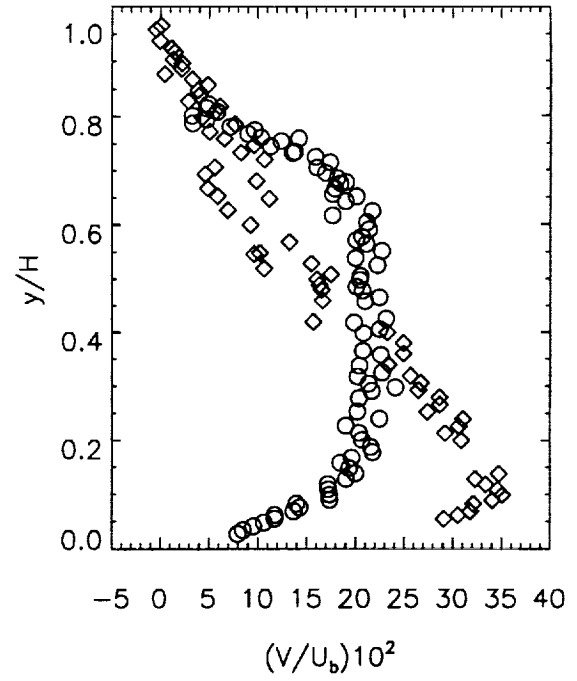
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.054	1.335	2.909 ⁻¹	1.816 ⁻²	-2.413 ⁻⁴	0.547	0.999	1.021 ⁻¹	2.978 ⁻²	7.821 ⁻³
0.061	1.346	3.054 ⁻¹	1.360 ⁻²	-1.811 ⁻³	0.567	0.983	1.326 ⁻¹	2.473 ⁻²	6.848 ⁻³
0.068	1.361	3.181 ⁻¹	1.430 ⁻²	-1.163 ⁻³	0.599	0.937	9.245 ⁻²	2.666 ⁻²	5.721 ⁻³
0.082	1.371	3.212 ⁻¹	1.043 ⁻²	-2.013 ⁻³	0.627	0.925	6.939 ⁻²	2.828 ⁻²	6.042 ⁻³
0.089	1.367	3.408 ⁻¹	1.026 ⁻²	-1.409 ⁻³	0.647	0.926	1.118 ⁻¹	2.144 ⁻²	5.610 ⁻³
0.098	1.346	3.508 ⁻¹	7.347 ⁻³	-7.895 ⁻⁴	0.653	0.898	5.897 ⁻²	2.795 ⁻²	5.837 ⁻³
0.108	1.356	3.463 ⁻¹	8.736 ⁻³	-1.625 ⁻³	0.667	0.900	4.867 ⁻²	2.563 ⁻²	4.739 ⁻³
0.118	1.356	3.339 ⁻¹	7.494 ⁻³	-1.799 ⁻³	0.680	0.894	9.866 ⁻²	2.256 ⁻²	5.324 ⁻³
0.128	1.361	3.231 ⁻¹	7.650 ⁻³	-1.357 ⁻³	0.694	0.882	4.623 ⁻²	2.471 ⁻²	5.614 ⁻³
0.138	1.327	3.474 ⁻¹	7.504 ⁻³	-3.200 ⁻⁴	0.707	0.870	5.615 ⁻²	2.301 ⁻²	4.969 ⁻³
0.200	1.318	3.090 ⁻¹	8.326 ⁻³	4.065 ⁻⁴	0.720	0.880	1.069 ⁻¹	1.868 ⁻²	3.950 ⁻³
0.213	1.316	2.923 ⁻¹	7.741 ⁻³	5.116 ⁻⁴	0.733	0.874	8.290 ⁻²	1.867 ⁻²	3.527 ⁻³
0.226	1.310	3.065 ⁻¹	5.338 ⁻³	3.448 ⁻⁵	0.746	0.858	9.641 ⁻²	1.765 ⁻²	4.316 ⁻³
0.240	1.300	3.107 ⁻¹	5.900 ⁻³	3.157 ⁻⁴	0.759	0.850	6.610 ⁻²	1.832 ⁻²	3.693 ⁻³
0.253	1.289	2.740 ⁻¹	7.007 ⁻³	1.324 ⁻³	0.773	0.834	5.089 ⁻²	1.749 ⁻²	3.594 ⁻³
0.266	1.278	2.868 ⁻¹	7.358 ⁻³	1.451 ⁻³	0.786	0.835	7.683 ⁻²	1.412 ⁻²	3.296 ⁻³
0.279	1.256	2.864 ⁻¹	9.254 ⁻³	2.392 ⁻³	0.799	0.822	4.324 ⁻²	1.526 ⁻²	3.139 ⁻³
0.292	1.241	2.647 ⁻¹	9.300 ⁻³	2.947 ⁻³	0.809	0.816	5.647 ⁻²	1.405 ⁻²	3.016 ⁻³
0.306	1.234	2.672 ⁻¹	1.109 ⁻²	3.120 ⁻³	0.818	0.814	6.132 ⁻²	1.377 ⁻²	3.024 ⁻³
0.318	1.212	2.565 ⁻¹	1.025 ⁻²	3.699 ⁻³	0.828	0.807	2.902 ⁻²	1.467 ⁻²	2.845 ⁻³
0.338	1.194	2.337 ⁻¹	1.104 ⁻²	4.370 ⁻³	0.838	0.797	3.982 ⁻²	1.327 ⁻²	2.519 ⁻³
0.359	1.178	2.492 ⁻¹	1.317 ⁻²	4.240 ⁻³	0.848	0.790	3.885 ⁻²	1.200 ⁻²	2.342 ⁻³
0.378	1.160	2.492 ⁻¹	1.148 ⁻²	4.177 ⁻³	0.858	0.787	4.908 ⁻²	1.135 ⁻²	2.292 ⁻³
0.398	1.134	2.327 ⁻¹	1.234 ⁻²	4.129 ⁻³	0.868	0.775	3.303 ⁻²	1.122 ⁻²	1.925 ⁻³
0.418	1.092	1.567 ⁻¹	2.340 ⁻²	7.956 ⁻³	0.877	0.769	4.538 ⁻³	1.099 ⁻²	2.409 ⁻³
0.458	1.068	1.663 ⁻¹	2.185 ⁻²	6.369 ⁻³	0.887	0.761	2.213 ⁻²	1.001 ⁻²	2.335 ⁻³
0.478	1.041	1.654 ⁻¹	2.140 ⁻²	7.673 ⁻³	0.897	0.754	2.225 ⁻²	9.818 ⁻³	2.129 ⁻³
0.487	1.048	1.631 ⁻¹	2.782 ⁻²	7.538 ⁻³	0.904	0.754	1.324 ⁻²	1.086 ⁻²	2.275 ⁻³
0.498	1.026	1.607 ⁻¹	2.199 ⁻²	7.804 ⁻³	0.918	0.734	1.473 ⁻²	9.861 ⁻³	2.595 ⁻³
0.507	1.033	1.748 ⁻¹	2.551 ⁻²	7.654 ⁻³	0.925	0.730	1.177 ⁻²	9.293 ⁻³	2.626 ⁻³
0.518	0.998	1.065 ⁻¹	2.993 ⁻²	7.808 ⁻³	0.938	0.694	-5.027 ⁻⁴	1.133 ⁻²	3.990 ⁻³
0.527	1.021	1.550 ⁻¹	2.359 ⁻²	7.417 ⁻³	0.959	0.674	-4.422 ⁻³	1.113 ⁻²	4.157 ⁻³
0.545	0.966	9.612 ⁻²	2.890 ⁻²	7.321 ⁻³	0.966	0.684	8.484 ⁻⁴	8.871 ⁻³	3.100 ⁻³

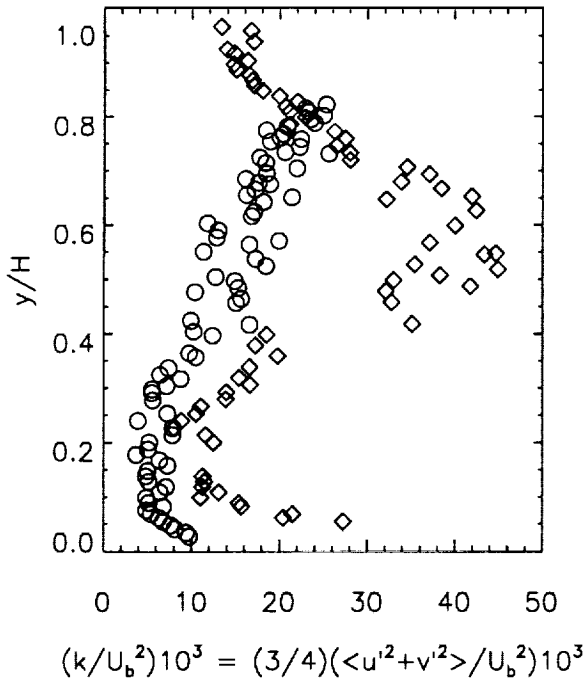
Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)



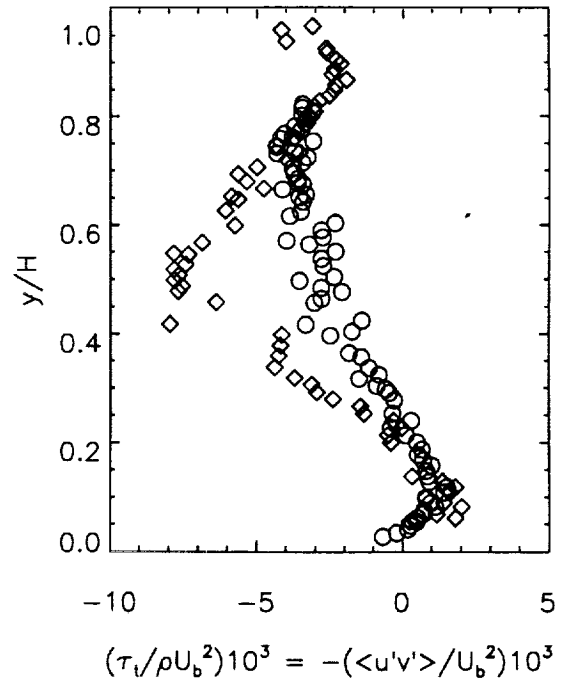
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 11. Summary of Table 11 ($\theta = 150$ deg).

Table 12. LDV flowfield data in TAD ($\theta = 180$ deg)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.158	-1.638 ⁻²	2.291 ⁻²	6.203 ⁻³	0.500	1.097	4.120 ⁻¹	8.602 ⁻³	3.887 ⁻⁴
0.027	-0.100	-5.528 ⁻³	4.194 ⁻²	9.809 ⁻³	0.520	1.087	4.065 ⁻¹	8.033 ⁻³	4.813 ⁻⁴
0.033	0.407	5.806 ⁻²	1.805 ⁻¹	2.940 ⁻²	0.530	1.069	3.679 ⁻¹	1.474 ⁻²	4.699 ⁻⁴
0.040	1.030	1.294 ⁻¹	1.097 ⁻¹	1.091 ⁻²	0.547	1.074	3.796 ⁻¹	1.394 ⁻²	1.612 ⁻⁴
0.047	1.073	1.561 ⁻¹	8.737 ⁻²	1.225 ⁻²	0.570	1.052	3.911 ⁻¹	8.594 ⁻³	1.164 ⁻³
0.053	1.041	1.790 ⁻¹	9.133 ⁻²	1.407 ⁻²	0.573	1.066	3.651 ⁻¹	1.614 ⁻²	1.140 ⁻⁴
0.060	1.211	2.093 ⁻¹	2.650 ⁻²	2.938 ⁻³	0.600	1.052	3.665 ⁻¹	1.227 ⁻²	6.108 ⁻⁴
0.067	1.192	2.310 ⁻¹	3.020 ⁻²	2.919 ⁻³	0.627	1.038	3.622 ⁻¹	1.096 ⁻²	6.046 ⁻⁴
0.073	1.257	2.417 ⁻¹	1.637 ⁻²	-4.256 ⁻⁴	0.630	1.030	3.590 ⁻¹	1.109 ⁻²	3.615 ⁻⁴
0.080	1.255	2.675 ⁻¹	1.184 ⁻²	-1.641 ⁻³	0.650	1.023	3.607 ⁻¹	7.880 ⁻³	6.576 ⁻⁴
0.087	1.239	2.864 ⁻¹	1.497 ⁻²	-2.095 ⁻³	0.653	1.029	3.191 ⁻¹	1.489 ⁻²	8.960 ⁻⁴
0.097	1.263	3.034 ⁻¹	1.165 ⁻²	-2.279 ⁻³	0.670	1.011	3.217 ⁻¹	1.384 ⁻²	-1.215 ⁻⁴
0.107	1.229	3.316 ⁻¹	9.672 ⁻³	-2.054 ⁻³	0.683	1.008	3.446 ⁻¹	8.700 ⁻³	7.875 ⁻⁴
0.127	1.193	3.893 ⁻¹	6.932 ⁻³	-1.777 ⁻³	0.697	1.002	3.259 ⁻¹	9.407 ⁻³	9.101 ⁻⁴
0.137	1.219	3.844 ⁻¹	7.595 ⁻³	-2.494 ⁻³	0.710	0.994	3.116 ⁻¹	1.162 ⁻²	6.364 ⁻⁴
0.147	1.209	4.085 ⁻¹	6.356 ⁻³	-2.273 ⁻³	0.723	0.994	2.808 ⁻¹	1.435 ⁻²	-3.135 ⁻⁴
0.157	1.200	4.198 ⁻¹	5.813 ⁻³	-2.124 ⁻³	0.733	1.001	2.917 ⁻¹	1.306 ⁻²	3.554 ⁻⁴
0.167	1.190	4.365 ⁻¹	4.663 ⁻³	-1.597 ⁻³	0.737	0.988	3.103 ⁻¹	8.323 ⁻³	1.135 ⁻³
0.177	1.222	4.113 ⁻¹	7.403 ⁻³	-2.887 ⁻³	0.750	0.983	2.727 ⁻¹	1.254 ⁻²	-2.046 ⁻⁴
0.187	1.213	4.341 ⁻¹	4.901 ⁻³	-1.590 ⁻³	0.760	0.993	2.587 ⁻¹	1.311 ⁻²	9.437 ⁻⁴
0.200	1.225	4.298 ⁻¹	5.046 ⁻³	-1.535 ⁻³	0.763	0.978	2.842 ⁻¹	9.608 ⁻³	7.384 ⁻⁴
0.227	1.210	4.478 ⁻¹	5.508 ⁻³	-1.119 ⁻³	0.777	0.976	2.693 ⁻¹	9.013 ⁻³	9.523 ⁻⁴
0.240	1.210	4.399 ⁻¹	4.134 ⁻³	-1.011 ⁻³	0.790	0.970	2.348 ⁻¹	1.342 ⁻²	2.863 ⁻⁴
0.253	1.206	4.376 ⁻¹	5.871 ⁻³	-9.167 ⁻⁴	0.803	0.965	2.472 ⁻¹	8.200 ⁻³	7.524 ⁻⁴
0.267	1.192	4.485 ⁻¹	3.606 ⁻³	-9.951 ⁻⁴	0.813	0.965	2.116 ⁻¹	1.150 ⁻²	-4.144 ⁻⁴
0.280	1.191	4.445 ⁻¹	5.672 ⁻³	-1.290 ⁻³	0.823	0.962	1.926 ⁻¹	1.090 ⁻²	2.592 ⁻⁴
0.283	1.198	4.455 ⁻¹	9.033 ⁻³	-3.085 ⁻⁴	0.833	0.957	2.122 ⁻¹	7.946 ⁻³	6.808 ⁻⁴
0.293	1.190	4.463 ⁻¹	6.171 ⁻³	-7.693 ⁻⁴	0.843	0.957	1.900 ⁻¹	9.013 ⁻³	5.599 ⁻⁴
0.307	1.189	4.496 ⁻¹	4.420 ⁻³	-4.369 ⁻⁴	0.853	0.952	1.903 ⁻¹	8.122 ⁻³	3.846 ⁻⁴
0.310	1.191	4.218 ⁻¹	1.092 ⁻²	-8.309 ⁻⁵	0.863	0.951	1.621 ⁻¹	8.688 ⁻³	1.308 ⁻⁴
0.320	1.181	4.418 ⁻¹	6.333 ⁻³	-2.168 ⁻⁴	0.873	0.950	1.235 ⁻¹	1.023 ⁻²	-8.596 ⁻⁵
0.337	1.173	4.322 ⁻¹	9.874 ⁻³	1.332 ⁻⁴	0.883	0.947	1.260 ⁻¹	7.708 ⁻³	3.583 ⁻⁴
0.340	1.181	4.269 ⁻¹	7.573 ⁻³	2.235 ⁻⁴	0.893	0.944	1.149 ⁻¹	7.630 ⁻³	1.257 ⁻⁴
0.360	1.168	4.295 ⁻¹	8.525 ⁻³	-1.730 ⁻⁴	0.903	0.943	7.863 ⁻²	7.839 ⁻³	5.573 ⁻⁴
0.380	1.155	4.103 ⁻¹	1.227 ⁻²	4.400 ⁻⁴	0.910	0.940	8.721 ⁻²	7.267 ⁻³	3.808 ⁻⁴
0.390	1.146	4.351 ⁻¹	9.698 ⁻³	5.227 ⁻⁴	0.917	0.937	7.467 ⁻²	7.201 ⁻³	6.383 ⁻⁴
0.400	1.149	4.265 ⁻¹	8.069 ⁻³	-2.017 ⁻⁴	0.923	0.933	8.147 ⁻²	6.329 ⁻³	4.739 ⁻⁴
0.417	1.135	4.006 ⁻¹	1.365 ⁻²	-3.654 ⁻⁴	0.930	0.937	8.374 ⁻²	6.129 ⁻³	4.077 ⁻⁴
0.440	1.126	4.166 ⁻¹	1.171 ⁻²	6.225 ⁻⁵	0.937	0.930	7.632 ⁻²	6.480 ⁻³	6.307 ⁻⁴
0.443	1.120	4.100 ⁻¹	1.172 ⁻²	4.077 ⁻⁵	0.943	0.922	6.450 ⁻²	6.259 ⁻³	9.228 ⁻⁴
0.460	1.116	4.097 ⁻¹	1.193 ⁻²	-3.223 ⁻⁴	0.950	0.916	5.367 ⁻²	5.199 ⁻³	8.722 ⁻⁴
0.470	1.104	3.807 ⁻¹	1.174 ⁻²	6.923 ⁻⁴	0.957	0.910	4.799 ⁻²	5.458 ⁻³	1.125 ⁻³
0.480	1.107	4.202 ⁻¹	7.663 ⁻³	2.639 ⁻⁴	0.963	0.899	4.496 ⁻²	4.886 ⁻³	1.045 ⁻³
0.490	1.094	4.028 ⁻¹	1.362 ⁻²	-5.999 ⁻⁴	0.970	0.878	3.853 ⁻²	5.231 ⁻³	1.762 ⁻³

Table 12. Continued ($\theta = 180$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.224	-1.522 ⁻³	2.381 ⁻²	1.544 ⁻³	0.480	1.232	3.711 ⁻¹	2.390 ⁻²	6.899 ⁻⁵
0.027	-0.254	8.330 ⁻⁴	2.424 ⁻²	2.587 ⁻⁴	0.487	1.227	3.750 ⁻¹	3.103 ⁻²	1.359 ⁻³
0.033	-0.242	9.487 ⁻³	2.677 ⁻²	5.454 ⁻⁴	0.507	1.218	3.620 ⁻¹	2.984 ⁻²	1.821 ⁻³
0.040	-0.252	6.789 ⁻³	3.056 ⁻²	-1.481 ⁻³	0.520	1.209	3.678 ⁻¹	2.232 ⁻²	-8.663 ⁻⁵
0.047	-0.223	2.095 ⁻²	4.481 ⁻²	1.422 ⁻⁴	0.547	1.199	3.333 ⁻¹	3.069 ⁻²	-8.165 ⁻⁴
0.053	-0.172	2.520 ⁻²	4.798 ⁻²	-4.052 ⁻⁴	0.573	1.182	3.280 ⁻¹	2.592 ⁻²	-8.849 ⁻⁴
0.060	-0.195	3.286 ⁻²	4.556 ⁻²	8.217 ⁻⁴	0.587	1.179	3.111 ⁻¹	3.358 ⁻²	1.001 ⁻⁴
0.067	-0.076	5.668 ⁻²	7.067 ⁻²	3.767 ⁻³	0.607	1.174	3.163 ⁻¹	2.853 ⁻²	-1.251 ⁻⁴
0.073	-0.132	3.891 ⁻²	5.599 ⁻²	-1.090 ⁻³	0.627	1.158	2.763 ⁻¹	3.195 ⁻²	-1.347 ⁻³
0.080	-0.015	6.997 ⁻²	1.064 ⁻¹	1.771 ⁻²	0.647	1.154	2.717 ⁻¹	3.031 ⁻²	-4.824 ⁻⁴
0.087	0.121	1.113 ⁻¹	1.489 ⁻¹	3.894 ⁻²	0.667	1.147	2.735 ⁻¹	2.954 ⁻²	-7.544 ⁻⁴
0.097	0.380	1.916 ⁻¹	2.076 ⁻¹	7.372 ⁻²	0.680	1.136	2.755 ⁻¹	2.862 ⁻²	-1.820 ⁻³
0.107	0.242	1.674 ⁻¹	1.454 ⁻¹	2.696 ⁻²	0.693	1.132	2.739 ⁻¹	2.663 ⁻²	-3.594 ⁻⁴
0.117	0.553	2.554 ⁻¹	1.861 ⁻¹	5.497 ⁻²	0.720	1.127	2.621 ⁻¹	2.514 ⁻²	-1.128 ⁻³
0.127	0.549	2.622 ⁻¹	1.911 ⁻¹	6.090 ⁻²	0.733	1.121	2.037 ⁻¹	2.778 ⁻²	-2.100 ⁻³
0.137	1.025	4.044 ⁻¹	1.177 ⁻¹	4.187 ⁻²	0.747	1.123	2.251 ⁻¹	2.537 ⁻²	-1.300 ⁻³
0.147	0.992	4.068 ⁻¹	1.283 ⁻¹	4.162 ⁻²	0.760	1.110	2.039 ⁻¹	2.367 ⁻²	-8.818 ⁻⁴
0.157	1.155	4.799 ⁻¹	7.900 ⁻²	2.282 ⁻²	0.773	1.108	1.781 ⁻¹	2.473 ⁻²	-1.398 ⁻³
0.167	1.076	4.569 ⁻¹	9.020 ⁻²	2.366 ⁻²	0.787	1.106	2.017 ⁻¹	2.068 ⁻²	-5.092 ⁻⁴
0.177	1.291	5.436 ⁻¹	3.126 ⁻²	5.362 ⁻³	0.800	1.103	1.547 ⁻¹	2.135 ⁻²	-1.864 ⁻³
0.187	1.286	5.479 ⁻¹	3.291 ⁻²	4.024 ⁻³	0.810	1.097	1.559 ⁻¹	2.031 ⁻²	-8.143 ⁻⁴
0.200	1.273	5.155 ⁻¹	3.402 ⁻²	3.143 ⁻⁴	0.820	1.089	1.930 ⁻¹	1.771 ⁻²	-9.170 ⁻⁴
0.213	1.286	5.523 ⁻¹	1.932 ⁻²	-1.272 ⁻³	0.830	1.090	1.576 ⁻¹	1.677 ⁻²	-6.889 ⁻⁴
0.227	1.306	5.709 ⁻¹	2.013 ⁻²	-2.795 ⁻⁵	0.840	1.086	1.387 ⁻¹	1.675 ⁻²	-9.653 ⁻⁴
0.240	1.333	5.567 ⁻¹	1.369 ⁻²	-1.712 ⁻³	0.850	1.078	1.315 ⁻¹	1.490 ⁻²	-2.416 ⁻⁴
0.253	1.306	5.672 ⁻¹	1.773 ⁻²	-5.972 ⁻⁴	0.860	1.071	1.187 ⁻¹	1.546 ⁻²	-3.862 ⁻⁴
0.267	1.284	5.734 ⁻¹	1.093 ⁻²	-1.894 ⁻³	0.870	1.071	8.960 ⁻²	1.519 ⁻²	-5.961 ⁻⁴
0.280	1.309	5.673 ⁻¹	1.302 ⁻²	6.793 ⁻⁵	0.880	1.065	1.126 ⁻¹	1.321 ⁻²	-5.264 ⁻⁴
0.293	1.296	5.800 ⁻¹	9.074 ⁻³	-1.655 ⁻³	0.890	1.059	9.860 ⁻²	1.075 ⁻²	1.518 ⁻⁴
0.307	1.299	5.485 ⁻¹	1.538 ⁻²	-7.135 ⁻⁵	0.900	1.058	8.510 ⁻²	1.085 ⁻²	5.971 ⁻⁵
0.320	1.309	5.389 ⁻¹	1.098 ⁻²	-4.905 ⁻⁴	0.907	1.057	5.976 ⁻²	1.252 ⁻²	9.085 ⁻⁴
0.340	1.300	5.295 ⁻¹	1.071 ⁻²	-5.949 ⁻⁴	0.913	1.049	6.081 ⁻²	1.030 ⁻²	4.127 ⁻⁴
0.380	1.286	4.847 ⁻¹	1.216 ⁻²	6.689 ⁻⁴	0.920	1.047	5.798 ⁻²	8.848 ⁻³	4.197 ⁻⁴
0.400	1.273	4.415 ⁻¹	1.762 ⁻²	1.078 ⁻³	0.927	1.049	6.118 ⁻²	8.417 ⁻³	5.340 ⁻⁴
0.420	1.267	4.445 ⁻¹	1.592 ⁻²	1.053 ⁻³	0.933	1.048	4.595 ⁻²	7.303 ⁻³	7.550 ⁻⁴
0.440	1.250	3.951 ⁻¹	2.789 ⁻²	2.283 ⁻³	0.940	1.044	4.669 ⁻²	6.350 ⁻³	4.804 ⁻⁴

Table 12. Continued ($\theta = 180$ deg)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.211	2.795 ⁻³	2.178 ⁻²	2.499 ⁻³	0.500	1.204	3.168 ⁻¹	3.511 ⁻²	-9.084 ⁻⁴
0.027	-0.200	-2.863 ⁻⁴	2.395 ⁻²	1.709 ⁻³	0.520	1.215	2.293 ⁻¹	4.419 ⁻²	-3.832 ⁻³
0.033	-0.221	9.734 ⁻³	2.850 ⁻²	2.053 ⁻³	0.540	1.199	2.984 ⁻¹	3.692 ⁻²	-2.248 ⁻³
0.040	-0.184	1.203 ⁻²	3.728 ⁻²	3.262 ⁻³	0.560	1.197	2.229 ⁻¹	4.432 ⁻²	-4.864 ⁻³
0.047	-0.184	2.268 ⁻²	3.990 ⁻²	1.251 ⁻³	0.580	1.191	2.328 ⁻¹	4.056 ⁻²	-4.470 ⁻³
0.053	-0.154	2.659 ⁻²	4.604 ⁻²	1.632 ⁻³	0.600	1.165	2.108 ⁻¹	3.833 ⁻²	-3.167 ⁻³
0.060	-0.098	5.035 ⁻²	6.901 ⁻²	7.315 ⁻³	0.620	1.179	1.292 ⁻¹	3.842 ⁻²	-5.035 ⁻³
0.073	-0.032	6.708 ⁻²	8.689 ⁻²	1.274 ⁻²	0.627	1.144	2.936 ⁻¹	3.155 ⁻²	-1.891 ⁻³
0.080	-0.034	8.167 ⁻²	9.334 ⁻²	1.332 ⁻²	0.640	1.175	8.256 ⁻²	3.686 ⁻²	-5.193 ⁻³
0.087	0.089	1.098 ⁻¹	1.246 ⁻¹	2.801 ⁻²	0.653	1.135	2.227 ⁻¹	3.372 ⁻²	-3.489 ⁻³
0.097	0.465	2.273 ⁻¹	2.256 ⁻¹	8.694 ⁻²	0.660	1.182	2.880 ⁻²	3.484 ⁻²	-4.139 ⁻³
0.107	0.769	3.110 ⁻¹	2.208 ⁻¹	9.273 ⁻²	0.673	1.161	8.790 ⁻²	3.515 ⁻²	-2.771 ⁻³
0.117	0.744	3.248 ⁻¹	2.148 ⁻¹	8.256 ⁻²	0.687	1.167	5.954 ⁻²	3.064 ⁻²	-3.906 ⁻³
0.127	0.850	3.710 ⁻¹	1.850 ⁻¹	7.685 ⁻²	0.700	1.139	1.328 ⁻¹	3.306 ⁻²	-3.711 ⁻³
0.137	1.100	4.630 ⁻¹	1.158 ⁻¹	4.441 ⁻²	0.707	1.118	2.029 ⁻¹	3.305 ⁻²	-3.169 ⁻³
0.147	1.035	4.410 ⁻¹	1.277 ⁻¹	4.280 ⁻²	0.713	1.142	6.328 ⁻²	3.015 ⁻²	-3.385 ⁻³
0.157	1.254	5.152 ⁻¹	5.007 ⁻²	8.030 ⁻³	0.727	1.139	4.973 ⁻²	2.575 ⁻²	-2.578 ⁻³
0.167	1.307	5.326 ⁻¹	3.106 ⁻²	4.301 ⁻³	0.740	1.134	-4.331 ⁻³	2.150 ⁻²	-1.432 ⁻³
0.177	1.245	5.275 ⁻¹	4.571 ⁻²	7.892 ⁻³	0.753	1.140	6.136 ⁻³	2.136 ⁻²	-1.292 ⁻³
0.187	1.310	5.523 ⁻¹	2.192 ⁻²	-1.267 ⁻³	0.767	1.134	-1.429 ⁻²	1.921 ⁻²	-4.602 ⁻⁴
0.200	1.289	5.459 ⁻¹	2.999 ⁻²	1.353 ⁻³	0.780	1.117	8.448 ⁻³	2.063 ⁻²	-7.877 ⁻⁴
0.213	1.293	5.765 ⁻¹	1.986 ⁻²	-1.561 ⁻⁴	0.793	1.113	4.563 ⁻²	1.975 ⁻²	-1.208 ⁻³
0.220	1.348	5.872 ⁻¹	1.405 ⁻²	-2.512 ⁻⁴	0.803	1.096	9.864 ⁻²	2.127 ⁻²	-1.307 ⁻³
0.227	1.327	5.228 ⁻¹	2.617 ⁻²	-2.988 ⁻³	0.813	1.110	2.000 ⁻²	1.998 ⁻²	-4.051 ⁻⁴
0.240	1.299	5.766 ⁻¹	2.269 ⁻²	-2.138 ⁻³	0.823	1.099	8.896 ⁻³	1.697 ⁻²	-1.623 ⁻⁴
0.247	1.353	5.487 ⁻¹	1.683 ⁻²	4.521 ⁻⁴	0.833	1.103	2.813 ⁻²	1.304 ⁻²	-1.016 ⁻⁴
0.253	1.312	5.704 ⁻¹	1.454 ⁻²	-2.109 ⁻³	0.843	1.094	3.103 ⁻³	1.244 ⁻²	1.808 ⁻⁴
0.267	1.307	5.737 ⁻¹	1.397 ⁻²	-1.997 ⁻³	0.853	1.090	1.008 ⁻²	1.287 ⁻²	3.584 ⁻⁴
0.273	1.337	5.259 ⁻¹	1.706 ⁻²	1.305 ⁻⁴	0.863	1.083	1.195 ⁻²	1.291 ⁻²	3.276 ⁻⁴
0.280	1.319	5.298 ⁻¹	2.060 ⁻²	-2.319 ⁻³	0.873	1.068	5.915 ⁻²	1.171 ⁻²	-2.180 ⁻⁴
0.293	1.320	5.541 ⁻¹	1.555 ⁻²	-1.248 ⁻³	0.883	1.074	7.654 ⁻³	8.700 ⁻³	7.212 ⁻⁴
0.300	1.323	5.000 ⁻¹	2.398 ⁻²	3.359 ⁻⁵	0.893	1.070	1.166 ⁻²	8.977 ⁻³	1.086 ⁻³
0.307	1.309	5.307 ⁻¹	1.573 ⁻²	5.716 ⁻⁴	0.900	1.063	3.992 ⁻³	7.659 ⁻³	7.422 ⁻⁴
0.320	1.298	4.647 ⁻¹	3.145 ⁻²	4.162 ⁻⁴	0.907	1.063	2.217 ⁻²	7.450 ⁻³	6.408 ⁻⁴
0.340	1.300	4.432 ⁻¹	2.664 ⁻²	1.265 ⁻³	0.913	1.056	2.475 ⁻²	7.463 ⁻³	5.319 ⁻⁴
0.360	1.284	4.515 ⁻¹	2.552 ⁻²	7.384 ⁻⁴	0.920	1.048	1.061 ⁻²	6.273 ⁻³	7.935 ⁻⁴
0.380	1.274	4.234 ⁻¹	2.719 ⁻²	1.092 ⁻³	0.927	1.049	1.555 ⁻²	6.815 ⁻³	1.210 ⁻³
0.400	1.259	4.118 ⁻¹	2.583 ⁻²	1.388 ⁻³	0.933	1.044	1.137 ⁻²	5.543 ⁻³	8.315 ⁻⁴
0.420	1.254	3.577 ⁻¹	3.515 ⁻²	-2.205 ⁻³	0.940	1.038	1.518 ⁻²	5.382 ⁻³	7.398 ⁻⁴
0.440	1.233	3.210 ⁻¹	3.660 ⁻²	-1.002 ⁻³	0.947	1.024	9.188 ⁻³	4.955 ⁻³	1.094 ⁻³
0.460	1.233	2.980 ⁻¹	3.823 ⁻²	-2.761 ⁻³	0.953	1.005	1.698 ⁻²	5.506 ⁻³	1.328 ⁻³
0.480	1.225	2.847 ⁻¹	4.054 ⁻²	-3.355 ⁻³	0.960	0.984	2.343 ⁻²	4.743 ⁻³	1.133 ⁻³

Table 12. Continued ($\theta = 180$ deg)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.079	1.334 ⁻²	1.798 ⁻²	1.692 ⁻³	0.547	1.148	3.776 ⁻¹	1.913 ⁻²	-7.850 ⁻⁴
0.027	-0.079	1.665 ⁻²	2.714 ⁻²	1.946 ⁻³	0.560	1.160	4.453 ⁻¹	1.449 ⁻²	8.250 ⁻⁴
0.033	-0.173	1.157 ⁻²	2.094 ⁻²	7.261 ⁻⁴	0.573	1.135	3.696 ⁻¹	1.748 ⁻²	-6.591 ⁻⁴
0.040	-0.179	1.487 ⁻²	2.269 ⁻²	6.938 ⁻⁴	0.580	1.148	3.548 ⁻¹	2.126 ⁻²	3.851 ⁻⁴
0.047	-0.191	1.566 ⁻²	2.612 ⁻²	-1.042 ⁻⁵	0.600	1.126	3.769 ⁻¹	1.758 ⁻²	-2.979 ⁻⁵
0.053	-0.192	2.459 ⁻²	2.888 ⁻²	6.816 ⁻⁵	0.620	1.124	3.925 ⁻¹	1.820 ⁻²	1.352 ⁻³
0.060	-0.163	2.871 ⁻²	3.387 ⁻²	-1.065 ⁻⁴	0.627	1.114	3.422 ⁻¹	1.502 ⁻²	-1.912 ⁻⁵
0.067	-0.152	3.666 ⁻²	3.515 ⁻²	1.303 ⁻³	0.640	1.132	3.591 ⁻¹	1.257 ⁻²	2.110 ⁻³
0.073	-0.113	4.794 ⁻²	4.460 ⁻²	2.474 ⁻³	0.653	1.099	3.386 ⁻¹	1.646 ⁻²	1.470 ⁻⁴
0.080	-0.092	5.946 ⁻²	5.000 ⁻²	7.351 ⁻⁴	0.660	1.119	3.156 ⁻¹	1.711 ⁻²	1.825 ⁻³
0.087	-0.063	6.779 ⁻²	5.661 ⁻²	3.031 ⁻³	0.673	1.106	3.175 ⁻¹	1.634 ⁻²	1.449 ⁻³
0.097	-0.027	8.854 ⁻²	6.067 ⁻²	3.515 ⁻³	0.680	1.087	3.254 ⁻¹	1.612 ⁻²	-6.759 ⁻⁴
0.107	0.111	1.305 ⁻¹	1.003 ⁻¹	1.711 ⁻²	0.687	1.107	3.055 ⁻¹	1.952 ⁻²	2.875 ⁻⁴
0.117	0.259	1.789 ⁻¹	1.357 ⁻¹	3.079 ⁻²	0.700	1.096	2.877 ⁻¹	2.065 ⁻²	-2.337 ⁻⁴
0.127	0.665	2.899 ⁻¹	1.729 ⁻¹	5.777 ⁻²	0.707	1.078	2.990 ⁻¹	1.620 ⁻²	-1.652 ⁻⁴
0.137	1.008	3.968 ⁻¹	1.116 ⁻¹	3.688 ⁻²	0.727	1.097	2.770 ⁻¹	1.583 ⁻²	2.674 ⁻⁴
0.147	0.945	3.866 ⁻¹	1.205 ⁻¹	3.912 ⁻²	0.733	1.067	2.664 ⁻¹	1.788 ⁻²	-4.646 ⁻⁴
0.157	1.071	4.298 ⁻¹	8.014 ⁻²	2.709 ⁻²	0.740	1.079	2.922 ⁻¹	1.413 ⁻²	1.668 ⁻³
0.167	1.129	4.557 ⁻¹	5.701 ⁻²	1.566 ⁻²	0.753	1.080	2.557 ⁻¹	1.768 ⁻²	3.693 ⁻⁴
0.177	1.249	4.924 ⁻¹	1.955 ⁻²	2.160 ⁻³	0.760	1.065	2.430 ⁻¹	1.740 ⁻²	-1.009 ⁻³
0.187	1.212	5.049 ⁻¹	2.683 ⁻²	4.555 ⁻³	0.767	1.074	2.303 ⁻¹	1.714 ⁻²	4.256 ⁻⁴
0.200	1.267	5.050 ⁻¹	1.457 ⁻²	-2.303 ⁻⁴	0.780	1.068	2.199 ⁻¹	1.727 ⁻²	1.959 ⁻⁴
0.213	1.294	5.071 ⁻¹	1.100 ⁻²	5.166 ⁻⁴	0.793	1.063	1.960 ⁻¹	1.552 ⁻²	-2.597 ⁻⁴
0.227	1.265	5.308 ⁻¹	9.975 ⁻³	-2.207 ⁻⁴	0.803	1.062	1.754 ⁻¹	1.773 ⁻²	-1.831 ⁻⁴
0.240	1.275	5.348 ⁻¹	7.273 ⁻³	-3.602 ⁻⁴	0.813	1.050	1.962 ⁻¹	1.378 ⁻²	1.075 ⁻³
0.253	1.278	5.231 ⁻¹	7.705 ⁻³	-2.483 ⁻⁴	0.823	1.058	1.551 ⁻¹	1.549 ⁻²	-7.706 ⁻⁴
0.267	1.279	5.318 ⁻¹	6.055 ⁻³	-2.667 ⁻⁴	0.833	1.040	1.644 ⁻¹	1.459 ⁻²	1.069 ⁻³
0.273	1.291	5.794 ⁻¹	8.731 ⁻³	-1.569 ⁻⁵	0.843	1.046	1.496 ⁻¹	1.297 ⁻²	-4.134 ⁻⁴
0.280	1.278	5.494 ⁻¹	5.963 ⁻³	-4.423 ⁻⁵	0.853	1.040	1.403 ⁻¹	1.282 ⁻²	-1.402 ⁻⁴
0.293	1.280	5.334 ⁻¹	5.078 ⁻³	-3.449 ⁻⁴	0.863	1.038	1.240 ⁻¹	1.238 ⁻²	-1.240 ⁻⁴
0.307	1.273	5.147 ⁻¹	5.930 ⁻³	-7.980 ⁻⁵	0.873	1.022	1.146 ⁻¹	1.152 ⁻²	2.368 ⁻⁴
0.320	1.267	5.068 ⁻¹	6.471 ⁻³	-1.395 ⁻⁴	0.883	1.022	9.968 ⁻²	1.209 ⁻²	1.027 ⁻³
0.327	1.269	5.683 ⁻¹	8.885 ⁻³	5.543 ⁻⁴	0.893	1.021	9.361 ⁻²	1.022 ⁻²	8.065 ⁻⁴
0.353	1.266	5.447 ⁻¹	1.034 ⁻²	1.122 ⁻³	0.900	1.023	6.629 ⁻²	1.007 ⁻²	-2.755 ⁻⁴
0.380	1.245	4.848 ⁻¹	1.396 ⁻²	3.381 ⁻⁴	0.907	1.018	7.607 ⁻²	9.257 ⁻³	3.128 ⁻⁴
0.407	1.237	5.342 ⁻¹	1.068 ⁻²	1.388 ⁻³	0.913	1.015	6.554 ⁻²	8.344 ⁻³	2.857 ⁻⁴
0.433	1.226	5.028 ⁻¹	1.294 ⁻²	1.621 ⁻³	0.920	1.014	6.679 ⁻²	7.144 ⁻³	1.591 ⁻⁴
0.460	1.203	4.549 ⁻¹	1.063 ⁻²	1.552 ⁻³	0.927	1.007	6.091 ⁻²	7.676 ⁻³	8.594 ⁻⁴
0.480	1.182	4.392 ⁻¹	1.529 ⁻²	1.486 ⁻⁴	0.933	1.011	5.320 ⁻²	6.513 ⁻³	4.422 ⁻⁴
0.500	1.177	4.360 ⁻¹	1.133 ⁻²	9.372 ⁻⁴	0.940	1.016	3.503 ⁻²	5.282 ⁻³	3.817 ⁻⁴
0.520	1.159	4.475 ⁻¹	1.288 ⁻²	1.100 ⁻³	0.953	1.002	1.919 ⁻²	4.983 ⁻³	1.176 ⁻³
0.540	1.166	4.632 ⁻¹	1.396 ⁻²	4.408 ⁻⁴					

Table 12. Concluded ($\theta = 180$ deg)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.060	2.488 ⁻²	2.791 ⁻²	1.294 ⁻³	0.460	1.206	3.958 ⁻¹	1.894 ⁻²	4.105 ⁻³
0.027	-0.114	2.259 ⁻²	2.491 ⁻²	6.178 ⁻⁴	0.480	1.190	3.875 ⁻¹	1.836 ⁻²	3.534 ⁻³
0.033	-0.109	2.509 ⁻²	3.033 ⁻²	1.521 ⁻³	0.500	1.178	3.683 ⁻¹	2.037 ⁻²	4.006 ⁻³
0.040	-0.064	3.373 ⁻²	4.005 ⁻²	1.939 ⁻³	0.540	1.153	3.411 ⁻¹	2.194 ⁻²	3.725 ⁻³
0.047	-0.030	5.033 ⁻²	4.646 ⁻²	3.489 ⁻³	0.547	1.124	3.711 ⁻¹	2.307 ⁻²	4.127 ⁻³
0.053	-0.077	4.915 ⁻²	3.996 ⁻²	-2.208 ⁻⁴	0.560	1.148	3.533 ⁻¹	1.775 ⁻²	3.242 ⁻³
0.060	0.008	6.716 ⁻²	6.635 ⁻²	7.247 ⁻³	0.580	1.138	3.632 ⁻¹	1.768 ⁻²	3.142 ⁻³
0.067	0.118	8.876 ⁻²	9.841 ⁻²	1.818 ⁻²	0.600	1.111	3.396 ⁻¹	2.344 ⁻²	2.700 ⁻³
0.073	0.512	1.932 ⁻¹	1.864 ⁻¹	6.955 ⁻²	0.620	1.118	3.160 ⁻¹	2.194 ⁻²	2.171 ⁻³
0.080	0.800	2.798 ⁻¹	1.783 ⁻¹	6.830 ⁻²	0.640	1.103	3.395 ⁻¹	1.926 ⁻²	2.605 ⁻³
0.087	0.353	1.778 ⁻¹	1.531 ⁻¹	4.441 ⁻²	0.653	1.092	2.550 ⁻¹	2.702 ⁻²	2.217 ⁻³
0.097	0.453	2.093 ⁻¹	1.695 ⁻¹	5.903 ⁻²	0.660	1.091	2.815 ⁻¹	2.795 ⁻²	1.867 ⁻³
0.107	1.051	3.931 ⁻¹	1.034 ⁻¹	4.456 ⁻²	0.673	1.083	2.322 ⁻¹	2.372 ⁻²	1.348 ⁻³
0.117	1.042	4.027 ⁻¹	9.774 ⁻²	3.609 ⁻²	0.680	1.082	2.348 ⁻¹	2.750 ⁻²	1.168 ⁻³
0.127	1.050	4.214 ⁻¹	1.022 ⁻¹	3.970 ⁻²	0.687	1.076	2.663 ⁻¹	2.139 ⁻²	1.631 ⁻³
0.137	1.286	5.055 ⁻¹	1.724 ⁻²	3.393 ⁻³	0.700	1.073	2.630 ⁻¹	2.279 ⁻²	1.888 ⁻³
0.147	1.202	4.840 ⁻¹	4.527 ⁻²	1.334 ⁻²	0.713	1.068	2.555 ⁻¹	2.619 ⁻²	2.157 ⁻³
0.157	1.279	5.182 ⁻¹	2.121 ⁻²	3.963 ⁻³	0.727	1.061	2.564 ⁻¹	2.000 ⁻²	2.312 ⁻³
0.167	1.243	5.218 ⁻¹	3.003 ⁻²	7.093 ⁻³	0.733	1.062	2.223 ⁻¹	2.445 ⁻²	1.112 ⁻³
0.177	1.299	5.346 ⁻¹	1.466 ⁻²	5.596 ⁻⁵	0.740	1.058	2.291 ⁻¹	2.209 ⁻²	1.564 ⁻³
0.187	1.318	5.412 ⁻¹	9.098 ⁻³	-8.523 ⁻⁴	0.753	1.057	2.238 ⁻¹	2.255 ⁻²	1.163 ⁻³
0.200	1.291	5.593 ⁻¹	9.107 ⁻³	-4.638 ⁻⁴	0.767	1.052	1.914 ⁻¹	1.985 ⁻²	1.390 ⁻³
0.213	1.317	5.488 ⁻¹	8.500 ⁻³	-6.909 ⁻⁴	0.780	1.044	1.958 ⁻¹	1.965 ⁻²	5.086 ⁻⁴
0.220	1.262	5.706 ⁻¹	1.364 ⁻²	6.508 ⁻⁵	0.803	1.043	1.670 ⁻¹	2.326 ⁻²	-3.690 ⁻⁴
0.227	1.316	5.510 ⁻¹	8.273 ⁻³	-8.662 ⁻⁴	0.813	1.035	1.407 ⁻¹	1.853 ⁻²	-2.288 ⁻⁴
0.240	1.301	5.440 ⁻¹	9.315 ⁻³	-1.307 ⁻³	0.823	1.036	1.460 ⁻¹	1.779 ⁻²	1.441 ⁻⁴
0.247	1.299	5.787 ⁻¹	7.974 ⁻³	-1.853 ⁻⁴	0.833	1.026	1.190 ⁻¹	1.781 ⁻²	1.128 ⁻⁴
0.253	1.306	5.530 ⁻¹	7.002 ⁻³	-9.774 ⁻⁴	0.843	1.033	1.162 ⁻¹	1.766 ⁻²	-7.694 ⁻⁴
0.267	1.292	5.602 ⁻¹	7.672 ⁻³	-1.063 ⁻³	0.853	1.014	9.786 ⁻²	1.673 ⁻²	-3.588 ⁻⁴
0.273	1.295	5.649 ⁻¹	6.868 ⁻³	1.868 ⁻⁶	0.863	1.023	9.803 ⁻²	1.861 ⁻²	7.655 ⁻⁴
0.280	1.328	5.735 ⁻¹	6.949 ⁻³	-6.701 ⁻⁴	0.873	1.016	7.897 ⁻²	1.347 ⁻²	-2.507 ⁻⁴
0.293	1.323	5.587 ⁻¹	7.479 ⁻³	-3.235 ⁻⁴	0.883	1.013	9.355 ⁻²	1.270 ⁻²	-7.352 ⁻⁵
0.300	1.297	5.558 ⁻¹	5.423 ⁻³	6.039 ⁻⁴	0.893	1.009	1.071 ⁻¹	1.183 ⁻²	3.335 ⁻⁴
0.307	1.294	5.379 ⁻¹	7.988 ⁻³	1.597 ⁻⁴	0.900	1.008	1.073 ⁻¹	1.119 ⁻²	-1.253 ⁻⁴
0.320	1.291	5.249 ⁻¹	6.779 ⁻³	2.509 ⁻⁶	0.907	1.010	1.004 ⁻¹	1.034 ⁻²	-2.176 ⁻⁴
0.327	1.288	5.207 ⁻¹	8.797 ⁻³	1.165 ⁻³	0.913	1.010	9.352 ⁻²	1.216 ⁻²	-5.507 ⁻⁵
0.340	1.283	5.014 ⁻¹	9.634 ⁻³	1.126 ⁻³	0.920	1.002	7.116 ⁻²	8.822 ⁻³	-1.041 ⁻⁴
0.353	1.277	5.170 ⁻¹	7.432 ⁻³	1.378 ⁻³	0.927	1.000	4.938 ⁻²	8.009 ⁻³	6.859 ⁻⁵
0.360	1.267	4.613 ⁻¹	1.438 ⁻²	2.743 ⁻³	0.933	1.002	5.595 ⁻²	7.012 ⁻³	1.467 ⁻⁴
0.380	1.252	4.545 ⁻¹	1.478 ⁻²	3.209 ⁻³	0.940	1.001	4.364 ⁻²	6.363 ⁻³	6.700 ⁻⁵
0.400	1.252	4.157 ⁻¹	1.609 ⁻²	3.910 ⁻³	0.947	0.988	3.385 ⁻²	6.246 ⁻³	7.695 ⁻⁴
0.440	1.208	4.019 ⁻¹	2.073 ⁻²	4.641 ⁻³	0.953	0.973	2.709 ⁻²	6.285 ⁻³	1.363 ⁻³

Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ ($+$)

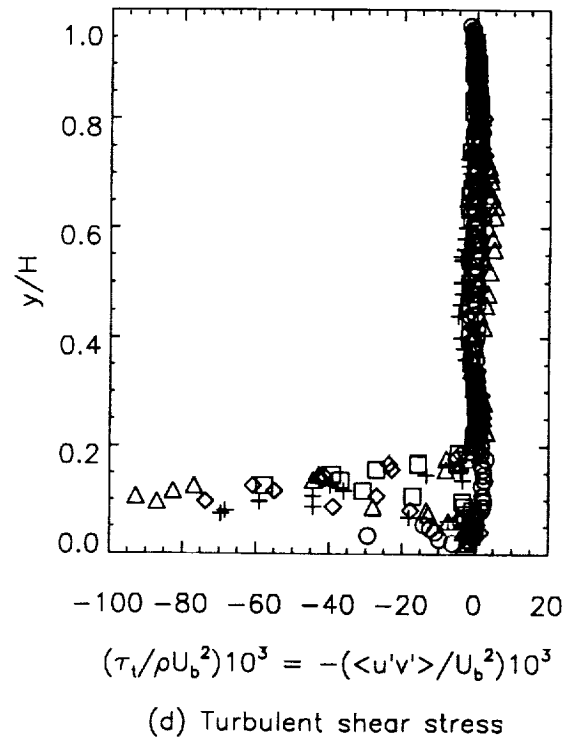
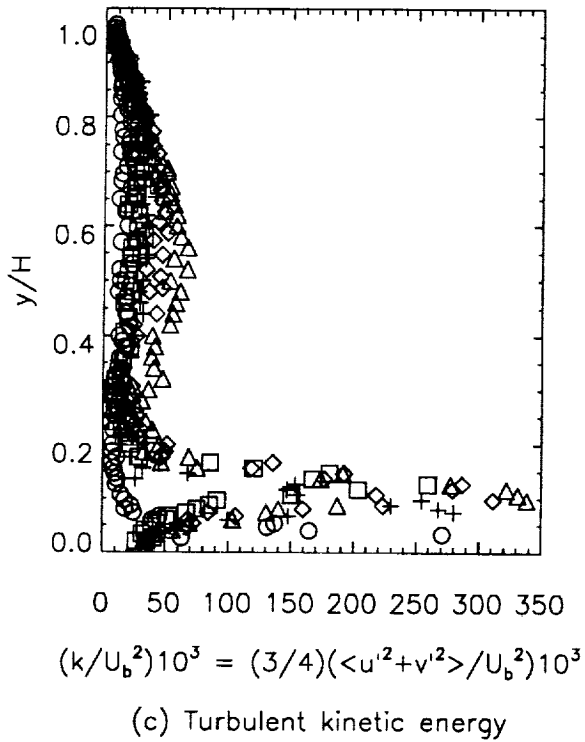
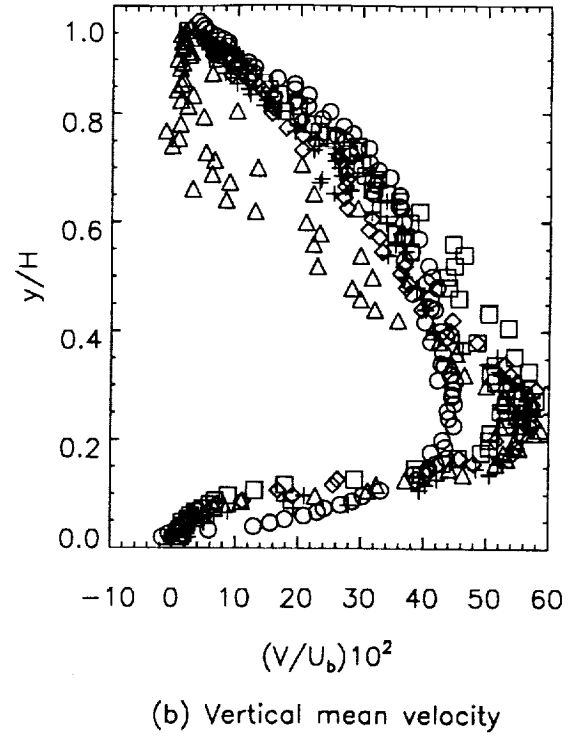
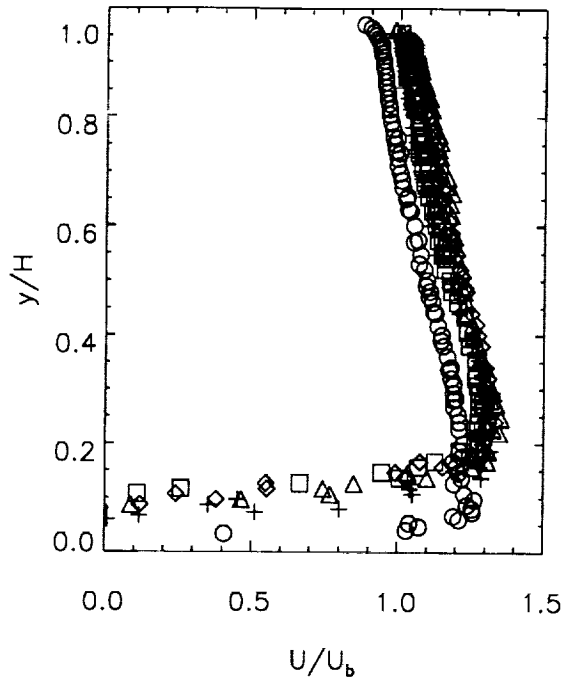


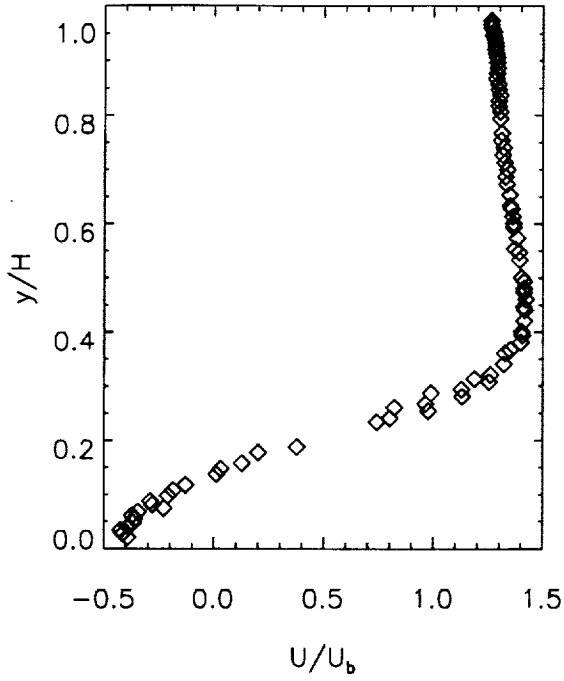
Figure 12. Summary of Table 12 ($\theta = 180$ deg).

Table 13. LDV flowfield data in TAD ($x/H = 0.5$)

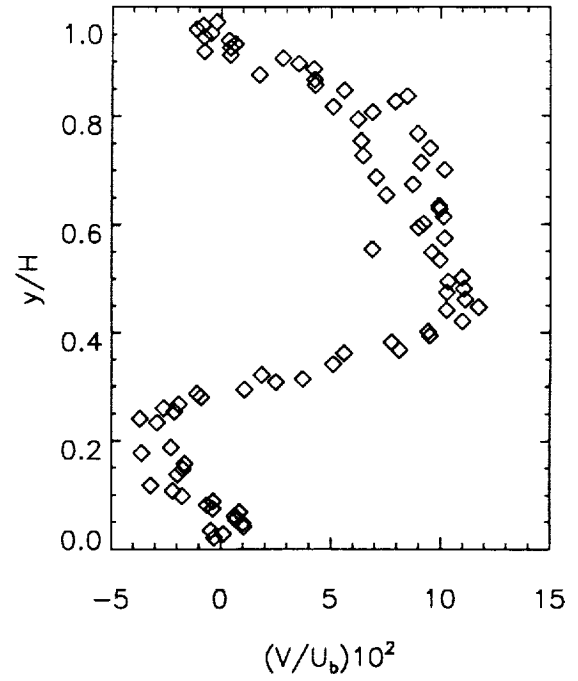
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.021	-0.392	-3.046 ⁻³	3.816 ⁻²	-2.483 ⁻³	0.493	1.415	1.034 ⁻¹	1.708 ⁻²	5.468 ⁻³
0.027	-0.415	1.107 ⁻³	3.610 ⁻²	-4.222 ⁻³	0.501	1.403	1.097 ⁻¹	2.369 ⁻²	5.755 ⁻³
0.034	-0.424	-4.592 ⁻³	3.436 ⁻²	-5.403 ⁻³	0.533	1.393	9.955 ⁻²	1.772 ⁻²	5.569 ⁻³
0.041	-0.390	1.042 ⁻²	4.231 ⁻²	-7.544 ⁻³	0.547	1.392	9.611 ⁻²	2.164 ⁻²	6.081 ⁻³
0.047	-0.368	9.989 ⁻³	5.093 ⁻²	-8.870 ⁻³	0.553	1.370	6.883 ⁻²	2.348 ⁻²	6.552 ⁻³
0.054	-0.362	6.742 ⁻³	5.498 ⁻²	-1.242 ⁻²	0.574	1.383	1.018 ⁻¹	1.971 ⁻²	5.937 ⁻³
0.061	-0.372	6.394 ⁻³	5.497 ⁻²	-1.104 ⁻²	0.593	1.366	8.994 ⁻²	1.884 ⁻²	6.121 ⁻³
0.067	-0.345	8.481 ⁻³	5.825 ⁻²	-1.148 ⁻²	0.601	1.366	9.217 ⁻²	2.368 ⁻²	5.698 ⁻³
0.074	-0.228	-3.720 ⁻³	8.256 ⁻²	-2.258 ⁻²	0.613	1.362	1.013 ⁻¹	1.805 ⁻²	4.407 ⁻³
0.081	-0.280	-6.377 ⁻³	7.824 ⁻²	-1.850 ⁻²	0.627	1.356	9.956 ⁻²	2.303 ⁻²	5.602 ⁻³
0.087	-0.290	-3.581 ⁻³	7.623 ⁻²	-2.086 ⁻²	0.633	1.350	9.929 ⁻²	1.930 ⁻²	4.916 ⁻³
0.097	-0.209	-1.764 ⁻²	9.263 ⁻²	-2.823 ⁻²	0.654	1.348	7.520 ⁻²	2.165 ⁻²	5.388 ⁻³
0.107	-0.186	-2.201 ⁻²	9.786 ⁻²	-3.053 ⁻²	0.673	1.334	8.730 ⁻²	1.936 ⁻²	4.556 ⁻³
0.117	-0.129	-3.203 ⁻²	1.064 ⁻¹	-3.515 ⁻²	0.687	1.329	7.060 ⁻²	1.997 ⁻²	4.980 ⁻³
0.137	0.011	-1.986 ⁻²	1.268 ⁻¹	-4.472 ⁻²	0.700	1.336	1.018 ⁻¹	1.678 ⁻²	4.682 ⁻³
0.147	0.031	-1.735 ⁻²	1.319 ⁻¹	-4.448 ⁻²	0.713	1.326	9.103 ⁻²	1.866 ⁻²	4.215 ⁻³
0.157	0.127	-1.662 ⁻²	1.414 ⁻¹	-4.862 ⁻²	0.727	1.316	6.469 ⁻²	2.273 ⁻²	4.176 ⁻³
0.177	0.202	-3.628 ⁻²	1.523 ⁻¹	-5.542 ⁻²	0.740	1.320	9.521 ⁻²	1.718 ⁻²	4.269 ⁻³
0.187	0.377	-2.283 ⁻²	1.665 ⁻¹	-5.431 ⁻²	0.753	1.309	6.387 ⁻²	1.854 ⁻²	4.167 ⁻³
0.233	0.742	-2.917 ⁻²	1.507 ⁻¹	-3.771 ⁻²	0.767	1.312	8.958 ⁻²	1.638 ⁻²	3.458 ⁻³
0.241	0.802	-3.707 ⁻²	1.533 ⁻¹	-3.744 ⁻²	0.793	1.304	6.225 ⁻²	1.806 ⁻²	3.116 ⁻³
0.254	0.976	-2.121 ⁻²	1.299 ⁻¹	-2.576 ⁻²	0.807	1.304	6.888 ⁻²	1.570 ⁻²	3.399 ⁻³
0.260	0.822	-2.618 ⁻²	1.353 ⁻¹	-3.434 ⁻²	0.817	1.297	5.104 ⁻²	1.872 ⁻²	3.127 ⁻³
0.267	0.964	-1.927 ⁻²	1.204 ⁻¹	-2.819 ⁻²	0.827	1.297	7.937 ⁻²	1.462 ⁻²	3.556 ⁻³
0.281	1.132	-9.115 ⁻³	8.806 ⁻²	-1.675 ⁻²	0.837	1.304	8.478 ⁻²	1.308 ⁻²	2.879 ⁻³
0.287	0.989	-1.093 ⁻²	9.952 ⁻²	-2.293 ⁻²	0.847	1.296	5.603 ⁻²	1.377 ⁻²	3.496 ⁻³
0.294	1.128	1.062 ⁻²	8.873 ⁻²	-2.221 ⁻²	0.857	1.295	4.287 ⁻²	1.393 ⁻²	3.061 ⁻³
0.307	1.254	2.492 ⁻²	5.415 ⁻²	-9.633 ⁻³	0.867	1.286	4.257 ⁻²	1.324 ⁻²	2.746 ⁻³
0.313	1.188	3.715 ⁻²	6.656 ⁻²	-1.283 ⁻²	0.877	1.288	1.749 ⁻²	1.273 ⁻²	2.639 ⁻³
0.321	1.261	1.841 ⁻²	5.477 ⁻²	-8.319 ⁻³	0.887	1.291	4.219 ⁻²	1.039 ⁻²	2.589 ⁻³
0.340	1.322	5.098 ⁻²	3.977 ⁻²	-3.812 ⁻³	0.897	1.290	3.530 ⁻²	9.994 ⁻³	1.987 ⁻³
0.361	1.326	5.593 ⁻²	4.336 ⁻²	-6.361 ⁻³	0.907	1.289	2.814 ⁻²	9.145 ⁻³	2.047 ⁻³
0.367	1.351	8.118 ⁻²	3.427 ⁻²	-3.452 ⁻³	0.913	1.284	4.276 ⁻³	1.090 ⁻²	3.256 ⁻³
0.381	1.399	7.763 ⁻²	2.986 ⁻²	-2.415 ⁻⁴	0.920	1.280	-7.672 ⁻³	8.517 ⁻³	1.972 ⁻³
0.393	1.406	9.503 ⁻²	2.111 ⁻²	1.182 ⁻³	0.927	1.282	4.234 ⁻³	7.373 ⁻³	2.150 ⁻³
0.401	1.403	9.422 ⁻²	2.815 ⁻²	-3.030 ⁻³	0.933	1.281	6.475 ⁻³	6.822 ⁻³	1.801 ⁻³
0.420	1.416	1.099 ⁻¹	2.095 ⁻²	8.598 ⁻⁴	0.940	1.277	3.568 ⁻³	6.232 ⁻³	1.659 ⁻³
0.441	1.417	1.027 ⁻¹	2.126 ⁻²	1.806 ⁻³	0.947	1.271	-7.796 ⁻³	5.700 ⁻³	1.610 ⁻³
0.447	1.413	1.173 ⁻¹	1.738 ⁻²	2.480 ⁻³	0.953	1.274	-4.497 ⁻³	4.910 ⁻³	1.299 ⁻³
0.461	1.423	1.113 ⁻¹	1.895 ⁻²	2.795 ⁻³	0.960	1.264	-1.115 ⁻²	4.675 ⁻³	1.575 ⁻³
0.473	1.415	1.028 ⁻¹	1.713 ⁻²	3.975 ⁻³	0.967	1.263	-8.293 ⁻³	4.311 ⁻³	1.635 ⁻³
0.481	1.415	1.105 ⁻¹	2.022 ⁻²	4.233 ⁻³	0.973	1.263	-2.031 ⁻³	4.329 ⁻³	1.353 ⁻³

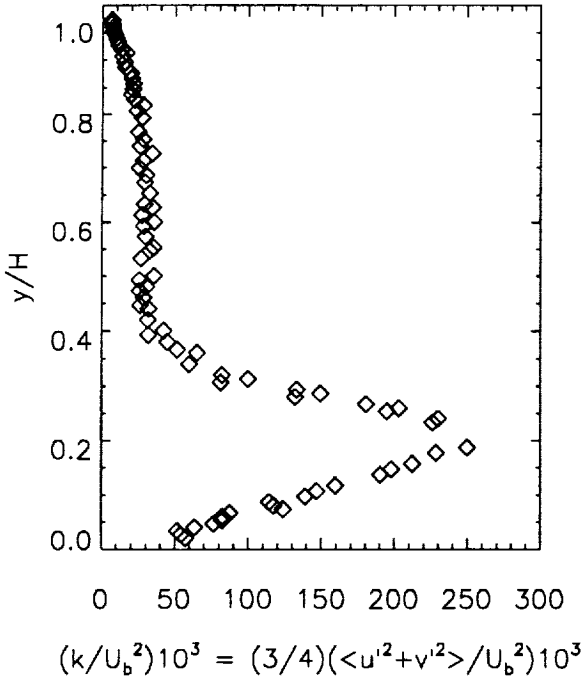
Legend: $Re = 1 \times 10^6$; $z/H = 0(\diamond)$



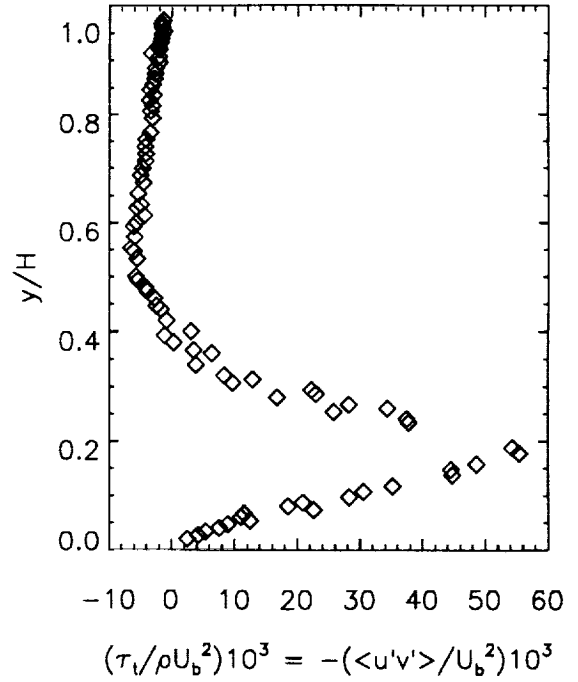
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 13. Summary of Table 13 ($x/H = 0.5$).

Table 14. LDV flowfield in TAD ($x/H = 1$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.028	0.021	-1.699 ⁻²	3.811 ⁻²	-3.976 ⁻³	0.461	1.228	4.628 ⁻²	1.351 ⁻²	-2.299 ⁻⁴
0.035	-0.044	-2.517 ⁻²	3.599 ⁻²	-3.048 ⁻³	0.481	1.226	8.655 ⁻²	1.101 ⁻²	-5.281 ⁻⁴
0.041	-0.011	-2.769 ⁻²	4.095 ⁻²	-5.494 ⁻³	0.521	1.241	7.867 ⁻²	1.143 ⁻²	-1.636 ⁻⁵
0.048	0.017	-3.060 ⁻²	4.649 ⁻²	-8.947 ⁻³	0.548	1.245	7.925 ⁻²	1.330 ⁻²	2.581 ⁻⁴
0.055	0.161	-4.481 ⁻²	6.919 ⁻²	-1.285 ⁻²	0.568	1.265	6.361 ⁻²	1.088 ⁻²	5.168 ⁻⁴
0.061	0.243	-5.687 ⁻²	7.750 ⁻²	-1.681 ⁻²	0.575	1.237	1.004 ⁻¹	1.152 ⁻²	7.248 ⁻⁴
0.068	0.264	-6.553 ⁻²	7.712 ⁻²	-1.820 ⁻²	0.608	1.260	7.769 ⁻²	1.089 ⁻²	9.015 ⁻⁴
0.075	0.375	-7.130 ⁻²	8.374 ⁻²	-1.899 ⁻²	0.648	1.255	1.001 ⁻¹	1.211 ⁻²	8.303 ⁻⁴
0.081	0.555	-8.556 ⁻²	9.140 ⁻²	-2.091 ⁻²	0.655	1.239	9.501 ⁻²	1.464 ⁻²	1.870 ⁻³
0.088	0.557	-8.780 ⁻²	7.951 ⁻²	-1.777 ⁻²	0.668	1.255	8.178 ⁻²	1.218 ⁻²	1.723 ⁻³
0.098	0.720	-9.798 ⁻²	6.764 ⁻²	-1.117 ⁻²	0.681	1.241	8.919 ⁻²	1.331 ⁻²	1.899 ⁻³
0.108	0.751	-1.019 ⁻¹	7.831 ⁻²	-1.052 ⁻²	0.708	1.235	8.995 ⁻²	1.425 ⁻²	2.216 ⁻³
0.118	0.817	-1.010 ⁻¹	6.301 ⁻²	-7.720 ⁻³	0.721	1.254	6.423 ⁻²	1.210 ⁻²	1.872 ⁻³
0.128	0.732	-1.076 ⁻¹	7.935 ⁻²	-1.113 ⁻²	0.735	1.242	8.376 ⁻²	1.216 ⁻²	2.140 ⁻³
0.138	0.819	-1.090 ⁻¹	6.925 ⁻²	-9.519 ⁻³	0.748	1.246	8.229 ⁻²	1.167 ⁻²	1.680 ⁻³
0.148	0.863	-1.109 ⁻¹	5.776 ⁻²	-4.216 ⁻³	0.761	1.235	8.186 ⁻²	1.275 ⁻²	2.168 ⁻³
0.158	0.889	-1.039 ⁻¹	5.205 ⁻²	-2.537 ⁻³	0.775	1.258	5.696 ⁻²	9.205 ⁻³	1.909 ⁻³
0.168	0.886	-9.939 ⁻²	5.574 ⁻²	-5.763 ⁻³	0.811	1.247	2.619 ⁻²	1.067 ⁻²	2.140 ⁻³
0.178	1.005	-1.015 ⁻¹	3.647 ⁻²	1.831 ⁻³	0.821	1.248	4.190 ⁻²	9.961 ⁻³	1.908 ⁻³
0.188	0.995	-1.122 ⁻¹	4.284 ⁻²	2.979 ⁻³	0.831	1.250	3.247 ⁻²	9.690 ⁻³	1.855 ⁻³
0.201	1.002	-1.044 ⁻¹	3.924 ⁻²	1.490 ⁻³	0.841	1.244	2.939 ⁻²	8.647 ⁻³	1.504 ⁻³
0.215	1.036	-9.653 ⁻²	3.477 ⁻²	2.501 ⁻³	0.851	1.250	2.814 ⁻²	8.087 ⁻³	1.706 ⁻³
0.228	1.085	-9.671 ⁻²	3.087 ⁻²	1.287 ⁻³	0.861	1.252	4.347 ⁻²	6.102 ⁻³	1.349 ⁻³
0.241	1.051	-9.624 ⁻²	2.973 ⁻²	1.446 ⁻³	0.871	1.255	3.215 ⁻²	5.864 ⁻³	1.059 ⁻³
0.255	1.087	-6.830 ⁻²	2.682 ⁻²	9.904 ⁻⁴	0.881	1.245	9.243 ⁻³	7.207 ⁻³	1.137 ⁻³
0.268	1.076	-9.001 ⁻²	2.838 ⁻²	1.534 ⁻³	0.891	1.248	1.643 ⁻²	5.584 ⁻³	1.155 ⁻³
0.281	1.113	-6.989 ⁻²	2.454 ⁻²	1.137 ⁻³	0.901	1.245	4.023 ⁻³	5.316 ⁻³	1.104 ⁻³
0.295	1.143	-6.158 ⁻²	2.198 ⁻²	1.912 ⁻³	0.908	1.245	1.321 ⁻²	5.093 ⁻³	1.047 ⁻³
0.308	1.145	-5.029 ⁻²	2.308 ⁻²	7.755 ⁻⁴	0.915	1.244	1.183 ⁻²	4.265 ⁻³	8.475 ⁻⁴
0.321	1.147	-3.274 ⁻²	1.804 ⁻²	1.022 ⁻³	0.921	1.240	-7.983 ⁻⁴	4.516 ⁻³	9.281 ⁻⁴
0.341	1.162	-3.055 ⁻²	1.923 ⁻²	1.734 ⁻⁴	0.928	1.241	3.885 ⁻³	3.772 ⁻³	8.320 ⁻⁴
0.361	1.185	-1.546 ⁻²	1.675 ⁻²	3.079 ⁻⁴	0.935	1.242	2.268 ⁻³	3.473 ⁻³	7.693 ⁻⁴
0.381	1.194	4.168 ⁻³	1.688 ⁻²	5.549 ⁻⁴	0.941	1.231	-7.539 ⁻³	3.558 ⁻³	8.591 ⁻⁴
0.388	1.219	-3.421 ⁻³	1.852 ⁻²	8.746 ⁻⁴	0.948	1.224	-6.302 ⁻³	3.259 ⁻³	7.158 ⁻⁴
0.401	1.206	1.296 ⁻²	1.539 ⁻²	1.768 ⁻⁴	0.955	1.220	-7.757 ⁻³	3.042 ⁻³	7.379 ⁻⁴
0.415	1.232	-8.073 ⁻³	1.396 ⁻²	-4.843 ⁻⁴	0.961	1.202	-7.645 ⁻³	3.093 ⁻³	6.197 ⁻⁴
0.421	1.208	4.879 ⁻²	1.451 ⁻²	1.329 ⁻⁴	0.968	1.196	2.059 ⁻³	3.521 ⁻³	6.200 ⁻⁴

Table 14. Continued ($x/H = 1$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.142	-2.810 ⁻²	4.528 ⁻²	-7.947 ⁻³	0.491	1.381	-8.231 ⁻²	2.543 ⁻²	2.322 ⁻³
0.027	-0.200	-1.239 ⁻²	3.924 ⁻²	-3.715 ⁻³	0.500	1.349	-9.922 ⁻²	2.967 ⁻²	3.213 ⁻³
0.033	-0.178	-1.270 ⁻²	4.568 ⁻²	-6.126 ⁻³	0.520	1.351	-4.064 ⁻²	2.707 ⁻²	4.193 ⁻³
0.040	-0.183	-1.677 ⁻²	4.838 ⁻²	-9.976 ⁻³	0.547	1.366	-3.893 ⁻²	2.483 ⁻²	4.150 ⁻³
0.047	-0.187	-3.139 ⁻²	5.060 ⁻²	-1.018 ⁻²	0.551	1.378	-6.001 ⁻²	2.961 ⁻²	6.280 ⁻³
0.053	-0.099	-1.498 ⁻²	6.148 ⁻²	-1.266 ⁻²	0.571	1.393	-2.563 ⁻²	2.457 ⁻²	5.336 ⁻³
0.060	-0.100	-2.615 ⁻²	6.265 ⁻²	-1.859 ⁻²	0.573	1.365	-3.514 ⁻²	2.502 ⁻²	4.530 ⁻³
0.067	-0.032	-5.046 ⁻²	7.061 ⁻²	-1.909 ⁻²	0.591	1.392	-2.934 ⁻²	2.764 ⁻²	6.104 ⁻³
0.073	-0.036	-4.866 ⁻²	7.560 ⁻²	-2.069 ⁻²	0.600	1.355	-6.336 ⁻²	3.232 ⁻²	6.949 ⁻³
0.087	-0.046	-4.911 ⁻²	7.557 ⁻²	-2.409 ⁻²	0.611	1.387	-3.427 ⁻²	2.719 ⁻²	4.949 ⁻³
0.097	0.012	-5.772 ⁻²	8.890 ⁻²	-3.251 ⁻²	0.627	1.351	-2.509 ⁻²	2.713 ⁻²	6.856 ⁻³
0.107	0.027	-5.568 ⁻²	9.238 ⁻²	-3.380 ⁻²	0.631	1.391	-5.113 ⁻²	2.730 ⁻²	6.083 ⁻³
0.117	0.071	-6.835 ⁻²	9.650 ⁻²	-3.907 ⁻²	0.651	1.384	-3.070 ⁻²	2.539 ⁻²	6.135 ⁻³
0.127	0.137	-8.213 ⁻²	1.076 ⁻¹	-4.358 ⁻²	0.653	1.353	-5.852 ⁻²	2.937 ⁻²	4.208 ⁻³
0.147	0.352	-1.118 ⁻¹	1.205 ⁻¹	-4.670 ⁻²	0.671	1.387	-1.891 ⁻²	2.592 ⁻²	6.018 ⁻³
0.157	0.362	-1.247 ⁻¹	1.242 ⁻¹	-5.119 ⁻²	0.680	1.354	-5.952 ⁻²	3.054 ⁻²	6.508 ⁻³
0.177	0.566	-1.385 ⁻¹	1.294 ⁻¹	-4.766 ⁻²	0.684	1.390	2.714 ⁻³	2.346 ⁻²	5.632 ⁻³
0.187	0.461	-1.508 ⁻¹	1.340 ⁻¹	-5.626 ⁻²	0.697	1.393	1.063 ⁻²	2.169 ⁻²	5.424 ⁻³
0.200	0.527	-1.707 ⁻¹	1.300 ⁻¹	-5.197 ⁻²	0.711	1.380	-2.871 ⁻²	2.665 ⁻²	5.833 ⁻³
0.213	0.711	-1.841 ⁻¹	1.300 ⁻¹	-4.493 ⁻²	0.724	1.389	-1.804 ⁻²	2.424 ⁻²	6.258 ⁻³
0.231	0.742	-1.512 ⁻¹	1.315 ⁻¹	-4.544 ⁻²	0.733	1.342	-5.142 ⁻²	2.644 ⁻²	5.452 ⁻³
0.240	0.811	-1.702 ⁻¹	1.057 ⁻¹	-3.214 ⁻²	0.737	1.371	-3.151 ⁻²	2.558 ⁻²	5.862 ⁻³
0.253	0.915	-1.518 ⁻¹	1.010 ⁻¹	-3.133 ⁻²	0.751	1.380	-5.287 ⁻²	2.801 ⁻²	6.239 ⁻³
0.257	0.824	-1.741 ⁻¹	1.146 ⁻¹	-3.762 ⁻²	0.764	1.378	-2.454 ⁻²	2.342 ⁻²	5.581 ⁻³
0.267	0.949	-1.399 ⁻¹	9.525 ⁻²	-2.739 ⁻²	0.777	1.381	-1.498 ⁻²	2.165 ⁻²	5.510 ⁻³
0.280	1.034	-1.493 ⁻¹	8.463 ⁻²	-2.582 ⁻²	0.791	1.381	-1.848 ⁻²	2.201 ⁻²	5.446 ⁻³
0.284	0.939	-1.618 ⁻¹	1.020 ⁻¹	-2.871 ⁻²	0.804	1.374	6.180 ⁻³	1.996 ⁻²	3.980 ⁻³
0.293	0.968	-1.561 ⁻¹	8.922 ⁻²	-2.686 ⁻²	0.814	1.380	-1.531 ⁻²	1.810 ⁻²	4.479 ⁻³
0.307	1.050	-1.416 ⁻¹	8.361 ⁻²	-2.465 ⁻²	0.824	1.376	4.114 ⁻³	1.640 ⁻²	4.307 ⁻³
0.311	1.089	-1.567 ⁻¹	7.979 ⁻²	-1.989 ⁻²	0.834	1.366	-3.995 ⁻²	1.812 ⁻²	4.400 ⁻³
0.320	1.031	-1.401 ⁻¹	7.978 ⁻²	-2.761 ⁻²	0.844	1.374	-2.070 ⁻²	1.636 ⁻²	4.134 ⁻³
0.337	1.113	-1.369 ⁻¹	7.478 ⁻²	-2.366 ⁻²	0.854	1.374	-2.383 ⁻²	1.638 ⁻²	4.473 ⁻³
0.340	1.115	-1.375 ⁻¹	7.148 ⁻²	-2.203 ⁻²	0.864	1.364	-3.645 ⁻²	1.491 ⁻²	3.517 ⁻³
0.360	1.202	-1.155 ⁻¹	5.100 ⁻²	-1.117 ⁻²	0.874	1.371	-2.095 ⁻²	1.357 ⁻²	3.324 ⁻³
0.364	1.231	-1.212 ⁻¹	4.852 ⁻²	-9.676 ⁻³	0.884	1.371	-2.273 ⁻²	1.245 ⁻²	3.353 ⁻³
0.380	1.226	-1.243 ⁻¹	5.085 ⁻²	-1.163 ⁻²	0.894	1.365	-1.666 ⁻²	1.184 ⁻²	3.885 ⁻³
0.400	1.281	-1.298 ⁻¹	3.696 ⁻²	-4.484 ⁻³	0.904	1.368	-2.859 ⁻³	9.486 ⁻³	2.638 ⁻³
0.417	1.291	-9.600 ⁻²	3.280 ⁻²	-4.821 ⁻³	0.911	1.364	-2.917 ⁻²	1.047 ⁻²	3.111 ⁻³
0.420	1.305	-9.069 ⁻²	3.304 ⁻²	-1.289 ⁻³	0.917	1.363	-2.556 ⁻²	8.707 ⁻³	2.714 ⁻³
0.440	1.315	-9.308 ⁻²	3.634 ⁻²	-4.228 ⁻³	0.924	1.359	-2.043 ⁻²	7.711 ⁻³	2.928 ⁻³
0.444	1.341	-8.608 ⁻²	3.103 ⁻²	-1.352 ⁻³	0.931	1.355	-1.971 ⁻²	8.109 ⁻³	2.950 ⁻³
0.460	1.334	-8.925 ⁻²	2.695 ⁻²	-1.981 ⁻³	0.937	1.349	-2.900 ⁻²	8.835 ⁻³	3.773 ⁻³
0.471	1.369	-7.260 ⁻²	2.994 ⁻²	1.109 ⁻³	0.944	1.341	-2.860 ⁻²	7.952 ⁻³	3.679 ⁻³
0.480	1.344	-5.045 ⁻²	2.585 ⁻²	-1.622 ⁻³	0.951	1.329	-2.860 ⁻²	7.466 ⁻³	3.310 ⁻³

Table 14. Continued ($x/H = 1$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	-0.041	-1.012 ⁻²	6.160 ⁻²	-1.065 ⁻²	0.547	1.345	-9.705 ⁻²	3.693 ⁻²	4.602 ⁻³
0.027	0.282	-4.275 ⁻²	9.441 ⁻²	-2.197 ⁻²	0.551	1.349	-7.558 ⁻²	4.038 ⁻²	4.280 ⁻³
0.033	0.362	-5.606 ⁻²	1.016 ⁻¹	-2.626 ⁻²	0.571	1.335	-2.133 ⁻¹	4.193 ⁻²	4.483 ⁻³
0.053	0.326	-6.469 ⁻²	9.880 ⁻²	-2.651 ⁻²	0.573	1.340	-9.565 ⁻²	4.057 ⁻²	6.928 ⁻³
0.060	0.518	-8.609 ⁻²	1.110 ⁻¹	-3.123 ⁻²	0.591	1.334	-8.831 ⁻²	3.512 ⁻²	5.707 ⁻³
0.067	0.612	-1.056 ⁻¹	1.073 ⁻¹	-3.076 ⁻²	0.600	1.345	-9.832 ⁻²	3.517 ⁻²	6.285 ⁻³
0.073	0.506	-8.976 ⁻²	1.227 ⁻¹	-3.816 ⁻²	0.611	1.339	-1.066 ⁻¹	3.643 ⁻²	5.639 ⁻³
0.080	0.656	-1.101 ⁻¹	1.149 ⁻¹	-3.754 ⁻²	0.627	1.336	-1.303 ⁻¹	3.718 ⁻²	6.244 ⁻³
0.087	0.453	-9.082 ⁻²	1.181 ⁻¹	-3.226 ⁻²	0.631	1.337	-1.241 ⁻¹	3.533 ⁻²	5.779 ⁻³
0.097	0.489	-9.517 ⁻²	1.062 ⁻¹	-3.275 ⁻²	0.651	1.334	-2.178 ⁻¹	3.742 ⁻²	5.281 ⁻³
0.107	0.630	-1.129 ⁻¹	1.152 ⁻¹	-3.623 ⁻²	0.653	1.333	-1.568 ⁻¹	3.898 ⁻²	5.495 ⁻³
0.127	0.799	-1.439 ⁻¹	1.086 ⁻¹	-3.293 ⁻²	0.671	1.341	-9.034 ⁻²	2.942 ⁻²	5.463 ⁻³
0.137	0.874	-1.469 ⁻¹	9.852 ⁻²	-2.970 ⁻²	0.680	1.337	-1.553 ⁻¹	3.216 ⁻²	4.093 ⁻³
0.157	0.953	-1.616 ⁻¹	9.547 ⁻²	-2.963 ⁻²	0.684	1.332	-2.012 ⁻¹	2.949 ⁻²	3.217 ⁻³
0.187	1.033	-1.620 ⁻¹	8.143 ⁻²	-2.383 ⁻²	0.697	1.330	-1.698 ⁻¹	2.876 ⁻²	3.963 ⁻³
0.213	1.129	-1.833 ⁻¹	6.133 ⁻²	-1.450 ⁻²	0.707	1.341	-9.882 ⁻²	3.149 ⁻²	3.497 ⁻³
0.227	1.152	-1.513 ⁻¹	5.795 ⁻²	-1.285 ⁻²	0.711	1.330	-1.760 ⁻¹	2.810 ⁻²	4.210 ⁻³
0.231	1.057	-1.525 ⁻¹	7.329 ⁻²	-1.863 ⁻²	0.724	1.332	-1.432 ⁻¹	2.516 ⁻²	3.275 ⁻³
0.240	1.220	-1.854 ⁻¹	4.512 ⁻²	-1.007 ⁻²	0.733	1.332	-1.390 ⁻¹	2.691 ⁻²	3.849 ⁻³
0.253	1.183	-1.552 ⁻¹	5.379 ⁻²	-1.076 ⁻²	0.737	1.330	-1.840 ⁻¹	2.350 ⁻²	2.915 ⁻³
0.257	1.218	-1.921 ⁻¹	4.560 ⁻²	-7.247 ⁻³	0.751	1.331	-1.222 ⁻¹	2.348 ⁻²	4.051 ⁻³
0.267	1.161	-1.389 ⁻¹	5.806 ⁻²	-1.141 ⁻²	0.764	1.323	-1.819 ⁻¹	1.990 ⁻²	2.803 ⁻³
0.280	1.180	-1.274 ⁻¹	5.855 ⁻²	-1.141 ⁻²	0.777	1.325	-1.708 ⁻¹	1.727 ⁻²	2.584 ⁻³
0.284	1.233	-1.568 ⁻¹	4.629 ⁻²	-8.822 ⁻³	0.791	1.327	-1.358 ⁻¹	2.043 ⁻²	4.118 ⁻³
0.293	1.274	-1.833 ⁻¹	3.845 ⁻²	-3.041 ⁻³	0.804	1.323	-1.212 ⁻¹	1.685 ⁻²	3.703 ⁻³
0.307	1.264	-1.677 ⁻¹	4.221 ⁻²	-5.036 ⁻³	0.814	1.324	-1.298 ⁻¹	1.673 ⁻²	2.779 ⁻³
0.311	1.256	-1.640 ⁻¹	4.070 ⁻²	-5.628 ⁻³	0.824	1.320	-1.210 ⁻¹	1.544 ⁻²	3.064 ⁻³
0.320	1.288	-1.790 ⁻¹	3.891 ⁻²	-3.294 ⁻³	0.834	1.320	-1.465 ⁻¹	1.438 ⁻²	3.283 ⁻³
0.337	1.281	-1.955 ⁻¹	4.222 ⁻²	-3.723 ⁻³	0.844	1.323	-9.422 ⁻²	1.439 ⁻²	3.065 ⁻³
0.340	1.281	-1.415 ⁻¹	4.266 ⁻²	-5.528 ⁻³	0.854	1.318	-9.871 ⁻²	1.304 ⁻²	2.869 ⁻³
0.360	1.266	-9.465 ⁻²	3.774 ⁻²	-3.736 ⁻³	0.864	1.316	-1.268 ⁻¹	1.019 ⁻²	2.638 ⁻³
0.364	1.298	-1.999 ⁻¹	3.881 ⁻²	-1.348 ⁻³	0.874	1.317	-9.322 ⁻²	1.272 ⁻²	3.129 ⁻³
0.380	1.317	-1.601 ⁻¹	3.503 ⁻²	5.426 ⁻⁴	0.884	1.319	-8.989 ⁻²	9.103 ⁻³	2.403 ⁻³
0.391	1.309	-8.102 ⁻²	3.267 ⁻²	8.588 ⁻⁴	0.894	1.316	-5.656 ⁻²	1.026 ⁻²	2.972 ⁻³
0.400	1.331	-1.119 ⁻¹	3.194 ⁻²	3.272 ⁻³	0.904	1.315	-6.921 ⁻²	8.431 ⁻³	2.029 ⁻³
0.420	1.328	-1.892 ⁻¹	4.074 ⁻²	2.569 ⁻³	0.911	1.312	-6.665 ⁻²	7.940 ⁻³	2.709 ⁻³
0.440	1.335	-1.771 ⁻¹	3.848 ⁻²	3.159 ⁻³	0.917	1.316	-3.651 ⁻²	1.056 ⁻²	3.771 ⁻³
0.444	1.329	-7.431 ⁻²	3.676 ⁻²	2.525 ⁻³	0.924	1.304	-5.979 ⁻²	8.209 ⁻³	2.996 ⁻³
0.460	1.343	-1.010 ⁻¹	3.328 ⁻²	3.566 ⁻³	0.931	1.310	-4.090 ⁻²	6.481 ⁻³	2.133 ⁻³
0.480	1.335	-8.150 ⁻²	3.628 ⁻²	3.835 ⁻³	0.937	1.305	-4.300 ⁻²	6.682 ⁻³	2.372 ⁻³
0.491	1.341	-8.538 ⁻²	3.545 ⁻²	3.626 ⁻³	0.944	1.291	-4.743 ⁻²	5.931 ⁻³	2.083 ⁻³
0.500	1.335	-1.839 ⁻¹	4.126 ⁻²	3.395 ⁻³	0.951	1.296	-3.631 ⁻²	5.949 ⁻³	2.484 ⁻³
0.511	1.346	-1.422 ⁻¹	4.173 ⁻²	5.119 ⁻³	0.957	1.291	-2.525 ⁻²	7.250 ⁻³	3.505 ⁻³
0.531	1.333	-1.660 ⁻¹	3.784 ⁻²	4.469 ⁻³	0.971	1.302	-6.868 ⁻³	6.570 ⁻³	2.749 ⁻³

Table 14. Continued ($x/H = 1$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.073	0.009	-5.428 ⁻²	7.783 ⁻²	-2.373 ⁻²	0.551	1.343	2.032 ⁻²	1.429 ⁻²	1.588 ⁻³
0.080	-0.006	-6.679 ⁻²	7.555 ⁻²	-2.606 ⁻²	0.571	1.350	2.228 ⁻²	1.354 ⁻²	9.513 ⁻⁴
0.087	-0.012	-4.490 ⁻²	7.451 ⁻²	-2.384 ⁻²	0.573	1.358	-1.629 ⁻³	1.248 ⁻²	1.607 ⁻³
0.097	-0.012	-6.254 ⁻²	7.712 ⁻²	-2.658 ⁻²	0.591	1.338	2.496 ⁻²	1.914 ⁻²	2.948 ⁻³
0.107	-0.021	-6.639 ⁻²	8.440 ⁻²	-2.981 ⁻²	0.611	1.337	2.827 ⁻²	1.568 ⁻²	3.291 ⁻³
0.117	0.131	-8.498 ⁻²	9.804 ⁻²	-3.831 ⁻²	0.627	1.352	3.184 ⁻²	1.739 ⁻²	2.736 ⁻³
0.127	0.140	-8.870 ⁻²	1.021 ⁻¹	-3.793 ⁻²	0.631	1.343	1.606 ⁻²	1.461 ⁻²	3.795 ⁻³
0.137	0.369	-1.344 ⁻¹	1.117 ⁻¹	-3.701 ⁻²	0.651	1.346	5.393 ⁻²	1.224 ⁻²	2.000 ⁻³
0.147	0.257	-1.224 ⁻¹	1.066 ⁻¹	-4.471 ⁻²	0.653	1.345	3.668 ⁻²	1.986 ⁻²	3.979 ⁻³
0.157	0.322	-1.350 ⁻¹	1.112 ⁻¹	-4.334 ⁻²	0.671	1.327	-6.413 ⁻³	1.910 ⁻²	4.889 ⁻³
0.167	0.320	-1.381 ⁻¹	1.102 ⁻¹	-4.655 ⁻²	0.684	1.344	2.826 ⁻²	1.429 ⁻²	4.377 ⁻³
0.177	0.416	-1.322 ⁻¹	1.208 ⁻¹	-4.265 ⁻²	0.697	1.328	5.982 ⁻²	1.482 ⁻²	3.446 ⁻³
0.187	0.507	-1.227 ⁻¹	1.302 ⁻¹	-4.956 ⁻²	0.707	1.346	4.233 ⁻²	1.830 ⁻²	3.974 ⁻³
0.200	0.424	-1.457 ⁻¹	1.246 ⁻¹	-4.636 ⁻²	0.711	1.338	3.073 ⁻²	1.191 ⁻²	4.017 ⁻³
0.213	0.585	-1.754 ⁻¹	1.113 ⁻¹	-4.137 ⁻²	0.724	1.327	1.991 ⁻²	1.613 ⁻²	4.624 ⁻³
0.227	0.734	-1.645 ⁻¹	1.115 ⁻¹	-3.901 ⁻²	0.737	1.329	1.289 ⁻²	1.687 ⁻²	4.606 ⁻³
0.231	0.738	-1.526 ⁻¹	1.051 ⁻¹	-2.971 ⁻²	0.751	1.320	1.052 ⁻²	1.656 ⁻²	4.326 ⁻³
0.240	0.818	-1.579 ⁻¹	9.594 ⁻²	-2.086 ⁻²	0.764	1.324	1.232 ⁻²	1.571 ⁻²	4.803 ⁻³
0.253	0.832	-1.586 ⁻¹	9.149 ⁻²	-2.729 ⁻²	0.777	1.321	4.672 ⁻³	1.518 ⁻²	4.601 ⁻³
0.257	0.925	-1.378 ⁻¹	8.186 ⁻²	-1.607 ⁻²	0.791	1.327	2.411 ⁻²	1.460 ⁻²	4.598 ⁻³
0.267	0.960	-1.255 ⁻¹	9.092 ⁻²	-1.421 ⁻²	0.804	1.323	1.144 ⁻²	1.291 ⁻²	3.946 ⁻³
0.284	0.939	-1.498 ⁻¹	8.036 ⁻²	-1.787 ⁻²	0.814	1.316	1.110 ⁻²	1.640 ⁻²	4.868 ⁻³
0.293	1.012	-1.652 ⁻¹	6.299 ⁻²	-1.286 ⁻²	0.824	1.314	3.119 ⁻³	1.351 ⁻²	4.169 ⁻³
0.311	1.110	-1.004 ⁻¹	5.103 ⁻²	-8.707 ⁻³	0.834	1.322	1.187 ⁻²	1.151 ⁻²	3.574 ⁻³
0.340	1.126	-1.372 ⁻¹	4.987 ⁻²	-9.994 ⁻³	0.844	1.309	-3.614 ⁻²	1.471 ⁻²	4.295 ⁻³
0.360	1.179	-8.017 ⁻²	4.429 ⁻²	-9.394 ⁻³	0.854	1.305	3.201 ⁻³	1.270 ⁻²	3.569 ⁻³
0.364	1.128	-1.194 ⁻¹	4.495 ⁻²	-7.510 ⁻³	0.864	1.320	8.025 ⁻³	9.972 ⁻³	3.263 ⁻³
0.380	1.185	-9.260 ⁻²	4.052 ⁻²	-6.300 ⁻³	0.874	1.315	-4.797 ⁻³	1.028 ⁻²	3.012 ⁻³
0.400	1.244	-1.070 ⁻¹	2.838 ⁻²	-1.800 ⁻³	0.884	1.319	1.122 ⁻³	9.554 ⁻³	3.250 ⁻³
0.417	1.242	-8.939 ⁻²	2.586 ⁻²	-4.277 ⁻³	0.894	1.316	-8.283 ⁻³	9.693 ⁻³	3.351 ⁻³
0.420	1.270	-4.694 ⁻²	2.377 ⁻²	-2.091 ⁻³	0.904	1.305	-1.660 ⁻²	9.509 ⁻³	2.779 ⁻³
0.440	1.272	-2.578 ⁻²	2.580 ⁻²	-2.805 ⁻³	0.911	1.302	-9.690 ⁻³	8.524 ⁻³	2.791 ⁻³
0.444	1.281	-4.854 ⁻²	2.290 ⁻²	-1.486 ⁻³	0.917	1.305	-1.601 ⁻²	7.937 ⁻³	2.678 ⁻³
0.460	1.302	-1.274 ⁻²	2.279 ⁻²	-2.216 ⁻³	0.924	1.308	-8.706 ⁻³	6.606 ⁻³	2.404 ⁻³
0.480	1.319	-7.710 ⁻³	1.851 ⁻²	-3.157 ⁻⁴	0.931	1.306	-4.594 ⁻³	6.373 ⁻³	2.485 ⁻³
0.491	1.313	-5.595 ⁻³	1.558 ⁻²	8.261 ⁻⁴	0.937	1.290	-1.636 ⁻²	8.125 ⁻³	3.486 ⁻³
0.500	1.337	-3.251 ⁻³	1.816 ⁻²	6.468 ⁻⁴	0.944	1.286	-1.842 ⁻²	7.093 ⁻³	3.319 ⁻³
0.511	1.328	5.505 ⁻³	1.598 ⁻²	2.861 ⁻⁴	0.951	1.283	-1.633 ⁻²	6.200 ⁻³	2.500 ⁻³
0.520	1.332	3.754 ⁻²	1.922 ⁻²	1.392 ⁻³	0.957	1.273	-1.863 ⁻²	6.547 ⁻³	2.870 ⁻³
0.531	1.335	1.378 ⁻²	1.562 ⁻²	1.886 ⁻³	0.964	1.262	-2.428 ⁻²	7.560 ⁻³	3.861 ⁻³
0.547	1.346	-1.424 ⁻²	2.154 ⁻²	2.091 ⁻³					

Table 14. Concluded ($x/H = 1$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.027	-0.064	-2.060 ⁻²	4.553 ⁻²	-7.327 ⁻³	0.487	1.339	-2.691 ⁻²	1.858 ⁻²	3.841 ⁻⁴
0.033	-0.049	-1.956 ⁻²	5.202 ⁻²	-9.842 ⁻³	0.500	1.352	5.643 ⁻³	1.971 ⁻²	1.193 ⁻³
0.040	-0.034	-2.599 ⁻²	5.912 ⁻²	-1.063 ⁻²	0.507	1.349	-3.025 ⁻²	1.899 ⁻²	4.747 ⁻³
0.047	-0.087	-2.317 ⁻²	5.184 ⁻²	-1.119 ⁻²	0.527	1.362	-1.590 ⁻²	1.560 ⁻²	3.409 ⁻³
0.053	-0.044	-2.122 ⁻²	5.689 ⁻²	-1.244 ⁻²	0.547	1.355	-8.095 ⁻³	1.858 ⁻²	4.522 ⁻³
0.060	0.034	-3.152 ⁻²	6.855 ⁻²	-1.715 ⁻²	0.567	1.354	5.860 ⁻³	1.778 ⁻²	5.235 ⁻³
0.067	0.021	-4.165 ⁻²	7.195 ⁻²	-2.328 ⁻²	0.587	1.339	3.230 ⁻²	1.881 ⁻²	5.941 ⁻³
0.073	0.128	-3.727 ⁻²	8.223 ⁻²	-2.569 ⁻²	0.607	1.336	-7.382 ⁻³	1.789 ⁻²	6.513 ⁻³
0.080	0.046	-4.512 ⁻²	7.759 ⁻²	-2.636 ⁻²	0.627	1.344	3.669 ⁻²	1.823 ⁻²	4.787 ⁻³
0.087	0.112	-4.489 ⁻²	8.683 ⁻²	-3.227 ⁻²	0.647	1.326	-1.637 ⁻²	1.908 ⁻²	7.403 ⁻³
0.097	0.131	-6.942 ⁻²	9.152 ⁻²	-3.692 ⁻²	0.653	1.330	1.872 ⁻²	1.988 ⁻²	5.607 ⁻³
0.107	0.100	-6.244 ⁻²	8.832 ⁻²	-3.555 ⁻²	0.667	1.342	4.375 ⁻²	1.753 ⁻²	6.229 ⁻³
0.117	0.171	-6.626 ⁻²	9.731 ⁻²	-4.199 ⁻²	0.694	1.328	2.573 ⁻²	1.759 ⁻²	6.719 ⁻³
0.127	0.202	-7.503 ⁻²	1.079 ⁻¹	-4.392 ⁻²	0.707	1.328	2.940 ⁻²	1.964 ⁻²	6.499 ⁻³
0.137	0.271	-8.023 ⁻²	1.077 ⁻¹	-4.070 ⁻²	0.760	1.317	-4.187 ⁻²	2.029 ⁻²	5.757 ⁻³
0.147	0.421	-1.016 ⁻¹	1.225 ⁻¹	-4.791 ⁻²	0.774	1.326	3.744 ⁻²	1.710 ⁻²	5.633 ⁻³
0.167	0.546	-1.122 ⁻¹	1.196 ⁻¹	-5.029 ⁻²	0.787	1.325	6.232 ⁻²	1.467 ⁻²	4.767 ⁻³
0.200	0.519	-1.253 ⁻¹	1.208 ⁻¹	-5.070 ⁻²	0.801	1.330	4.414 ⁻²	1.611 ⁻²	5.887 ⁻³
0.213	0.607	-1.315 ⁻¹	1.196 ⁻¹	-4.964 ⁻²	0.811	1.320	3.157 ⁻²	1.618 ⁻²	5.091 ⁻³
0.227	0.725	-1.411 ⁻¹	1.093 ⁻¹	-4.173 ⁻²	0.821	1.326	5.103 ⁻²	1.374 ⁻²	4.554 ⁻³
0.240	0.791	-1.382 ⁻¹	1.094 ⁻¹	-3.798 ⁻²	0.831	1.323	4.316 ⁻²	1.579 ⁻²	4.825 ⁻³
0.254	0.815	-1.506 ⁻¹	1.014 ⁻¹	-3.467 ⁻²	0.841	1.313	-1.553 ⁻²	1.657 ⁻²	4.844 ⁻³
0.267	0.842	-1.523 ⁻¹	9.440 ⁻²	-3.147 ⁻²	0.851	1.324	3.964 ⁻²	1.374 ⁻²	3.869 ⁻³
0.280	0.936	-1.459 ⁻¹	8.209 ⁻²	-2.629 ⁻²	0.861	1.322	3.680 ⁻²	1.270 ⁻²	3.628 ⁻³
0.293	0.932	-1.477 ⁻¹	9.013 ⁻²	-2.764 ⁻²	0.871	1.322	3.845 ⁻²	1.251 ⁻²	3.549 ⁻³
0.307	1.065	-1.458 ⁻¹	6.864 ⁻²	-2.099 ⁻²	0.881	1.314	1.599 ⁻²	1.355 ⁻²	3.909 ⁻³
0.334	1.059	-1.261 ⁻¹	5.794 ⁻²	-1.275 ⁻²	0.891	1.315	5.812 ⁻³	1.140 ⁻²	3.210 ⁻³
0.340	1.140	-1.256 ⁻¹	5.458 ⁻²	-1.439 ⁻²	0.901	1.316	5.762 ⁻³	1.006 ⁻²	2.833 ⁻³
0.360	1.212	-1.172 ⁻¹	4.363 ⁻²	-9.583 ⁻³	0.907	1.316	1.345 ⁻²	1.003 ⁻²	3.041 ⁻³
0.387	1.282	-6.669 ⁻²	2.901 ⁻²	-3.889 ⁻³	0.914	1.320	9.160 ⁻³	8.476 ⁻³	2.859 ⁻³
0.400	1.297	-1.195 ⁻¹	3.746 ⁻²	-4.912 ⁻³	0.921	1.311	9.520 ⁻³	8.601 ⁻³	2.197 ⁻³
0.414	1.278	-7.854 ⁻²	3.017 ⁻²	-5.539 ⁻³	0.927	1.311	5.204 ⁻³	7.626 ⁻³	2.362 ⁻³
0.420	1.289	-7.026 ⁻²	2.796 ⁻²	-1.210 ⁻³	0.934	1.313	1.535 ⁻²	7.107 ⁻³	2.278 ⁻³
0.440	1.315	-5.831 ⁻²	2.575 ⁻²	-2.087 ⁻³	0.941	1.300	-2.125 ⁻³	6.953 ⁻³	2.528 ⁻³
0.460	1.331	-2.500 ⁻²	2.403 ⁻²	6.151 ⁻⁴	0.947	1.305	6.145 ⁻³	5.910 ⁻³	2.126 ⁻³
0.467	1.341	-2.751 ⁻²	2.082 ⁻²	1.531 ⁻³	0.954	1.299	3.711 ⁻³	6.200 ⁻³	2.174 ⁻³
0.480	1.331	-2.126 ⁻²	2.028 ⁻²	1.015 ⁻³					

Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)

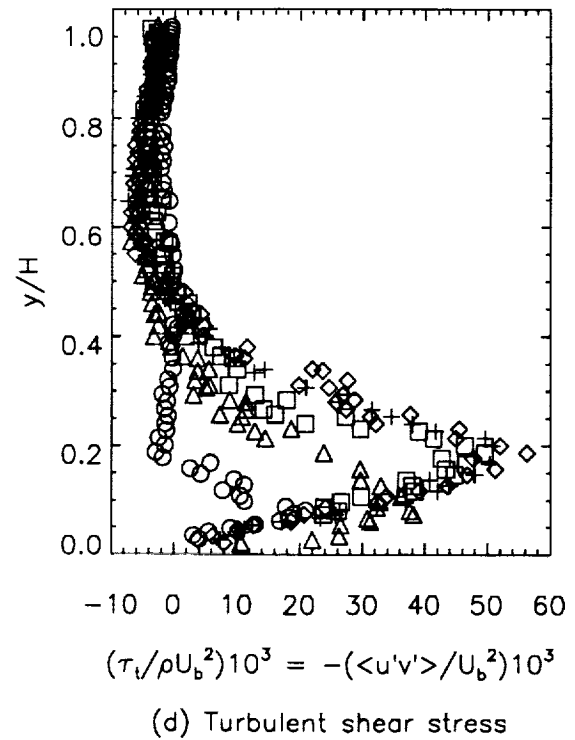
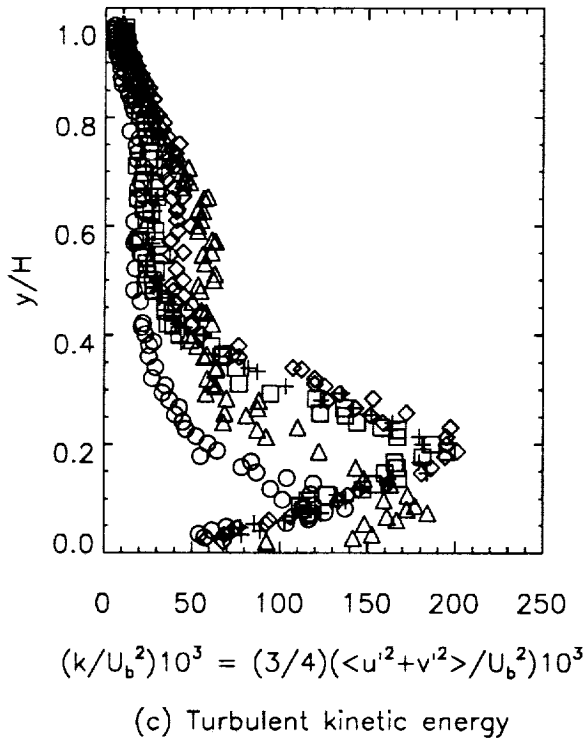
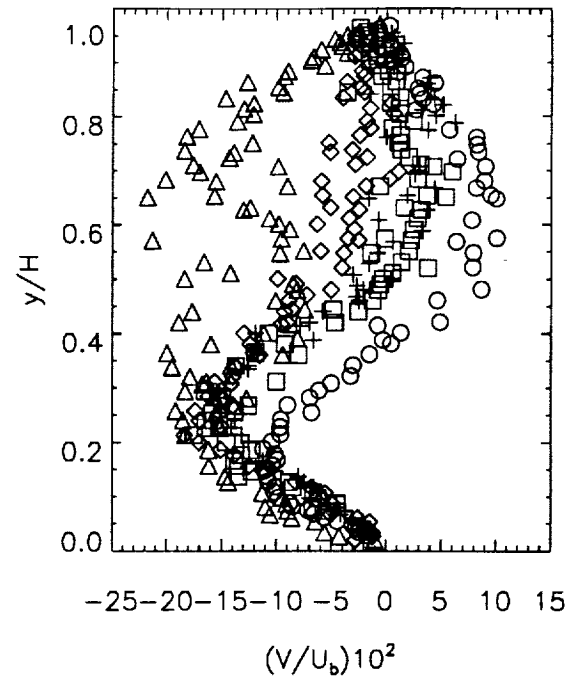
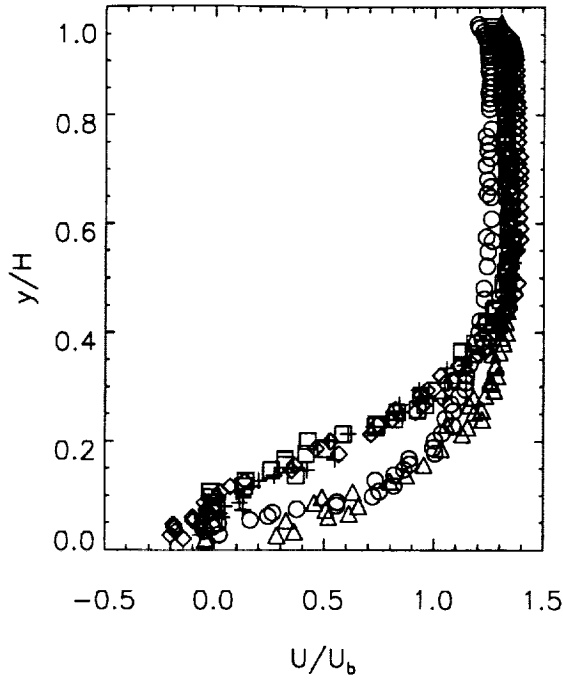


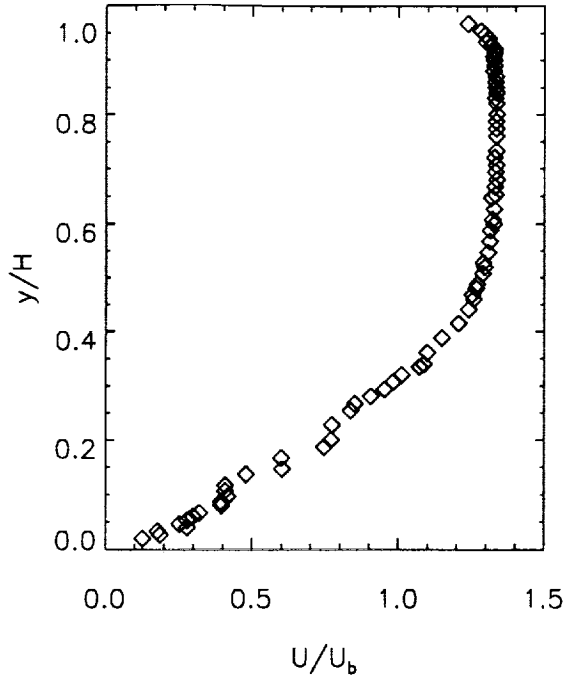
Figure 14. Summary of Table 14 ($x/H = 1$).

Table 15. LDV flowfield data in TAD ($x/H = 1.5$)

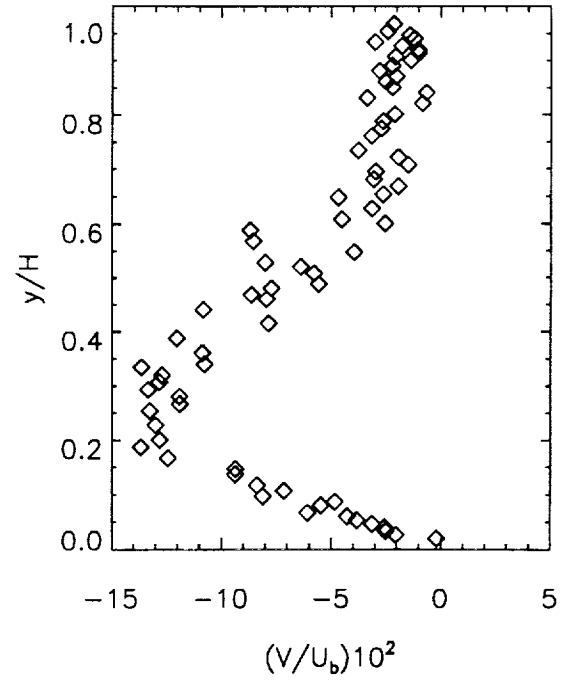
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.127	-2.016 ⁻³	4.468 ⁻²	-7.656 ⁻³	0.528	1.291	-8.003 ⁻²	3.084 ⁻²	-6.006 ⁻⁴
0.027	0.187	-2.054 ⁻²	5.000 ⁻²	-9.512 ⁻³	0.547	1.308	-3.956 ⁻²	2.723 ⁻²	8.573 ⁻⁴
0.033	0.177	-2.515 ⁻²	4.686 ⁻²	-8.485 ⁻³	0.568	1.313	-8.545 ⁻²	2.795 ⁻²	3.261 ⁻³
0.040	0.279	-2.571 ⁻²	6.517 ⁻²	-1.390 ⁻²	0.588	1.315	-8.681 ⁻²	2.742 ⁻²	4.133 ⁻³
0.047	0.253	-3.134 ⁻²	5.488 ⁻²	-1.583 ⁻²	0.600	1.327	-2.553 ⁻²	2.447 ⁻²	1.953 ⁻³
0.053	0.278	-3.827 ⁻²	6.178 ⁻²	-1.854 ⁻²	0.608	1.322	-4.519 ⁻²	2.642 ⁻²	2.891 ⁻³
0.060	0.299	-4.273 ⁻²	6.606 ⁻²	-1.601 ⁻²	0.627	1.328	-3.143 ⁻²	2.515 ⁻²	3.585 ⁻³
0.067	0.320	-6.082 ⁻²	7.036 ⁻²	-2.036 ⁻²	0.648	1.319	-4.674 ⁻²	2.531 ⁻²	4.136 ⁻³
0.080	0.395	-5.468 ⁻²	8.265 ⁻²	-2.612 ⁻²	0.653	1.333	-2.634 ⁻²	2.585 ⁻²	3.785 ⁻³
0.087	0.394	-4.831 ⁻²	8.128 ⁻²	-2.454 ⁻²	0.668	1.331	-1.951 ⁻²	2.299 ⁻²	4.232 ⁻³
0.097	0.416	-8.113 ⁻²	8.525 ⁻²	-2.525 ⁻²	0.681	1.337	-3.069 ⁻²	2.364 ⁻²	4.334 ⁻³
0.107	0.408	-7.150 ⁻²	8.641 ⁻²	-3.053 ⁻²	0.695	1.332	-2.985 ⁻²	2.276 ⁻²	4.442 ⁻³
0.117	0.408	-8.378 ⁻²	8.422 ⁻²	-2.954 ⁻²	0.707	1.335	-1.496 ⁻²	2.259 ⁻²	4.535 ⁻³
0.137	0.479	-9.371 ⁻²	9.185 ⁻²	-3.193 ⁻²	0.721	1.329	-1.946 ⁻²	2.177 ⁻²	4.363 ⁻³
0.147	0.602	-9.362 ⁻²	9.645 ⁻²	-3.444 ⁻²	0.734	1.335	-3.766 ⁻²	2.372 ⁻²	4.445 ⁻³
0.167	0.599	-1.243 ⁻¹	9.917 ⁻²	-3.830 ⁻²	0.761	1.335	-3.161 ⁻²	2.283 ⁻²	4.938 ⁻³
0.187	0.746	-1.368 ⁻¹	9.361 ⁻²	-3.634 ⁻²	0.775	1.335	-2.722 ⁻²	1.866 ⁻²	4.150 ⁻³
0.200	0.770	-1.281 ⁻¹	8.874 ⁻²	-3.412 ⁻²	0.788	1.334	-2.643 ⁻²	1.731 ⁻²	4.059 ⁻³
0.227	0.772	-1.300 ⁻¹	9.475 ⁻²	-3.950 ⁻²	0.801	1.337	-2.105 ⁻²	1.727 ⁻²	3.834 ⁻³
0.254	0.836	-1.327 ⁻¹	9.675 ⁻²	-3.683 ⁻²	0.821	1.335	-8.436 ⁻³	1.490 ⁻²	3.384 ⁻³
0.267	0.850	-1.190 ⁻¹	9.174 ⁻²	-3.477 ⁻²	0.831	1.332	-3.363 ⁻²	1.493 ⁻²	3.720 ⁻³
0.281	0.905	-1.191 ⁻¹	8.490 ⁻²	-3.199 ⁻²	0.841	1.336	-6.607 ⁻³	1.354 ⁻²	3.332 ⁻³
0.293	0.952	-1.334 ⁻¹	8.161 ⁻²	-3.184 ⁻²	0.851	1.333	-2.211 ⁻²	1.364 ⁻²	3.155 ⁻³
0.307	0.983	-1.283 ⁻¹	7.491 ⁻²	-2.596 ⁻²	0.861	1.332	-2.494 ⁻²	1.305 ⁻²	3.152 ⁻³
0.320	1.010	-1.271 ⁻¹	8.070 ⁻²	-3.091 ⁻²	0.871	1.334	-2.030 ⁻²	1.156 ⁻²	3.038 ⁻³
0.335	1.072	-1.365 ⁻¹	6.287 ⁻²	-2.015 ⁻²	0.881	1.325	-2.802 ⁻²	1.089 ⁻²	2.754 ⁻³
0.340	1.087	-1.077 ⁻¹	6.481 ⁻²	-2.136 ⁻²	0.891	1.329	-2.209 ⁻²	9.726 ⁻³	2.921 ⁻³
0.361	1.099	-1.087 ⁻¹	5.851 ⁻²	-1.707 ⁻²	0.901	1.327	-1.364 ⁻²	8.690 ⁻³	2.348 ⁻³
0.388	1.149	-1.204 ⁻¹	4.609 ⁻²	-1.162 ⁻²	0.908	1.324	-2.072 ⁻²	7.945 ⁻³	2.313 ⁻³
0.415	1.206	-7.861 ⁻²	3.917 ⁻²	-8.158 ⁻³	0.915	1.329	-9.989 ⁻³	7.377 ⁻³	2.209 ⁻³
0.441	1.240	-1.082 ⁻¹	3.734 ⁻²	-6.917 ⁻³	0.921	1.328	-1.029 ⁻²	7.361 ⁻³	2.347 ⁻³
0.460	1.258	-7.949 ⁻²	3.486 ⁻²	-4.974 ⁻³	0.928	1.318	-1.773 ⁻²	7.179 ⁻³	2.279 ⁻³
0.468	1.253	-8.635 ⁻²	3.296 ⁻²	-5.269 ⁻³	0.935	1.299	-2.990 ⁻²	7.849 ⁻³	2.706 ⁻³
0.480	1.267	-7.734 ⁻²	4.108 ⁻²	-5.060 ⁻³	0.941	1.308	-1.197 ⁻²	7.372 ⁻³	2.807 ⁻³
0.488	1.269	-5.576 ⁻²	2.776 ⁻²	-1.449 ⁻³	0.948	1.296	-1.409 ⁻²	7.275 ⁻³	2.697 ⁻³
0.508	1.289	-5.786 ⁻²	2.713 ⁻²	-2.517 ⁻³	0.955	1.282	-2.413 ⁻²	7.824 ⁻³	3.173 ⁻³
0.520	1.295	-6.390 ⁻²	3.490 ⁻²	2.673 ⁻⁴	0.968	1.237	-2.138 ⁻²	9.617 ⁻³	3.329 ⁻³

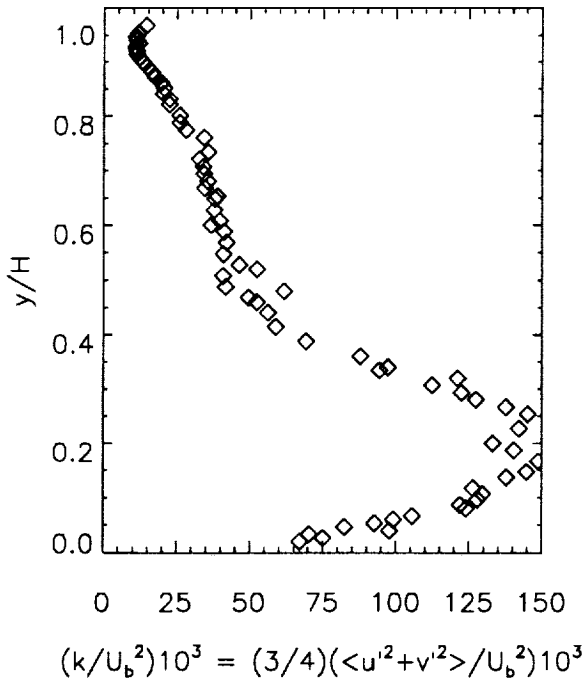
Legend: $Re = 1 \times 10^6$; $z/H = 0(\diamond)$



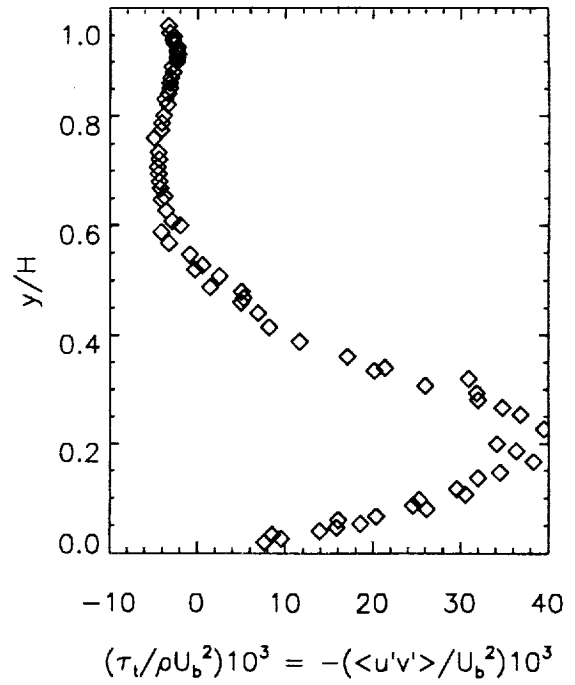
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 15. Summary of Table 15 ($x/H = 1.5$).

Table 16. LDV flowfield data in TAD ($x/H = 2$)(Re = 1×10^5 , $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.017	0.581	-2.308 ⁻²	1.598 ⁻²	-2.222 ⁻³	0.526	1.159	3.307 ⁻²	1.868 ⁻²	-3.053 ⁻⁴
0.024	0.564	-2.597 ⁻²	1.980 ⁻²	-4.168 ⁻³	0.544	1.156	5.927 ⁻²	1.459 ⁻²	-1.050 ⁻³
0.031	0.528	-2.877 ⁻²	2.258 ⁻²	-5.782 ⁻³	0.546	1.161	4.139 ⁻²	1.699 ⁻²	-7.428 ⁻⁴
0.037	0.523	-3.503 ⁻²	2.294 ⁻²	-5.839 ⁻³	0.566	1.169	4.641 ⁻²	1.426 ⁻²	-5.237 ⁻⁴
0.044	0.532	-3.791 ⁻²	2.505 ⁻²	-7.175 ⁻³	0.571	1.168	3.911 ⁻²	1.491 ⁻²	-2.814 ⁻⁴
0.051	0.569	-3.795 ⁻²	2.549 ⁻²	-5.992 ⁻³	0.586	1.176	4.352 ⁻²	1.499 ⁻²	3.185 ⁻⁴
0.057	0.618	-3.436 ⁻²	2.869 ⁻²	-4.945 ⁻³	0.597	1.174	7.366 ⁻²	1.190 ⁻²	-4.043 ⁻⁴
0.064	0.675	-3.925 ⁻²	2.908 ⁻²	-5.095 ⁻³	0.606	1.183	4.372 ⁻²	1.103 ⁻²	1.126 ⁻⁴
0.071	0.701	-4.260 ⁻²	3.244 ⁻²	-5.329 ⁻³	0.624	1.179	6.548 ⁻²	1.322 ⁻²	4.911 ⁻⁴
0.077	0.652	-4.193 ⁻²	3.103 ⁻²	-6.924 ⁻³	0.646	1.189	6.665 ⁻²	9.748 ⁻³	1.669 ⁻⁴
0.084	0.753	-4.284 ⁻²	3.388 ⁻²	-5.235 ⁻³	0.651	1.183	7.839 ⁻²	1.193 ⁻²	2.151 ⁻⁴
0.094	0.778	-4.177 ⁻²	3.305 ⁻²	-5.037 ⁻³	0.666	1.188	4.081 ⁻²	1.452 ⁻²	1.146 ⁻³
0.124	0.795	-6.191 ⁻²	3.192 ⁻²	-6.874 ⁻³	0.677	1.187	7.023 ⁻²	1.205 ⁻²	4.340 ⁻⁴
0.144	0.850	-6.974 ⁻²	3.052 ⁻²	-6.353 ⁻³	0.679	1.192	5.032 ⁻²	1.165 ⁻²	8.715 ⁻⁴
0.174	0.864	-5.037 ⁻²	3.305 ⁻²	-6.387 ⁻³	0.704	1.187	6.512 ⁻²	1.392 ⁻²	1.041 ⁻³
0.184	0.877	-6.398 ⁻²	3.538 ⁻²	-5.145 ⁻³	0.706	1.193	5.054 ⁻²	1.195 ⁻²	1.387 ⁻³
0.197	0.867	-5.549 ⁻²	3.705 ⁻²	-5.633 ⁻³	0.731	1.192	6.657 ⁻²	1.199 ⁻²	9.523 ⁻⁴
0.211	0.897	-6.017 ⁻²	3.476 ⁻²	-5.481 ⁻³	0.733	1.197	5.320 ⁻²	9.950 ⁻³	7.508 ⁻⁴
0.224	1.003	-7.702 ⁻²	3.071 ⁻²	-5.551 ⁻³	0.746	1.204	5.221 ⁻²	8.451 ⁻³	1.207 ⁻³
0.237	0.963	-5.794 ⁻²	2.995 ⁻²	-4.218 ⁻³	0.757	1.197	7.215 ⁻²	9.984 ⁻³	1.064 ⁻³
0.277	1.048	-6.365 ⁻²	2.910 ⁻²	-3.765 ⁻³	0.759	1.207	3.318 ⁻²	8.545 ⁻³	1.558 ⁻³
0.279	1.060	-6.795 ⁻²	2.785 ⁻²	-3.094 ⁻³	0.773	1.204	4.146 ⁻²	9.934 ⁻³	1.149 ⁻³
0.291	1.023	-4.887 ⁻²	3.022 ⁻²	-4.258 ⁻³	0.786	1.198	2.188 ⁻²	1.079 ⁻²	1.759 ⁻³
0.304	1.047	-5.887 ⁻²	2.866 ⁻²	-3.455 ⁻³	0.799	1.204	3.367 ⁻²	8.744 ⁻³	1.477 ⁻³
0.306	1.071	-5.304 ⁻²	2.709 ⁻²	-3.144 ⁻³	0.809	1.201	3.167 ⁻²	9.417 ⁻³	1.401 ⁻³
0.317	1.086	-4.286 ⁻²	2.852 ⁻²	-2.695 ⁻³	0.819	1.202	1.641 ⁻²	9.109 ⁻³	1.227 ⁻³
0.333	1.089	-4.011 ⁻²	2.950 ⁻²	-3.698 ⁻³	0.829	1.203	2.610 ⁻²	8.592 ⁻³	1.723 ⁻³
0.357	1.086	-3.079 ⁻³	2.405 ⁻²	-1.904 ⁻³	0.839	1.199	1.421 ⁻²	9.308 ⁻³	1.604 ⁻³
0.359	1.102	-3.435 ⁻²	2.335 ⁻²	-2.223 ⁻³	0.849	1.210	2.874 ⁻²	7.073 ⁻³	1.116 ⁻³
0.386	1.108	-3.318 ⁻²	2.026 ⁻²	-1.230 ⁻³	0.859	1.209	2.881 ⁻²	6.348 ⁻³	1.493 ⁻³
0.397	1.104	-2.269 ⁻²	2.321 ⁻²	-1.517 ⁻³	0.869	1.202	1.486 ⁻²	7.291 ⁻³	1.617 ⁻³
0.413	1.122	1.600 ⁻²	1.786 ⁻²	-1.729 ⁻³	0.879	1.204	1.097 ⁻²	6.287 ⁻³	1.366 ⁻³
0.417	1.109	-1.761 ⁻²	2.577 ⁻²	-1.528 ⁻³	0.889	1.209	9.413 ⁻³	5.934 ⁻³	1.348 ⁻³
0.437	1.107	1.293 ⁻²	2.078 ⁻²	-1.766 ⁻³	0.899	1.209	1.465 ⁻²	5.527 ⁻³	1.367 ⁻³
0.439	1.126	-1.435 ⁻²	2.402 ⁻²	-2.198 ⁻³	0.906	1.206	1.095 ⁻²	5.321 ⁻³	1.276 ⁻³
0.457	1.138	1.411 ⁻²	2.011 ⁻²	-7.984 ⁻⁴	0.913	1.205	9.315 ⁻³	5.205 ⁻³	1.510 ⁻³
0.466	1.146	2.805 ⁻²	1.640 ⁻²	-1.378 ⁻³	0.919	1.207	8.623 ⁻³	5.216 ⁻³	1.473 ⁻³
0.477	1.135	2.598 ⁻²	1.640 ⁻²	-8.289 ⁻⁴	0.926	1.205	3.571 ⁻³	4.731 ⁻³	1.359 ⁻³
0.486	1.155	2.217 ⁻²	1.917 ⁻²	-9.938 ⁻⁴	0.933	1.202	1.031 ⁻³	5.245 ⁻³	1.593 ⁻³
0.497	1.146	2.765 ⁻²	1.808 ⁻²	-9.183 ⁻⁴	0.939	1.206	4.533 ⁻³	4.720 ⁻³	1.361 ⁻³
0.506	1.155	2.051 ⁻²	1.508 ⁻²	-1.498 ⁻³	0.946	1.196	-1.233 ⁻³	5.446 ⁻³	1.653 ⁻³
0.517	1.155	3.092 ⁻²	1.310 ⁻²	-2.177 ⁻⁴					

Table 16. Continued ($x/H = 2$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.471	-1.585 ⁻²	3.879 ⁻²	-3.873 ⁻³	0.500	1.191	-5.941 ⁻²	3.587 ⁻²	-1.005 ⁻²
0.027	0.421	-1.752 ⁻²	4.098 ⁻²	-6.674 ⁻³	0.509	1.186	-5.993 ⁻²	3.233 ⁻²	-3.018 ⁻³
0.033	0.414	-1.769 ⁻²	4.191 ⁻²	-7.116 ⁻³	0.520	1.206	-8.437 ⁻²	3.642 ⁻²	-5.405 ⁻³
0.040	0.417	-2.265 ⁻²	4.365 ⁻²	-7.891 ⁻³	0.529	1.187	-4.191 ⁻²	3.208 ⁻²	-5.541 ⁻³
0.047	0.474	-2.369 ⁻²	4.622 ⁻²	-7.639 ⁻³	0.569	1.221	-5.600 ⁻²	2.806 ⁻²	-2.021 ⁻⁴
0.053	0.472	-2.353 ⁻²	4.759 ⁻²	-8.833 ⁻³	0.589	1.229	-4.904 ⁻²	2.639 ⁻²	-6.033 ⁻⁴
0.067	0.522	-2.955 ⁻²	5.761 ⁻²	-1.510 ⁻²	0.600	1.241	-4.258 ⁻²	3.078 ⁻²	-2.013 ⁻⁴
0.073	0.564	-5.231 ⁻²	5.780 ⁻²	-1.284 ⁻²	0.609	1.225	-3.414 ⁻²	2.524 ⁻²	-9.690 ⁻⁴
0.080	0.607	-5.530 ⁻²	5.979 ⁻²	-1.717 ⁻²	0.627	1.251	-5.558 ⁻²	2.964 ⁻²	1.605 ⁻³
0.087	0.630	-4.833 ⁻²	6.034 ⁻²	-1.484 ⁻²	0.629	1.241	-1.744 ⁻²	2.232 ⁻²	1.677 ⁻⁴
0.097	0.589	-4.456 ⁻²	6.250 ⁻²	-1.714 ⁻²	0.649	1.247	-2.243 ⁻²	2.233 ⁻²	9.812 ⁻⁴
0.107	0.577	-4.565 ⁻²	6.565 ⁻²	-2.031 ⁻²	0.653	1.257	-4.408 ⁻²	2.870 ⁻²	1.504 ⁻³
0.117	0.614	-5.570 ⁻²	6.412 ⁻²	-2.032 ⁻²	0.669	1.254	-3.831 ⁻²	2.075 ⁻²	8.628 ⁻⁴
0.147	0.715	-7.836 ⁻²	7.153 ⁻²	-2.764 ⁻²	0.682	1.250	-3.768 ⁻²	2.221 ⁻²	2.575 ⁻³
0.157	0.657	-5.055 ⁻²	7.083 ⁻²	-2.776 ⁻²	0.695	1.260	-1.027 ⁻²	1.806 ⁻²	1.951 ⁻³
0.177	0.704	-7.268 ⁻²	7.057 ⁻²	-2.665 ⁻²	0.709	1.261	-1.150 ⁻²	1.936 ⁻²	1.812 ⁻³
0.187	0.771	-7.616 ⁻²	6.963 ⁻²	-2.824 ⁻²	0.722	1.265	-1.978 ⁻³	1.616 ⁻²	2.232 ⁻³
0.200	0.776	-7.593 ⁻²	6.993 ⁻²	-2.861 ⁻²	0.735	1.257	-2.330 ⁻²	2.051 ⁻²	3.059 ⁻³
0.213	0.835	-9.791 ⁻²	7.466 ⁻²	-2.861 ⁻²	0.749	1.260	-2.164 ⁻²	2.048 ⁻²	3.098 ⁻³
0.229	0.812	-8.299 ⁻²	6.894 ⁻²	-2.819 ⁻²	0.762	1.263	-3.320 ⁻²	1.655 ⁻²	2.905 ⁻³
0.240	0.901	-9.720 ⁻²	6.784 ⁻²	-2.610 ⁻²	0.775	1.261	-1.497 ⁻²	1.549 ⁻²	2.778 ⁻³
0.255	0.854	-7.592 ⁻²	6.655 ⁻²	-2.720 ⁻²	0.789	1.267	-1.238 ⁻²	1.526 ⁻²	3.113 ⁻³
0.267	0.932	-9.468 ⁻²	7.152 ⁻²	-2.832 ⁻²	0.802	1.272	-2.090 ⁻³	1.332 ⁻²	2.263 ⁻³
0.280	0.945	-9.907 ⁻²	6.645 ⁻²	-2.922 ⁻²	0.812	1.271	-2.091 ⁻²	1.358 ⁻²	2.442 ⁻³
0.293	0.953	-8.598 ⁻²	6.638 ⁻²	-2.732 ⁻²	0.822	1.266	-2.517 ⁻²	1.369 ⁻²	2.509 ⁻³
0.307	0.954	-8.256 ⁻²	6.051 ⁻²	-2.253 ⁻²	0.832	1.269	-3.945 ⁻²	1.217 ⁻²	2.533 ⁻³
0.309	0.940	-8.424 ⁻²	5.959 ⁻²	-2.457 ⁻²	0.852	1.262	-4.661 ⁻²	1.182 ⁻²	2.766 ⁻³
0.320	0.975	-7.863 ⁻²	6.421 ⁻²	-2.362 ⁻²	0.862	1.271	-2.645 ⁻²	1.069 ⁻²	2.430 ⁻³
0.335	0.979	-5.035 ⁻²	5.433 ⁻²	-1.677 ⁻²	0.872	1.272	-2.109 ⁻²	1.004 ⁻²	2.802 ⁻³
0.360	1.050	-9.984 ⁻²	5.619 ⁻²	-2.015 ⁻²	0.882	1.263	-3.053 ⁻²	9.221 ⁻³	2.590 ⁻³
0.362	1.029	-8.336 ⁻²	4.984 ⁻²	-1.801 ⁻²	0.892	1.273	-2.373 ⁻²	7.760 ⁻³	2.211 ⁻³
0.380	1.075	-9.538 ⁻²	5.342 ⁻²	-1.852 ⁻²	0.902	1.269	-1.253 ⁻²	8.227 ⁻³	2.283 ⁻³
0.400	1.072	-8.186 ⁻²	4.752 ⁻²	-1.512 ⁻²	0.909	1.268	-2.752 ⁻²	8.523 ⁻³	2.434 ⁻³
0.415	1.082	-3.358 ⁻²	4.471 ⁻²	-1.502 ⁻²	0.915	1.268	-1.433 ⁻²	7.798 ⁻³	2.353 ⁻³
0.420	1.097	-9.200 ⁻²	5.111 ⁻²	-1.658 ⁻²	0.922	1.268	-1.250 ⁻²	7.823 ⁻³	2.568 ⁻³
0.440	1.153	-8.269 ⁻²	4.122 ⁻²	-1.117 ⁻²	0.929	1.255	-2.163 ⁻²	7.461 ⁻³	2.459 ⁻³
0.442	1.113	-4.826 ⁻²	4.213 ⁻²	-1.270 ⁻²	0.935	1.249	-2.244 ⁻²	7.600 ⁻³	2.640 ⁻³
0.460	1.163	-7.141 ⁻²	4.482 ⁻²	-1.147 ⁻²	0.942	1.237	-2.271 ⁻²	7.959 ⁻³	2.607 ⁻³
0.469	1.141	-6.129 ⁻²	4.017 ⁻²	-1.022 ⁻²	0.949	1.244	-1.386 ⁻²	7.565 ⁻³	2.661 ⁻³
0.480	1.187	-6.501 ⁻²	3.617 ⁻²	-6.100 ⁻³	0.955	1.224	-1.877 ⁻²	8.688 ⁻³	2.515 ⁻³
0.489	1.155	-3.866 ⁻²	3.772 ⁻²	-1.043 ⁻²					

Table 16. Continued ($x/H = 2$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.490	-1.237 ⁻²	4.821 ⁻²	-5.924 ⁻³	0.567	1.215	-1.702 ⁻¹	3.695 ⁻²	-3.850 ⁻³
0.027	0.586	-1.950 ⁻²	4.551 ⁻²	-5.296 ⁻³	0.587	1.221	-1.790 ⁻¹	3.600 ⁻²	-3.252 ⁻³
0.033	0.659	-2.421 ⁻²	4.862 ⁻²	-8.146 ⁻³	0.600	1.234	-6.614 ⁻²	2.757 ⁻²	1.429 ⁻³
0.040	0.772	-4.216 ⁻²	4.930 ⁻²	-8.673 ⁻³	0.627	1.227	-9.167 ⁻²	3.128 ⁻²	-4.981 ⁻³
0.067	0.663	-3.118 ⁻²	4.475 ⁻²	-1.103 ⁻²	0.647	1.233	-1.254 ⁻¹	3.274 ⁻²	-5.701 ⁻⁴
0.073	0.841	-6.535 ⁻²	4.916 ⁻²	-1.296 ⁻²	0.653	1.237	-5.711 ⁻²	2.533 ⁻²	1.955 ⁻³
0.080	0.855	-6.922 ⁻²	5.035 ⁻²	-1.307 ⁻²	0.667	1.236	-1.202 ⁻¹	3.094 ⁻²	-8.679 ⁻⁴
0.087	0.814	-5.194 ⁻²	5.420 ⁻²	-1.510 ⁻²	0.680	1.241	-8.740 ⁻²	2.833 ⁻²	9.942 ⁻⁴
0.097	0.829	-5.772 ⁻²	5.264 ⁻²	-1.425 ⁻²	0.694	1.237	-6.760 ⁻²	2.956 ⁻²	1.109 ⁻³
0.107	0.939	-9.573 ⁻²	4.647 ⁻²	-1.508 ⁻²	0.707	1.244	-9.035 ⁻²	2.565 ⁻²	1.543 ⁻³
0.117	0.930	-9.026 ⁻²	4.795 ⁻²	-1.712 ⁻²	0.721	1.243	-9.905 ⁻²	2.893 ⁻²	1.875 ⁻⁴
0.127	0.851	-5.138 ⁻²	5.354 ⁻²	-1.527 ⁻²	0.734	1.244	-8.916 ⁻²	2.618 ⁻²	8.892 ⁻⁴
0.137	0.873	-7.380 ⁻²	5.426 ⁻²	-1.590 ⁻²	0.748	1.243	-1.175 ⁻¹	2.981 ⁻²	1.583 ⁻³
0.167	0.962	-8.743 ⁻²	5.166 ⁻²	-1.688 ⁻²	0.760	1.246	-1.337 ⁻¹	2.409 ⁻²	1.532 ⁻³
0.177	0.979	-1.142 ⁻¹	5.052 ⁻²	-1.865 ⁻²	0.774	1.253	-1.194 ⁻¹	2.537 ⁻²	1.095 ⁻³
0.200	1.003	-1.028 ⁻¹	4.714 ⁻²	-1.845 ⁻²	0.788	1.237	-1.758 ⁻¹	2.280 ⁻²	-2.354 ⁻⁴
0.213	0.954	-6.961 ⁻²	5.310 ⁻²	-1.988 ⁻²	0.801	1.253	-1.747 ⁻¹	2.495 ⁻²	1.907 ⁻³
0.227	0.999	-1.134 ⁻¹	4.899 ⁻²	-1.927 ⁻²	0.812	1.257	-1.490 ⁻¹	2.167 ⁻²	2.648 ⁻³
0.240	1.069	-1.251 ⁻¹	4.187 ⁻²	-1.490 ⁻²	0.822	1.256	-7.302 ⁻²	2.175 ⁻²	2.449 ⁻³
0.267	1.069	-1.140 ⁻¹	4.395 ⁻²	-1.416 ⁻²	0.832	1.260	-1.176 ⁻¹	2.242 ⁻²	1.884 ⁻³
0.280	1.082	-1.022 ⁻¹	4.267 ⁻²	-1.340 ⁻²	0.842	1.256	-1.253 ⁻¹	1.913 ⁻²	2.096 ⁻³
0.282	1.074	-1.206 ⁻¹	4.975 ⁻²	-1.667 ⁻²	0.852	1.254	-1.680 ⁻¹	1.459 ⁻²	1.417 ⁻³
0.307	1.098	-1.099 ⁻¹	4.267 ⁻²	-1.368 ⁻²	0.862	1.255	-1.561 ⁻¹	1.418 ⁻²	1.516 ⁻³
0.320	1.093	-1.107 ⁻¹	4.621 ⁻²	-1.588 ⁻²	0.872	1.254	-1.275 ⁻¹	1.713 ⁻²	1.627 ⁻³
0.340	1.139	-1.435 ⁻¹	4.141 ⁻²	-1.134 ⁻²	0.882	1.249	-1.335 ⁻¹	1.257 ⁻²	8.707 ⁻⁴
0.360	1.102	-6.735 ⁻²	3.733 ⁻²	-1.145 ⁻²	0.892	1.254	-1.182 ⁻¹	1.125 ⁻²	1.829 ⁻³
0.362	1.125	-1.377 ⁻¹	4.617 ⁻²	-1.567 ⁻²	0.902	1.255	-9.459 ⁻²	1.325 ⁻²	2.272 ⁻³
0.380	1.145	-7.839 ⁻²	3.442 ⁻²	-7.354 ⁻³	0.909	1.252	-1.230 ⁻¹	8.272 ⁻³	1.673 ⁻³
0.389	1.097	-8.475 ⁻²	4.619 ⁻²	-1.430 ⁻²	0.915	1.256	-8.658 ⁻²	9.365 ⁻³	1.963 ⁻³
0.400	1.122	-6.879 ⁻²	3.969 ⁻²	-1.032 ⁻²	0.922	1.253	-8.623 ⁻²	7.604 ⁻³	1.421 ⁻³
0.420	1.168	-1.267 ⁻¹	3.874 ⁻²	-7.909 ⁻³	0.929	1.246	-7.821 ⁻²	6.588 ⁻³	1.139 ⁻³
0.440	1.173	-8.047 ⁻²	3.538 ⁻²	-5.923 ⁻³	0.935	1.246	-6.557 ⁻²	6.825 ⁻³	1.718 ⁻³
0.442	1.137	-8.129 ⁻²	4.264 ⁻²	-1.173 ⁻²	0.942	1.244	-4.327 ⁻²	6.101 ⁻³	1.750 ⁻³
0.460	1.177	-7.104 ⁻²	3.517 ⁻²	-7.720 ⁻³	0.949	1.216	-5.125 ⁻²	7.237 ⁻³	2.041 ⁻³
0.500	1.198	-9.833 ⁻²	3.544 ⁻²	-4.776 ⁻³	0.955	1.211	-3.058 ⁻²	9.031 ⁻³	3.531 ⁻³
0.527	1.212	-1.850 ⁻¹	3.538 ⁻²	-2.012 ⁻³	0.962	1.206	-1.551 ⁻²	7.010 ⁻³	2.065 ⁻³
0.547	1.207	-9.332 ⁻²	3.307 ⁻²	-2.790 ⁻³					

Table 16. Continued ($x/H = 2$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

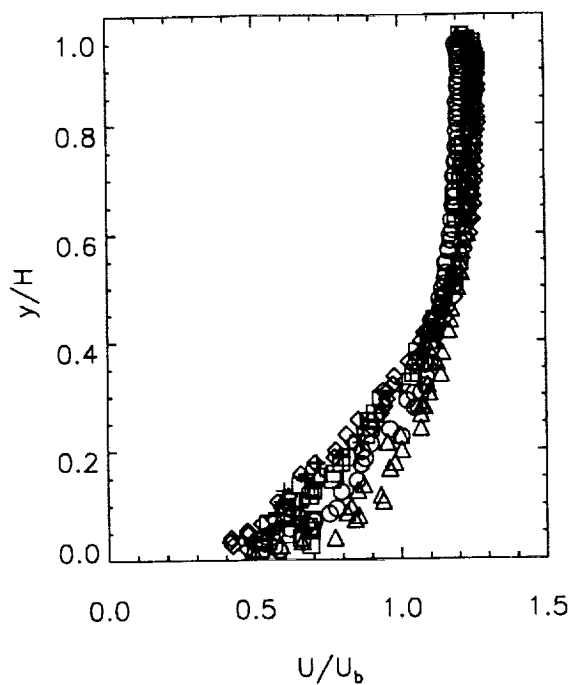
y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.515	-1.387 ⁻²	3.431 ⁻²	-4.094 ⁻³	0.520	1.188	-3.467 ⁻²	2.453 ⁻²	-3.434 ⁻³
0.027	0.688	-2.667 ⁻²	4.014 ⁻²	-5.532 ⁻³	0.547	1.207	-8.752 ⁻³	2.034 ⁻²	-2.426 ⁻³
0.040	0.658	-2.051 ⁻²	3.818 ⁻²	-6.228 ⁻³	0.627	1.222	3.142 ⁻²	2.018 ⁻²	-7.826 ⁻⁴
0.047	0.609	-1.425 ⁻²	3.855 ⁻²	-5.072 ⁻³	0.629	1.196	9.427 ⁻³	2.418 ⁻²	-3.318 ⁻³
0.053	0.692	-2.898 ⁻²	4.444 ⁻²	-8.534 ⁻³	0.649	1.196	-7.759 ⁻³	2.310 ⁻²	-1.884 ⁻³
0.060	0.683	-2.440 ⁻²	4.678 ⁻²	-1.111 ⁻²	0.653	1.233	3.842 ⁻²	1.701 ⁻²	9.045 ⁻⁴
0.067	0.542	-3.272 ⁻²	4.262 ⁻²	-6.978 ⁻³	0.695	1.213	-3.627 ⁻²	2.284 ⁻²	-1.452 ⁻³
0.073	0.695	-3.079 ⁻²	4.597 ⁻²	-9.917 ⁻³	0.707	1.242	2.273 ⁻²	1.746 ⁻²	2.695 ⁻³
0.080	0.626	-3.554 ⁻²	4.731 ⁻²	-8.040 ⁻³	0.709	1.214	6.598 ⁻³	2.052 ⁻²	-2.788 ⁻³
0.087	0.602	-3.785 ⁻²	4.782 ⁻²	-1.079 ⁻²	0.722	1.217	3.269 ⁻²	1.965 ⁻²	-1.590 ⁻³
0.097	0.608	-5.059 ⁻²	4.999 ⁻²	-1.371 ⁻²	0.735	1.225	2.826 ⁻²	2.118 ⁻²	-1.110 ⁻³
0.107	0.625	-4.749 ⁻²	5.243 ⁻²	-1.377 ⁻²	0.762	1.222	2.238 ⁻²	2.195 ⁻²	-1.545 ⁻⁴
0.117	0.687	-3.788 ⁻²	5.418 ⁻²	-1.559 ⁻²	0.775	1.243	-2.235 ⁻²	1.892 ⁻²	1.905 ⁻³
0.127	0.698	-5.141 ⁻²	5.140 ⁻²	-1.424 ⁻²	0.789	1.243	1.861 ⁻²	1.878 ⁻²	5.032 ⁻⁴
0.137	0.655	-6.187 ⁻²	5.307 ⁻²	-1.570 ⁻²	0.822	1.248	1.685 ⁻²	1.514 ⁻²	1.006 ⁻³
0.147	0.764	-4.663 ⁻²	5.646 ⁻²	-1.608 ⁻²	0.832	1.256	5.925 ⁻³	1.730 ⁻²	2.049 ⁻³
0.157	0.772	-5.227 ⁻²	5.433 ⁻²	-1.474 ⁻²	0.842	1.256	1.321 ⁻²	1.375 ⁻²	2.332 ⁻³
0.177	0.794	-4.621 ⁻²	5.579 ⁻²	-1.786 ⁻²	0.852	1.258	2.514 ⁻²	1.410 ⁻²	2.032 ⁻³
0.187	0.815	-4.878 ⁻²	5.553 ⁻²	-1.805 ⁻²	0.862	1.260	1.883 ⁻²	1.481 ⁻²	2.055 ⁻³
0.227	0.881	-6.418 ⁻²	5.136 ⁻²	-1.605 ⁻²	0.872	1.250	2.490 ⁻³	1.570 ⁻²	2.492 ⁻³
0.240	0.896	-5.720 ⁻²	5.227 ⁻²	-1.648 ⁻²	0.882	1.260	-1.353 ⁻³	1.353 ⁻²	3.577 ⁻³
0.253	0.889	-5.427 ⁻²	5.074 ⁻²	-1.835 ⁻²	0.892	1.255	-8.639 ⁻⁴	1.488 ⁻²	3.744 ⁻³
0.267	0.912	-4.893 ⁻²	5.046 ⁻²	-1.625 ⁻²	0.902	1.260	1.202 ⁻²	1.375 ⁻²	2.965 ⁻³
0.293	0.933	-6.604 ⁻²	4.862 ⁻²	-1.596 ⁻²	0.909	1.266	9.062 ⁻³	1.001 ⁻²	2.431 ⁻³
0.340	1.045	-3.943 ⁻²	4.044 ⁻²	-1.233 ⁻²	0.915	1.270	1.866 ⁻²	9.301 ⁻³	2.282 ⁻³
0.360	1.069	-3.572 ⁻²	3.625 ⁻²	-1.180 ⁻²	0.922	1.265	6.172 ⁻⁴	8.835 ⁻³	2.278 ⁻³
0.380	1.059	-6.265 ⁻²	3.602 ⁻²	-1.042 ⁻²	0.929	1.262	-1.371 ⁻³	8.362 ⁻³	2.197 ⁻³
0.400	1.098	-4.185 ⁻²	3.121 ⁻²	-1.013 ⁻²	0.935	1.259	-1.053 ⁻²	7.518 ⁻³	2.481 ⁻³
0.420	1.110	-3.435 ⁻²	2.810 ⁻²	-7.770 ⁻³	0.942	1.251	-1.917 ⁻²	8.296 ⁻³	2.506 ⁻³
0.440	1.121	1.306 ⁻²	3.106 ⁻²	-7.178 ⁻³	0.949	1.254	-8.574 ⁻³	6.902 ⁻³	2.299 ⁻³
0.460	1.142	-1.741 ⁻²	2.903 ⁻²	-6.126 ⁻³	0.955	1.234	-1.463 ⁻²	7.136 ⁻³	2.602 ⁻³
0.480	1.151	-9.138 ⁻³	2.489 ⁻²	-6.830 ⁻³	0.962	1.215	-1.293 ⁻²	9.263 ⁻³	3.381 ⁻³
0.500	1.180	2.773 ⁻³	2.258 ⁻²	-4.129 ⁻³					

Table 16. Concluded ($x/H = 2$)

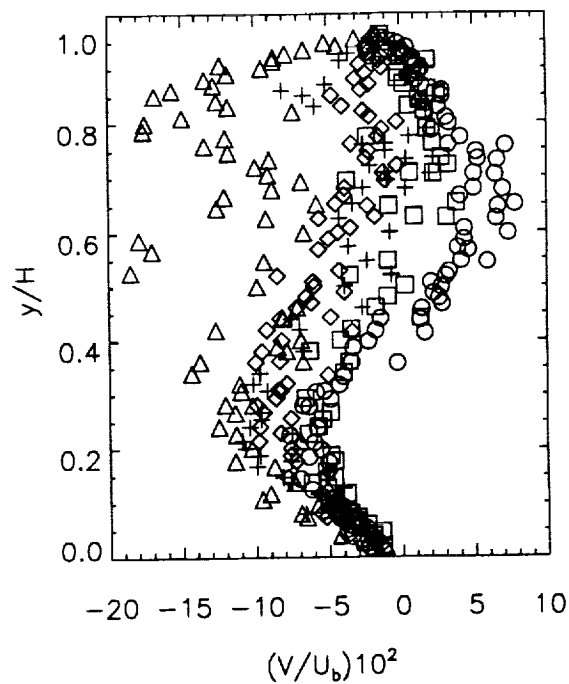
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.545	-2.474 ⁻²	3.892 ⁻²	-3.579 ⁻³	0.520	1.186	-6.618 ⁻³	2.193 ⁻²	-2.555 ⁻³
0.027	0.471	-1.672 ⁻²	3.512 ⁻²	-4.048 ⁻³	0.547	1.207	-2.299 ⁻²	2.135 ⁻²	9.041 ⁻⁵
0.033	0.486	-1.504 ⁻²	3.972 ⁻²	-4.698 ⁻³	0.573	1.208	-3.582 ⁻²	2.015 ⁻²	1.456 ⁻³
0.040	0.520	-2.942 ⁻²	4.016 ⁻²	-6.497 ⁻³	0.600	1.206	-7.276 ⁻³	2.327 ⁻²	1.554 ⁻³
0.047	0.548	-2.994 ⁻²	4.339 ⁻²	-7.026 ⁻³	0.627	1.216	-4.157 ⁻²	2.259 ⁻²	3.010 ⁻³
0.053	0.560	-2.324 ⁻²	4.611 ⁻²	-6.262 ⁻³	0.653	1.217	-3.289 ⁻²	2.483 ⁻²	2.089 ⁻³
0.060	0.568	-3.362 ⁻²	5.051 ⁻²	-1.029 ⁻²	0.680	1.231	3.679 ⁻³	1.913 ⁻²	3.067 ⁻³
0.067	0.598	-3.443 ⁻²	4.942 ⁻²	-1.093 ⁻²	0.682	1.201	-2.532 ⁻²	2.325 ⁻²	-1.851 ⁻³
0.073	0.653	-4.375 ⁻²	5.137 ⁻²	-1.091 ⁻²	0.695	1.209	-8.476 ⁻³	2.252 ⁻²	-1.831 ⁻³
0.080	0.635	-6.626 ⁻²	5.874 ⁻²	-1.391 ⁻²	0.707	1.237	2.031 ⁻²	1.797 ⁻²	3.866 ⁻³
0.087	0.569	-3.812 ⁻²	5.227 ⁻²	-1.434 ⁻²	0.709	1.200	-1.024 ⁻²	2.437 ⁻²	-9.685 ⁻⁵
0.097	0.652	-5.129 ⁻²	5.696 ⁻²	-1.484 ⁻²	0.722	1.220	-2.056 ⁻²	1.948 ⁻²	1.158 ⁻⁴
0.107	0.592	-4.724 ⁻²	5.942 ⁻²	-1.822 ⁻²	0.733	1.237	4.225 ⁻³	1.619 ⁻²	3.764 ⁻³
0.117	0.685	-5.780 ⁻²	6.024 ⁻²	-1.803 ⁻²	0.735	1.213	2.261 ⁻²	2.138 ⁻²	-1.756 ⁻⁴
0.127	0.599	-4.090 ⁻²	5.782 ⁻²	-1.892 ⁻²	0.749	1.222	-1.005 ⁻²	2.013 ⁻²	1.487 ⁻³
0.137	0.701	-7.590 ⁻²	5.976 ⁻²	-1.951 ⁻²	0.760	1.229	-2.504 ⁻²	1.829 ⁻²	4.413 ⁻³
0.147	0.669	-8.166 ⁻²	6.213 ⁻²	-2.054 ⁻²	0.762	1.223	-1.015 ⁻²	2.098 ⁻²	1.253 ⁻³
0.157	0.675	-5.016 ⁻²	5.988 ⁻²	-1.988 ⁻²	0.775	1.231	6.258 ⁻³	1.883 ⁻²	2.324 ⁻³
0.167	0.720	-9.954 ⁻²	6.016 ⁻²	-2.267 ⁻²	0.789	1.230	1.856 ⁻²	1.897 ⁻²	1.148 ⁻³
0.177	0.713	-7.600 ⁻²	6.166 ⁻²	-2.245 ⁻²	0.822	1.242	1.822 ⁻²	1.511 ⁻²	2.832 ⁻³
0.187	0.800	-9.713 ⁻²	5.955 ⁻²	-2.098 ⁻²	0.832	1.235	-5.804 ⁻²	1.726 ⁻²	3.608 ⁻³
0.200	0.821	-1.072 ⁻¹	6.111 ⁻²	-2.036 ⁻²	0.842	1.245	1.515 ⁻²	1.625 ⁻²	2.930 ⁻³
0.213	0.863	-1.090 ⁻¹	5.458 ⁻²	-1.939 ⁻²	0.852	1.237	-6.594 ⁻²	2.006 ⁻²	3.546 ⁻³
0.227	0.851	-7.525 ⁻²	5.888 ⁻²	-2.026 ⁻²	0.862	1.223	-8.067 ⁻²	1.923 ⁻²	2.898 ⁻³
0.240	0.872	-1.042 ⁻¹	5.835 ⁻²	-2.150 ⁻²	0.872	1.236	-5.067 ⁻²	1.851 ⁻²	3.162 ⁻³
0.253	0.888	-9.642 ⁻²	5.617 ⁻²	-1.870 ⁻²	0.882	1.249	5.486 ⁻³	1.415 ⁻²	3.160 ⁻³
0.267	0.909	-9.650 ⁻²	5.716 ⁻²	-2.135 ⁻²	0.892	1.247	5.686 ⁻³	1.392 ⁻²	2.634 ⁻³
0.307	0.997	-9.194 ⁻²	4.833 ⁻²	-1.473 ⁻²	0.902	1.245	1.813 ⁻²	1.432 ⁻²	2.562 ⁻³
0.320	1.007	-1.017 ⁻¹	4.811 ⁻²	-1.392 ⁻²	0.909	1.244	-1.752 ⁻²	1.328 ⁻²	3.388 ⁻³
0.340	1.035	-9.703 ⁻²	4.220 ⁻²	-1.249 ⁻²	0.915	1.238	-4.077 ⁻²	1.474 ⁻²	4.691 ⁻³
0.380	1.062	-6.682 ⁻²	3.935 ⁻²	-1.122 ⁻²	0.922	1.258	-1.849 ⁻³	1.077 ⁻²	2.606 ⁻³
0.420	1.119	-6.955 ⁻²	3.135 ⁻²	-7.406 ⁻³	0.929	1.243	-3.498 ⁻²	9.901 ⁻³	2.912 ⁻³
0.440	1.134	-7.508 ⁻²	3.159 ⁻²	-6.941 ⁻³	0.935	1.244	-1.695 ⁻²	8.619 ⁻³	2.454 ⁻³
0.460	1.141	-2.656 ⁻²	2.812 ⁻²	-5.733 ⁻³	0.942	1.252	-3.032 ⁻³	9.045 ⁻³	3.255 ⁻³
0.500	1.166	-3.854 ⁻²	2.615 ⁻²	-4.698 ⁻³	0.949	1.245	-2.692 ⁻³	8.769 ⁻³	3.632 ⁻³

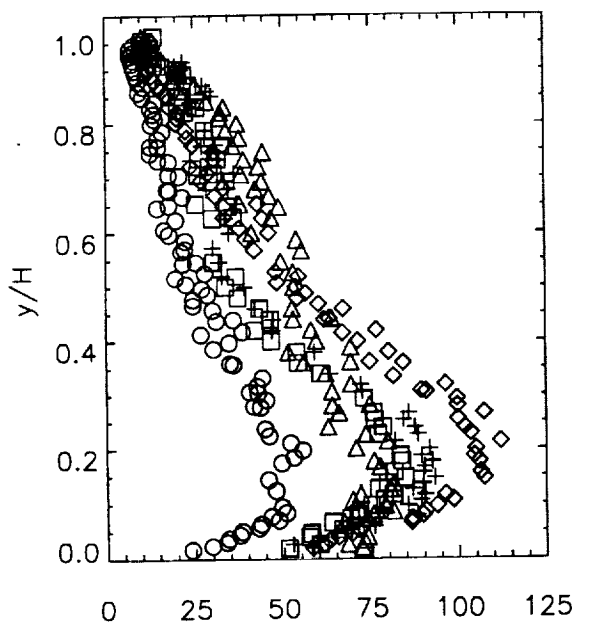
Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)



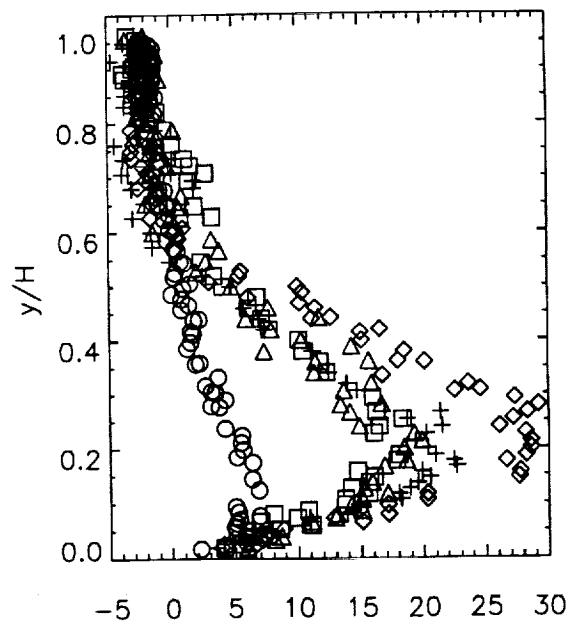
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

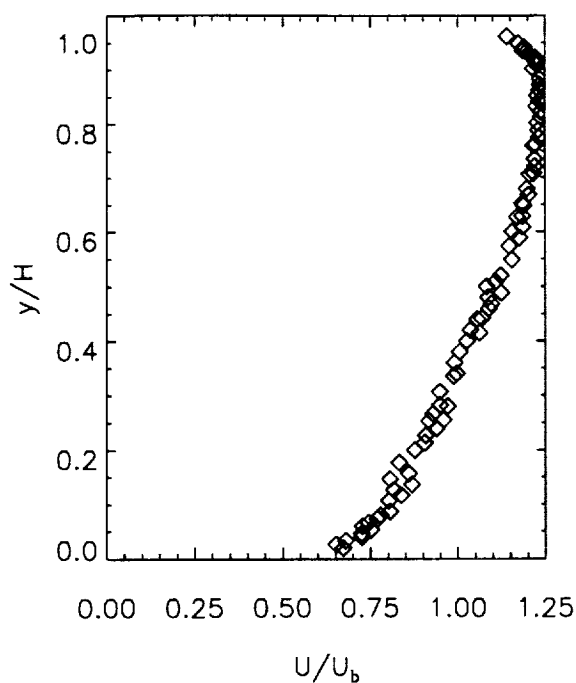
Figure 16. Summary of Table 16 ($x/H = 2$).

Table 17. LDV flowfield data in TAD ($x/H = 3$)

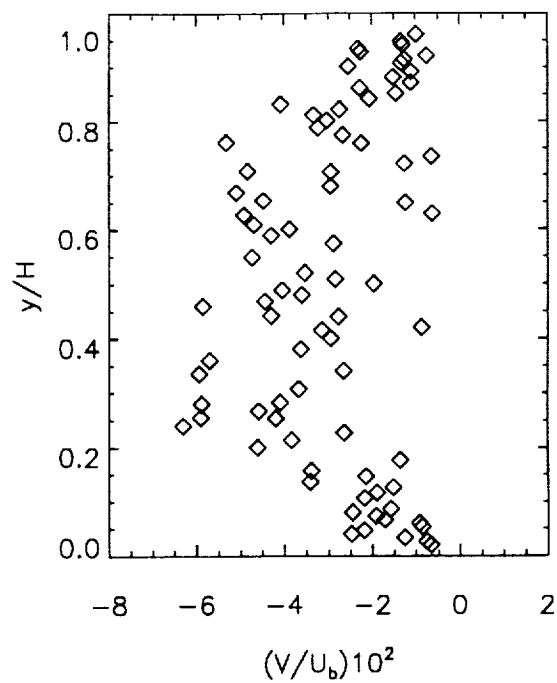
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.672	-6.629 ⁻³	2.650 ⁻²	-2.905 ⁻³	0.500	1.082	-1.966 ⁻²	3.385 ⁻²	-1.130 ⁻²
0.026	0.652	-7.641 ⁻³	2.585 ⁻²	-2.013 ⁻³	0.508	1.108	-2.839 ⁻²	3.530 ⁻²	-1.136 ⁻²
0.033	0.679	-1.262 ⁻²	2.909 ⁻²	-3.416 ⁻³	0.520	1.123	-3.532 ⁻²	3.164 ⁻²	-8.202 ⁻³
0.040	0.725	-2.478 ⁻²	3.208 ⁻²	-5.479 ⁻³	0.548	1.155	-4.728 ⁻²	3.110 ⁻²	-7.441 ⁻³
0.046	0.724	-2.189 ⁻²	2.747 ⁻²	-4.261 ⁻³	0.573	1.147	-2.880 ⁻²	2.758 ⁻²	-6.294 ⁻³
0.053	0.752	-8.624 ⁻³	3.032 ⁻²	-4.111 ⁻³	0.588	1.176	-4.292 ⁻²	2.657 ⁻²	-4.007 ⁻³
0.060	0.727	-9.268 ⁻³	3.067 ⁻²	-4.723 ⁻³	0.600	1.156	-3.882 ⁻²	2.653 ⁻²	-4.349 ⁻³
0.066	0.744	-1.718 ⁻²	3.169 ⁻²	-5.783 ⁻³	0.608	1.185	-4.684 ⁻²	2.669 ⁻²	-4.328 ⁻³
0.073	0.770	-1.916 ⁻²	3.276 ⁻²	-6.317 ⁻³	0.626	1.169	-4.911 ⁻²	2.569 ⁻²	-3.266 ⁻³
0.080	0.779	-2.450 ⁻²	3.289 ⁻²	-7.454 ⁻³	0.628	1.185	-6.305 ⁻³	2.487 ⁻²	-3.213 ⁻³
0.086	0.805	-1.580 ⁻²	3.336 ⁻²	-5.940 ⁻³	0.648	1.188	-1.238 ⁻²	2.444 ⁻²	-3.445 ⁻³
0.106	0.802	-2.183 ⁻²	3.640 ⁻²	-9.896 ⁻³	0.653	1.185	-4.469 ⁻²	2.406 ⁻²	-2.161 ⁻³
0.116	0.838	-1.899 ⁻²	3.576 ⁻²	-1.196 ⁻²	0.668	1.202	-5.083 ⁻²	2.327 ⁻²	-2.542 ⁻³
0.126	0.817	-1.526 ⁻²	3.637 ⁻²	-9.554 ⁻³	0.680	1.197	-2.944 ⁻²	2.091 ⁻²	-1.606 ⁻³
0.136	0.868	-3.419 ⁻²	3.966 ⁻²	-1.352 ⁻²	0.706	1.205	-2.938 ⁻²	1.860 ⁻²	6.060 ⁻⁵
0.146	0.805	-2.148 ⁻²	3.771 ⁻²	-1.286 ⁻²	0.708	1.217	-4.829 ⁻²	2.028 ⁻²	-4.514 ⁻⁴
0.156	0.859	-3.395 ⁻²	4.015 ⁻²	-1.272 ⁻²	0.722	1.220	-1.262 ⁻²	1.908 ⁻²	-7.973 ⁻⁴
0.176	0.832	-1.368 ⁻²	3.755 ⁻²	-1.235 ⁻²	0.735	1.220	-6.473 ⁻³	1.870 ⁻²	-1.226 ⁻⁴
0.200	0.877	-4.613 ⁻²	3.951 ⁻²	-1.397 ⁻²	0.760	1.216	-2.243 ⁻²	1.941 ⁻²	-3.569 ⁻⁴
0.213	0.905	-3.844 ⁻²	4.042 ⁻²	-1.448 ⁻²	0.762	1.222	-5.314 ⁻²	1.659 ⁻²	1.332 ⁻³
0.226	0.908	-2.646 ⁻²	4.019 ⁻²	-1.613 ⁻²	0.775	1.233	-2.669 ⁻²	1.479 ⁻²	1.106 ⁻³
0.240	0.939	-6.309 ⁻²	4.120 ⁻²	-1.669 ⁻²	0.788	1.230	-3.229 ⁻²	1.548 ⁻²	8.441 ⁻⁴
0.253	0.917	-4.199 ⁻²	4.085 ⁻²	-1.446 ⁻²	0.802	1.228	-3.029 ⁻²	1.556 ⁻²	1.114 ⁻⁴
0.255	0.959	-5.907 ⁻²	4.280 ⁻²	-1.761 ⁻²	0.812	1.237	-3.332 ⁻²	1.245 ⁻²	8.681 ⁻⁴
0.266	0.929	-4.590 ⁻²	4.074 ⁻²	-1.407 ⁻²	0.822	1.237	-2.741 ⁻²	1.172 ⁻²	1.104 ⁻³
0.280	0.971	-5.886 ⁻²	4.071 ⁻²	-1.689 ⁻²	0.832	1.225	-4.076 ⁻²	1.264 ⁻²	1.774 ⁻³
0.282	0.949	-4.103 ⁻²	4.159 ⁻²	-1.479 ⁻²	0.842	1.233	-2.062 ⁻²	1.148 ⁻²	1.133 ⁻³
0.306	0.948	-3.681 ⁻²	4.239 ⁻²	-1.563 ⁻²	0.852	1.227	-1.455 ⁻²	1.302 ⁻²	5.236 ⁻⁴
0.335	0.988	-5.939 ⁻²	4.276 ⁻²	-1.723 ⁻²	0.862	1.234	-2.278 ⁻²	1.049 ⁻²	1.837 ⁻³
0.340	0.997	-2.659 ⁻²	3.957 ⁻²	-1.366 ⁻²	0.872	1.235	-1.112 ⁻²	1.228 ⁻²	1.901 ⁻³
0.360	0.990	-5.702 ⁻²	3.811 ⁻²	-1.555 ⁻²	0.882	1.235	-1.519 ⁻²	1.005 ⁻²	2.828 ⁻³
0.380	1.005	-3.628 ⁻²	4.138 ⁻²	-1.473 ⁻²	0.892	1.241	-1.106 ⁻²	8.361 ⁻³	1.495 ⁻³
0.400	1.026	-2.945 ⁻²	3.772 ⁻²	-1.287 ⁻²	0.902	1.215	-2.541 ⁻²	1.189 ⁻²	2.502 ⁻³
0.415	1.062	-3.152 ⁻²	3.878 ⁻²	-1.285 ⁻²	0.908	1.226	-1.335 ⁻²	1.028 ⁻²	2.253 ⁻³
0.420	1.035	-8.783 ⁻³	3.767 ⁻²	-1.306 ⁻²	0.915	1.222	-1.264 ⁻²	8.838 ⁻³	1.793 ⁻³
0.440	1.056	-2.772 ⁻²	3.506 ⁻²	-1.241 ⁻²	0.922	1.221	-7.540 ⁻³	8.214 ⁻³	1.967 ⁻³
0.442	1.068	-4.303 ⁻²	3.898 ⁻²	-1.303 ⁻²	0.928	1.203	-2.267 ⁻²	1.103 ⁻²	2.369 ⁻³
0.460	1.089	-5.850 ⁻²	3.453 ⁻²	-1.050 ⁻²	0.935	1.185	-2.317 ⁻²	1.085 ⁻²	2.800 ⁻³
0.468	1.095	-4.439 ⁻²	3.876 ⁻²	-1.181 ⁻²	0.942	1.190	-1.309 ⁻²	1.153 ⁻²	2.455 ⁻³
0.480	1.087	-3.602 ⁻²	3.548 ⁻²	-1.273 ⁻²	0.948	1.174	-1.336 ⁻²	1.144 ⁻²	2.610 ⁻³
0.488	1.124	-4.045 ⁻²	3.476 ⁻²	-1.057 ⁻²	0.962	1.140	-9.906 ⁻³	1.173 ⁻²	2.693 ⁻³

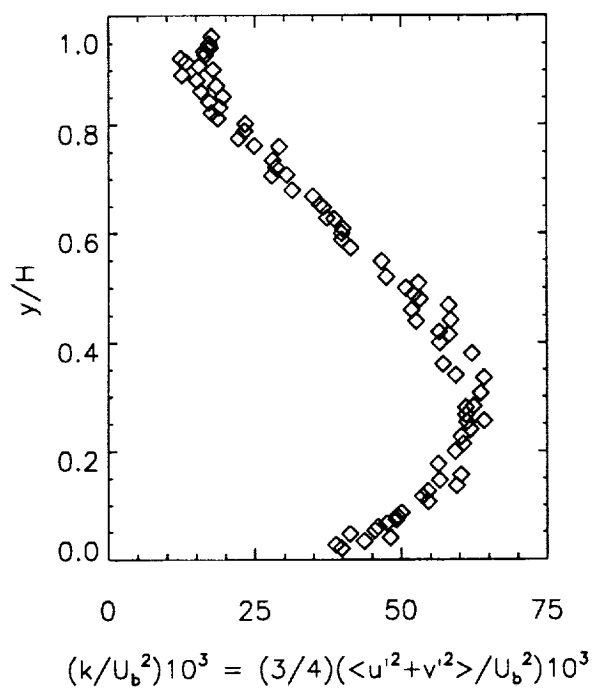
Legend: $Re = 1 \times 10^5$; $z/H = 0(\diamond)$



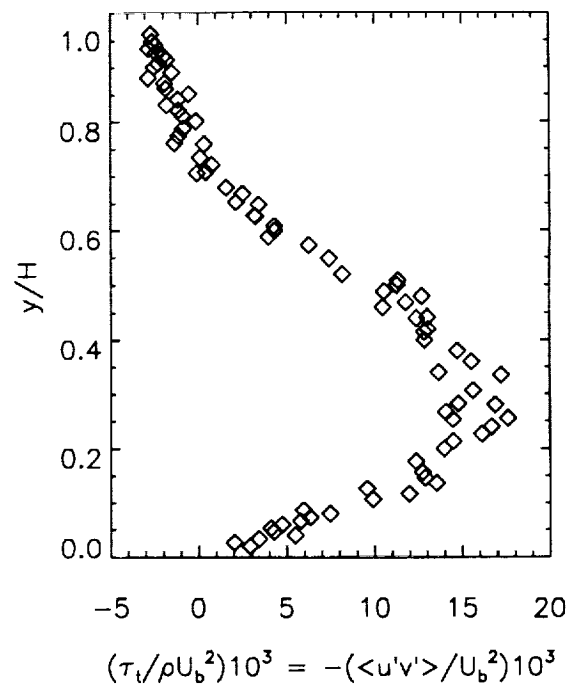
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 17. Summary of Table 17 ($x/H = 3$).

Table 18. LDV flowfield data in TAD ($x/H = 4$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.032	0.767	-1.221 ⁻²	1.029 ⁻²	-1.278 ⁻³	0.628	1.100	5.538 ⁻³	1.650 ⁻²	-3.033 ⁻³
0.038	0.781	-1.114 ⁻²	1.081 ⁻²	-1.111 ⁻³	0.648	1.113	-2.246 ⁻²	1.565 ⁻²	-2.481 ⁻³
0.045	0.784	-1.289 ⁻²	1.216 ⁻²	-1.682 ⁻³	0.682	1.123	4.414 ⁻³	1.258 ⁻²	-1.977 ⁻³
0.052	0.792	-1.581 ⁻²	1.371 ⁻²	-1.839 ⁻³	0.695	1.124	-7.747 ⁻³	1.310 ⁻²	-1.715 ⁻³
0.058	0.789	-1.426 ⁻²	1.317 ⁻²	-1.905 ⁻³	0.708	1.131	-1.857 ⁻²	1.251 ⁻²	-1.091 ⁻³
0.065	0.813	-1.665 ⁻²	1.445 ⁻²	-2.237 ⁻³	0.722	1.126	4.299 ⁻³	1.258 ⁻²	-1.576 ⁻³
0.072	0.812	-1.916 ⁻²	1.463 ⁻²	-2.149 ⁻³	0.735	1.132	-1.783 ⁻⁴	1.089 ⁻²	-1.337 ⁻³
0.078	0.808	-2.031 ⁻²	1.515 ⁻²	-2.563 ⁻³	0.748	1.145	2.873 ⁻³	9.086 ⁻³	-7.117 ⁻⁴
0.085	0.806	-1.775 ⁻²	1.472 ⁻²	-2.181 ⁻³	0.762	1.137	3.016 ⁻³	9.810 ⁻³	-7.974 ⁻⁴
0.092	0.808	-2.540 ⁻²	1.503 ⁻²	-2.406 ⁻³	0.775	1.137	3.045 ⁻²	9.477 ⁻³	-9.418 ⁻⁴
0.098	0.814	-1.973 ⁻²	1.512 ⁻²	-2.691 ⁻³	0.788	1.151	1.064 ⁻²	8.126 ⁻³	-1.996 ⁻⁴
0.108	0.815	-1.398 ⁻²	1.460 ⁻²	-1.837 ⁻³	0.802	1.157	1.534 ⁻²	7.577 ⁻³	-2.857 ⁻⁴
0.118	0.834	-1.164 ⁻²	1.655 ⁻²	-1.244 ⁻³	0.812	1.163	7.659 ⁻³	6.648 ⁻³	-4.304 ⁻⁴
0.128	0.849	-7.267 ⁻³	1.767 ⁻²	-1.894 ⁻³	0.822	1.166	1.865 ⁻³	6.651 ⁻³	-1.957 ⁻⁴
0.148	0.857	-2.586 ⁻²	1.817 ⁻²	-3.317 ⁻³	0.832	1.167	6.652 ⁻³	6.718 ⁻³	4.908 ⁻⁵
0.158	0.867	-1.082 ⁻²	1.735 ⁻²	-2.225 ⁻³	0.842	1.167	1.111 ⁻²	6.721 ⁻³	7.748 ⁻⁵
0.188	0.895	1.248 ⁻³	1.877 ⁻²	-1.309 ⁻³	0.852	1.173	3.831 ⁻³	5.889 ⁻³	1.346 ⁻⁴
0.198	0.893	2.634 ⁻³	2.049 ⁻²	-2.195 ⁻³	0.862	1.168	-3.519 ⁻³	6.065 ⁻³	4.030 ⁻⁴
0.238	0.928	1.990 ⁻²	2.033 ⁻²	-2.713 ⁻³	0.872	1.166	-9.243 ⁻³	5.823 ⁻³	7.562 ⁻⁴
0.265	0.970	2.657 ⁻²	2.156 ⁻²	-3.315 ⁻³	0.882	1.178	1.050 ⁻²	5.420 ⁻³	-8.966 ⁻⁵
0.362	1.032	1.094 ⁻²	2.305 ⁻²	-6.085 ⁻³	0.892	1.171	1.661 ⁻³	5.655 ⁻³	6.536 ⁻⁴
0.388	1.010	2.735 ⁻²	2.371 ⁻²	-5.035 ⁻³	0.902	1.180	5.333 ⁻³	5.042 ⁻³	4.262 ⁻⁴
0.415	1.048	2.595 ⁻²	2.400 ⁻²	-5.816 ⁻³	0.908	1.179	3.520 ⁻³	4.733 ⁻³	4.660 ⁻⁴
0.442	1.045	5.153 ⁻³	2.295 ⁻²	-6.306 ⁻³	0.915	1.185	4.719 ⁻³	4.370 ⁻³	1.939 ⁻⁴
0.468	1.060	-2.317 ⁻²	2.139 ⁻²	-5.345 ⁻³	0.922	1.177	2.775 ⁻³	4.476 ⁻³	4.387 ⁻⁴
0.488	1.082	-3.446 ⁻²	1.937 ⁻²	-4.121 ⁻³	0.928	1.174	1.832 ⁻³	4.506 ⁻³	5.670 ⁻⁴
0.548	1.091	-3.652 ⁻²	1.898 ⁻²	-3.573 ⁻³	0.935	1.170	5.756 ⁻⁴	4.587 ⁻³	9.119 ⁻⁴
0.568	1.091	8.086 ⁻⁴	1.924 ⁻²	-4.852 ⁻³	0.942	1.152	1.486 ⁻⁴	5.056 ⁻³	1.100 ⁻³
0.588	1.078	1.298 ⁻²	1.689 ⁻²	-3.383 ⁻³	0.948	1.133	-1.696 ⁻³	6.361 ⁻³	1.597 ⁻³
0.608	1.095	1.900 ⁻²	1.454 ⁻²	-2.613 ⁻³					

Table 18. Continued ($x/H = 4$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.750	-1.685 ⁻³	2.018 ⁻²	-2.324 ⁻³	0.546	1.084	-1.444 ⁻²	2.561 ⁻²	-8.193 ⁻³
0.026	0.744	-4.098 ⁻³	2.014 ⁻²	-2.282 ⁻³	0.551	1.078	-1.342 ⁻²	2.530 ⁻²	-8.333 ⁻³
0.033	0.760	4.861 ⁻⁴	1.955 ⁻²	-2.011 ⁻³	0.572	1.085	-1.820 ⁻²	2.563 ⁻²	-8.706 ⁻³
0.040	0.795	-8.397 ⁻³	2.113 ⁻²	-3.057 ⁻³	0.591	1.100	-2.109 ⁻²	2.300 ⁻²	-7.312 ⁻³
0.046	0.818	-5.321 ⁻³	2.168 ⁻²	-4.257 ⁻³	0.600	1.097	-2.505 ⁻²	2.421 ⁻²	-7.997 ⁻³
0.053	0.822	-3.761 ⁻³	2.221 ⁻²	-4.603 ⁻³	0.626	1.103	-8.117 ⁻³	2.454 ⁻²	-7.623 ⁻³
0.060	0.827	-2.498 ⁻³	2.222 ⁻²	-4.228 ⁻³	0.631	1.127	-2.473 ⁻²	2.256 ⁻²	-6.727 ⁻³
0.066	0.872	-4.143 ⁻³	2.421 ⁻²	-4.827 ⁻³	0.652	1.126	-7.716 ⁻³	2.149 ⁻²	-5.935 ⁻³
0.073	0.891	-1.888 ⁻²	2.498 ⁻²	-5.654 ⁻³	0.671	1.155	-2.882 ⁻²	1.802 ⁻²	-5.051 ⁻³
0.080	0.872	-2.039 ⁻⁴	2.301 ⁻²	-3.875 ⁻³	0.680	1.125	-1.483 ⁻³	2.252 ⁻²	-5.829 ⁻³
0.086	0.861	3.087 ⁻³	2.379 ⁻²	-4.525 ⁻³	0.684	1.155	-2.238 ⁻²	1.790 ⁻²	-4.515 ⁻³
0.096	0.904	-9.480 ⁻³	2.635 ⁻²	-6.324 ⁻³	0.698	1.153	-2.286 ⁻²	1.777 ⁻²	-3.958 ⁻³
0.116	0.906	-1.084 ⁻²	2.747 ⁻²	-8.008 ⁻³	0.706	1.139	-1.967 ⁻²	2.028 ⁻²	-4.341 ⁻³
0.126	0.891	3.364 ⁻³	2.539 ⁻²	-7.633 ⁻³	0.711	1.156	-1.938 ⁻²	1.776 ⁻²	-3.489 ⁻³
0.136	0.900	-6.304 ⁻³	2.634 ⁻²	-6.273 ⁻³	0.724	1.164	-1.984 ⁻²	1.676 ⁻²	-2.580 ⁻³
0.146	0.912	-2.084 ⁻²	2.554 ⁻²	-7.046 ⁻³	0.738	1.162	-7.034 ⁻⁴	1.592 ⁻²	-2.867 ⁻³
0.156	0.912	-9.863 ⁻³	2.685 ⁻²	-7.826 ⁻³	0.751	1.175	-5.094 ⁻³	1.486 ⁻²	-2.615 ⁻³
0.166	0.932	1.350 ⁻³	2.704 ⁻²	-6.236 ⁻³	0.760	1.159	-2.054 ⁻²	1.716 ⁻²	-2.589 ⁻³
0.176	0.909	-1.217 ⁻²	2.700 ⁻²	-8.551 ⁻³	0.764	1.181	-2.038 ⁻²	1.492 ⁻²	-2.021 ⁻³
0.186	0.915	5.988 ⁻³	2.709 ⁻²	-7.228 ⁻³	0.778	1.197	-1.259 ⁻²	1.263 ⁻²	-1.195 ⁻³
0.200	0.929	-1.730 ⁻²	2.737 ⁻²	-9.636 ⁻³	0.791	1.199	-2.366 ⁻²	1.201 ⁻²	-9.056 ⁻⁴
0.213	0.950	-2.616 ⁻²	2.904 ⁻²	-1.076 ⁻²	0.804	1.194	-9.639 ⁻³	1.355 ⁻²	-1.360 ⁻³
0.226	0.948	-2.583 ⁻²	3.085 ⁻²	-1.125 ⁻²	0.814	1.200	-2.182 ⁻²	1.173 ⁻²	-1.827 ⁻⁴
0.240	0.919	-4.155 ⁻⁴	2.777 ⁻²	-9.252 ⁻³	0.824	1.203	-2.612 ⁻²	1.142 ⁻²	8.573 ⁻⁵
0.253	0.954	4.074 ⁻³	3.046 ⁻²	-9.174 ⁻³	0.834	1.207	-1.266 ⁻²	1.021 ⁻²	4.881 ⁻⁵
0.293	0.982	-3.242 ⁻²	3.073 ⁻²	-1.090 ⁻²	0.844	1.205	-1.530 ⁻²	1.072 ⁻²	5.026 ⁻⁴
0.306	0.963	-2.205 ⁻³	2.993 ⁻²	-1.178 ⁻²	0.854	1.215	-1.310 ⁻²	9.366 ⁻³	4.247 ⁻⁴
0.320	0.975	-1.127 ⁻²	2.761 ⁻²	-1.006 ⁻²	0.864	1.204	-1.905 ⁻²	1.150 ⁻²	7.677 ⁻⁴
0.364	0.976	-2.053 ⁻²	3.043 ⁻²	-1.212 ⁻²	0.874	1.203	-2.492 ⁻²	1.067 ⁻²	1.291 ⁻³
0.380	1.002	-2.728 ⁻²	2.990 ⁻²	-1.216 ⁻²	0.884	1.209	-1.795 ⁻²	9.220 ⁻³	1.038 ⁻³
0.400	0.998	-1.659 ⁻³	2.766 ⁻²	-9.910 ⁻³	0.894	1.202	-1.915 ⁻²	1.132 ⁻²	1.714 ⁻³
0.419	1.004	3.472 ⁻³	2.869 ⁻²	-9.971 ⁻³	0.904	1.193	-2.366 ⁻²	1.234 ⁻²	1.722 ⁻³
0.440	1.037	-2.622 ⁻²	2.832 ⁻²	-1.104 ⁻²	0.911	1.193	-2.491 ⁻²	1.059 ⁻²	2.208 ⁻³
0.444	1.023	-1.326 ⁻²	2.832 ⁻²	-1.009 ⁻²	0.918	1.202	-1.692 ⁻²	1.013 ⁻²	1.664 ⁻³
0.471	1.034	-1.663 ⁻²	2.840 ⁻²	-1.079 ⁻²	0.924	1.192	-1.736 ⁻²	1.034 ⁻²	1.439 ⁻³
0.480	1.046	-3.029 ⁻²	2.814 ⁻²	-9.554 ⁻³	0.931	1.184	-1.844 ⁻²	9.583 ⁻³	1.326 ⁻³
0.491	1.057	-1.873 ⁻²	2.638 ⁻²	-9.903 ⁻³	0.938	1.185	-1.513 ⁻²	1.166 ⁻²	1.674 ⁻³
0.500	1.057	-9.371 ⁻⁴	2.580 ⁻²	-8.672 ⁻³	0.944	1.173	-1.972 ⁻²	1.170 ⁻²	2.398 ⁻³
0.511	1.068	-1.700 ⁻²	2.805 ⁻²	-1.057 ⁻²	0.951	1.180	-1.336 ⁻²	1.008 ⁻²	1.555 ⁻³
0.531	1.076	-1.841 ⁻²	2.635 ⁻²	-9.620 ⁻³	0.958	1.151	-1.509 ⁻²	1.102 ⁻²	1.591 ⁻³

Table 18. Continued ($x/H = 4$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.762	3.700^{-3}	1.753^{-2}	-2.194^{-3}	0.600	1.153	-8.508^{-2}	2.114^{-2}	-3.573^{-3}
0.026	0.765	7.818^{-3}	1.787^{-2}	-1.878^{-3}	0.611	1.154	-4.684^{-2}	2.219^{-2}	-7.808^{-3}
0.053	0.996	-1.995^{-2}	2.098^{-2}	-2.604^{-3}	0.631	1.153	-4.780^{-2}	2.154^{-2}	-6.498^{-3}
0.060	1.025	-3.845^{-2}	2.183^{-2}	-4.567^{-3}	0.652	1.175	-7.352^{-2}	1.819^{-2}	-3.415^{-3}
0.073	1.055	-4.892^{-2}	2.023^{-2}	-4.169^{-3}	0.680	1.163	-8.758^{-2}	1.772^{-2}	-2.099^{-3}
0.080	1.047	-5.410^{-2}	2.084^{-2}	-4.334^{-3}	0.706	1.176	-7.419^{-2}	1.679^{-2}	-2.105^{-3}
0.086	1.052	-5.668^{-2}	2.127^{-2}	-4.999^{-3}	0.711	1.195	-5.809^{-2}	1.506^{-2}	-1.756^{-3}
0.096	1.053	-5.251^{-2}	2.237^{-2}	-5.187^{-3}	0.724	1.190	-3.809^{-2}	1.511^{-2}	-2.858^{-3}
0.106	1.036	-6.329^{-2}	2.225^{-2}	-6.675^{-3}	0.733	1.175	-4.800^{-2}	1.579^{-2}	-8.905^{-4}
0.116	1.004	-3.429^{-2}	2.601^{-2}	-7.496^{-3}	0.738	1.192	-4.625^{-2}	1.439^{-2}	-2.005^{-3}
0.126	1.032	-4.319^{-2}	2.405^{-2}	-4.867^{-3}	0.764	1.199	-5.571^{-2}	1.346^{-2}	-1.159^{-3}
0.136	1.055	-6.434^{-2}	2.323^{-2}	-6.641^{-3}	0.778	1.200	-6.346^{-2}	1.169^{-2}	-2.922^{-4}
0.146	1.007	-4.496^{-2}	2.645^{-2}	-8.774^{-3}	0.791	1.201	-4.867^{-2}	1.117^{-2}	-1.613^{-4}
0.156	1.040	-5.481^{-2}	2.656^{-2}	-8.061^{-3}	0.804	1.206	-3.655^{-2}	1.151^{-2}	-4.226^{-4}
0.166	1.024	-4.800^{-2}	2.615^{-2}	-6.486^{-3}	0.814	1.208	-3.291^{-2}	1.089^{-2}	2.587^{-4}
0.176	1.061	-8.346^{-2}	2.381^{-2}	-6.589^{-3}	0.824	1.207	-4.220^{-2}	9.182^{-3}	8.443^{-4}
0.186	1.054	-7.982^{-2}	2.494^{-2}	-8.730^{-3}	0.834	1.208	-3.550^{-2}	9.753^{-3}	6.169^{-4}
0.200	1.030	-4.916^{-2}	2.682^{-2}	-8.734^{-3}	0.844	1.208	-3.564^{-2}	9.235^{-3}	1.152^{-3}
0.226	1.048	-5.781^{-2}	2.762^{-2}	-8.637^{-3}	0.854	1.209	-2.292^{-2}	8.882^{-3}	9.578^{-4}
0.240	1.033	-6.517^{-2}	2.753^{-2}	-9.824^{-3}	0.864	1.198	-2.756^{-2}	8.786^{-3}	6.214^{-4}
0.280	1.042	-3.537^{-2}	3.114^{-2}	-9.867^{-3}	0.874	1.191	-2.990^{-2}	8.953^{-3}	7.374^{-4}
0.320	1.037	-4.514^{-2}	2.882^{-2}	-1.148^{-2}	0.884	1.196	-2.481^{-2}	8.688^{-3}	8.013^{-4}
0.338	1.053	-5.123^{-2}	3.089^{-2}	-1.200^{-2}	0.894	1.192	-2.293^{-2}	9.500^{-3}	5.069^{-4}
0.400	1.080	-8.461^{-2}	2.907^{-2}	-1.071^{-2}	0.904	1.174	-2.769^{-2}	8.216^{-3}	1.342^{-3}
0.418	1.096	-5.442^{-2}	2.882^{-2}	-1.070^{-2}	0.911	1.180	-2.151^{-2}	8.566^{-3}	8.852^{-4}
0.444	1.102	-5.757^{-2}	3.067^{-2}	-1.130^{-2}	0.918	1.154	-2.550^{-2}	9.026^{-3}	1.233^{-3}
0.471	1.109	-5.348^{-2}	2.836^{-2}	-1.092^{-2}	0.924	1.165	-2.378^{-2}	8.225^{-3}	7.841^{-4}
0.480	1.104	-5.744^{-2}	2.759^{-2}	-9.285^{-3}	0.931	1.160	-2.144^{-2}	8.745^{-3}	1.018^{-3}
0.491	1.111	-5.411^{-2}	2.834^{-2}	-1.054^{-2}	0.938	1.144	-1.801^{-2}	9.380^{-3}	8.140^{-4}
0.500	1.095	-4.056^{-2}	2.757^{-2}	-8.257^{-3}	0.944	1.143	-1.381^{-2}	8.963^{-3}	7.958^{-4}
0.520	1.102	-5.389^{-2}	2.709^{-2}	-7.933^{-3}	0.951	1.140	-1.190^{-2}	8.976^{-3}	1.020^{-3}
0.531	1.131	-7.055^{-2}	2.572^{-2}	-8.162^{-3}	0.958	1.121	-6.335^{-3}	9.156^{-3}	8.723^{-4}
0.551	1.119	-3.495^{-2}	2.614^{-2}	-9.869^{-3}	0.964	1.113	-2.941^{-3}	8.700^{-3}	7.624^{-4}
0.572	1.146	-7.733^{-2}	2.217^{-2}	-5.933^{-3}	0.971	1.073	1.229^{-4}	9.942^{-3}	1.044^{-3}
0.591	1.144	-5.034^{-2}	2.313^{-2}	-7.108^{-3}					

Table 18. Continued ($x/H = 4$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.020	0.759	-9.633 ⁻³	1.859 ⁻²	-2.637 ⁻³	0.600	1.093	-5.568 ⁻³	2.381 ⁻²	-5.091 ⁻³
0.026	0.777	4.587 ⁻⁴	1.818 ⁻²	-2.474 ⁻³	0.626	1.094	5.957 ⁻³	2.134 ⁻²	-4.926 ⁻³
0.060	0.841	1.251 ⁻²	1.891 ⁻²	-3.661 ⁻³	0.631	1.083	3.006 ⁻³	2.023 ⁻²	-6.249 ⁻³
0.086	0.871	1.801 ⁻³	2.096 ⁻²	-4.130 ⁻³	0.652	1.093	1.861 ⁻²	2.079 ⁻²	-5.693 ⁻³
0.096	0.834	-9.803 ⁻⁴	2.067 ⁻²	-4.033 ⁻³	0.680	1.113	-3.055 ⁻³	2.011 ⁻²	-5.335 ⁻³
0.116	0.901	1.791 ⁻²	2.155 ⁻²	-4.692 ⁻³	0.684	1.118	8.428 ⁻³	1.832 ⁻²	-5.058 ⁻³
0.136	0.895	3.189 ⁻³	2.250 ⁻²	-6.245 ⁻³	0.698	1.115	-2.475 ⁻⁴	1.875 ⁻²	-4.884 ⁻³
0.146	0.874	2.558 ⁻²	2.171 ⁻²	-4.626 ⁻³	0.706	1.123	2.841 ⁻³	1.823 ⁻²	-3.788 ⁻³
0.156	0.928	8.249 ⁻³	2.463 ⁻²	-5.338 ⁻³	0.711	1.124	-7.126 ⁻³	1.673 ⁻²	-2.577 ⁻³
0.176	0.904	5.630 ⁻³	2.351 ⁻²	-7.491 ⁻³	0.724	1.137	-6.364 ⁻⁵	1.607 ⁻²	-3.457 ⁻³
0.186	0.881	3.246 ⁻³	2.350 ⁻²	-7.059 ⁻³	0.751	1.149	-1.213 ⁻²	1.427 ⁻²	-2.932 ⁻³
0.200	0.879	1.556 ⁻³	2.388 ⁻²	-7.395 ⁻³	0.760	1.147	1.614 ⁻³	1.676 ⁻²	-3.130 ⁻³
0.213	0.906	9.144 ⁻⁵	2.668 ⁻²	-9.016 ⁻³	0.764	1.169	9.810 ⁻³	1.254 ⁻²	-2.118 ⁻³
0.226	0.934	1.858 ⁻²	2.700 ⁻²	-7.149 ⁻³	0.778	1.168	-1.198 ⁻²	1.137 ⁻²	-1.427 ⁻³
0.240	0.948	7.620 ⁻³	2.852 ⁻²	-9.696 ⁻³	0.791	1.178	-1.268 ⁻²	1.055 ⁻²	-8.990 ⁻⁴
0.253	0.950	-8.136 ⁻⁴	2.705 ⁻²	-9.040 ⁻³	0.804	1.178	5.147 ⁻³	1.094 ⁻²	-1.434 ⁻³
0.258	0.958	2.727 ⁻²	2.891 ⁻²	-9.201 ⁻³	0.814	1.183	-7.816 ⁻³	1.030 ⁻²	-3.993 ⁻⁴
0.266	0.959	1.656 ⁻³	2.556 ⁻²	-6.672 ⁻³	0.824	1.180	-1.192 ⁻²	1.020 ⁻²	-3.747 ⁻⁴
0.280	0.962	1.850 ⁻²	2.640 ⁻²	-7.988 ⁻³	0.834	1.184	-4.603 ⁻³	9.315 ⁻³	-4.150 ⁻⁴
0.293	0.956	1.009 ⁻³	2.532 ⁻²	-8.925 ⁻³	0.844	1.185	-1.263 ⁻²	1.052 ⁻²	-2.707 ⁻⁴
0.311	0.952	2.896 ⁻²	2.891 ⁻²	-9.100 ⁻³	0.854	1.185	2.305 ⁻³	9.314 ⁻³	-9.141 ⁻⁴
0.320	0.986	-8.915 ⁻⁴	2.671 ⁻²	-9.260 ⁻³	0.874	1.188	-1.758 ⁻³	8.951 ⁻³	4.546 ⁻⁴
0.339	0.978	4.446 ⁻³	2.724 ⁻²	-1.021 ⁻²	0.884	1.192	-9.880 ⁻³	8.217 ⁻³	1.208 ⁻³
0.360	0.995	2.425 ⁻²	2.845 ⁻²	-9.875 ⁻³	0.894	1.179	-1.339 ⁻²	9.202 ⁻³	9.104 ⁻⁴
0.391	0.991	2.381 ⁻²	3.023 ⁻²	-1.019 ⁻²	0.904	1.191	-9.749 ⁻³	7.887 ⁻³	4.221 ⁻⁴
0.471	1.004	2.648 ⁻²	2.796 ⁻²	-1.024 ⁻²	0.911	1.188	-9.893 ⁻³	7.270 ⁻³	8.144 ⁻⁴
0.480	1.042	-4.053 ⁻³	2.512 ⁻²	-9.375 ⁻³	0.918	1.184	-1.311 ⁻²	7.999 ⁻³	9.756 ⁻⁴
0.491	1.019	1.600 ⁻²	2.736 ⁻²	-9.901 ⁻³	0.924	1.185	-1.372 ⁻²	7.905 ⁻³	8.764 ⁻⁴
0.500	1.027	1.309 ⁻²	2.679 ⁻²	-8.712 ⁻³	0.931	1.177	-1.330 ⁻²	7.278 ⁻³	1.210 ⁻³
0.531	1.047	-2.694 ⁻³	2.474 ⁻²	-8.225 ⁻³	0.938	1.158	-1.961 ⁻²	8.740 ⁻³	1.240 ⁻³
0.546	1.060	1.719 ⁻²	2.207 ⁻²	-7.338 ⁻³	0.944	1.134	-1.933 ⁻²	9.203 ⁻³	1.381 ⁻³
0.551	1.044	1.746 ⁻²	2.493 ⁻²	-8.336 ⁻³	0.958	1.144	-1.503 ⁻²	8.344 ⁻³	1.168 ⁻³
0.572	1.068	4.858 ⁻³	2.327 ⁻²	-7.850 ⁻³	0.964	1.113	-1.797 ⁻²	8.993 ⁻³	1.341 ⁻³
0.591	1.074	2.131 ⁻³	2.237 ⁻²	-7.039 ⁻³	0.971	1.081	-1.178 ⁻²	8.401 ⁻³	1.582 ⁻³

Table 18. Concluded ($x/H = 4$)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.026	0.797	-3.636 ⁻³	1.935 ⁻²	-1.966 ⁻³	0.520	1.039	-4.347 ⁻³	2.486 ⁻²	-7.908 ⁻³
0.033	0.805	-7.960 ⁻³	2.052 ⁻²	-2.350 ⁻³	0.531	1.026	-8.015 ⁻³	2.411 ⁻²	-9.046 ⁻³
0.046	0.811	-1.182 ⁻²	2.310 ⁻²	-4.090 ⁻³	0.546	1.051	-9.322 ⁻³	2.389 ⁻²	-7.812 ⁻³
0.066	0.866	-4.793 ⁻³	2.250 ⁻²	-3.831 ⁻³	0.551	1.049	-1.171 ⁻²	2.418 ⁻²	-8.907 ⁻³
0.073	0.827	1.114 ⁻²	2.237 ⁻²	-3.494 ⁻³	0.591	1.048	-5.799 ⁻³	2.373 ⁻²	-7.906 ⁻³
0.080	0.840	-5.294 ⁻³	2.230 ⁻²	-4.719 ⁻³	0.600	1.071	-1.627 ⁻²	2.453 ⁻²	-6.659 ⁻³
0.096	0.880	1.103 ⁻²	2.372 ⁻²	-4.402 ⁻³	0.611	1.067	-1.572 ⁻²	2.113 ⁻²	-6.484 ⁻³
0.106	0.855	-6.041 ⁻³	2.470 ⁻²	-5.957 ⁻³	0.626	1.099	-1.852 ⁻²	2.107 ⁻²	-4.379 ⁻³
0.116	0.850	2.233 ⁻³	2.423 ⁻²	-5.005 ⁻³	0.631	1.065	-2.525 ⁻³	2.159 ⁻²	-5.501 ⁻³
0.136	0.874	5.688 ⁻³	2.545 ⁻²	-7.742 ⁻³	0.652	1.087	-5.203 ⁻³	2.143 ⁻²	-5.733 ⁻³
0.146	0.872	-1.596 ⁻²	2.577 ⁻²	-7.227 ⁻³	0.680	1.121	-9.231 ⁻³	1.986 ⁻²	-3.489 ⁻³
0.156	0.902	-2.333 ⁻²	2.604 ⁻²	-7.379 ⁻³	0.684	1.094	1.801 ⁻³	1.870 ⁻²	-5.097 ⁻³
0.166	0.870	-2.217 ⁻³	2.612 ⁻²	-8.190 ⁻³	0.698	1.112	-1.769 ⁻²	1.775 ⁻²	-2.911 ⁻³
0.176	0.890	2.399 ⁻³	2.686 ⁻²	-7.944 ⁻³	0.711	1.134	-3.538 ⁻²	1.533 ⁻²	-9.452 ⁻⁴
0.200	0.901	-2.181 ⁻²	2.855 ⁻²	-8.535 ⁻³	0.724	1.139	-2.889 ⁻²	1.622 ⁻²	-1.288 ⁻³
0.240	0.907	8.356 ⁻³	2.742 ⁻²	-7.920 ⁻³	0.738	1.136	-2.900 ⁻²	1.636 ⁻²	-9.812 ⁻⁴
0.253	0.906	-2.074 ⁻³	2.753 ⁻²	-9.554 ⁻³	0.751	1.127	-1.318 ⁻³	1.597 ⁻²	-2.669 ⁻³
0.293	0.950	-1.049 ⁻²	2.847 ⁻²	-9.578 ⁻³	0.764	1.137	-3.110 ⁻²	1.513 ⁻²	-1.480 ⁻³
0.320	0.948	-1.086 ⁻²	2.833 ⁻²	-9.948 ⁻³	0.778	1.141	-2.092 ⁻²	1.469 ⁻²	-1.441 ⁻³
0.339	0.943	-1.325 ⁻³	2.863 ⁻²	-1.096 ⁻²	0.791	1.153	-2.083 ⁻²	1.441 ⁻²	-9.981 ⁻⁴
0.364	0.936	-1.203 ⁻³	2.791 ⁻²	-1.063 ⁻²	0.804	1.156	-1.577 ⁻²	1.452 ⁻²	-1.064 ⁻³
0.400	0.987	-2.251 ⁻²	2.910 ⁻²	-1.026 ⁻²	0.814	1.151	-1.523 ⁻²	1.613 ⁻²	-1.313 ⁻³
0.419	0.980	-1.454 ⁻²	2.878 ⁻²	-1.115 ⁻²	0.824	1.153	-2.358 ⁻²	1.353 ⁻²	3.173 ⁻⁴
0.440	1.003	-1.794 ⁻²	2.696 ⁻²	-9.004 ⁻³	0.844	1.149	-3.583 ⁻²	1.487 ⁻²	1.322 ⁻³
0.444	0.966	-1.423 ⁻²	3.081 ⁻²	-1.188 ⁻²	0.854	1.149	-2.379 ⁻²	1.633 ⁻²	1.229 ⁻³
0.460	1.001	7.434 ⁻³	2.651 ⁻²	-8.678 ⁻³	0.874	1.161	-2.660 ⁻²	1.293 ⁻²	1.725 ⁻³
0.480	1.023	-2.108 ⁻²	2.689 ⁻²	-9.187 ⁻³	0.894	1.166	-2.792 ⁻²	1.091 ⁻²	2.621 ⁻³
0.491	0.993	-2.880 ⁻³	2.593 ⁻²	-9.883 ⁻³	0.904	1.162	-2.302 ⁻²	1.301 ⁻²	2.265 ⁻³
0.500	1.013	-5.961 ⁻³	2.634 ⁻²	-8.232 ⁻³					

Legend: $Re=1 \times 10^5$: $z/H=0$ (\odot); $Re=1 \times 10^6$: $z/H=0$ (\diamond), $z/H=1$ (Δ), $z/H=2$ (\square), $z/H=3$ (+)

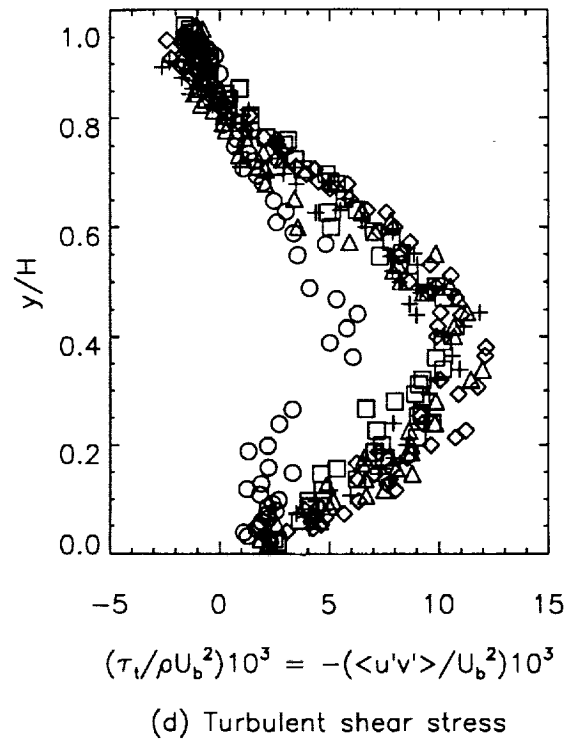
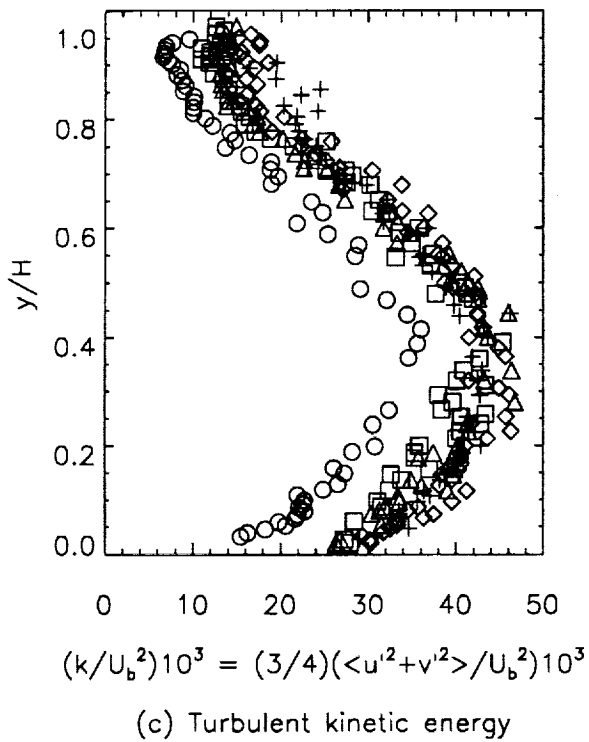
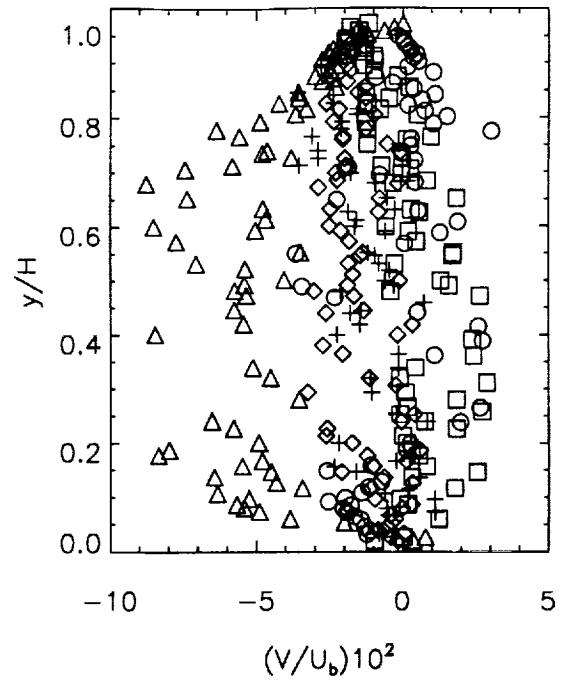
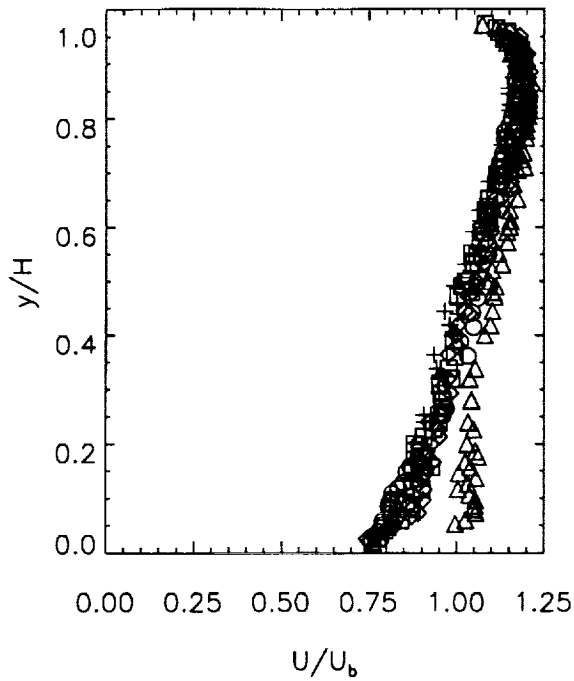


Figure 18. Summary of Table 18 ($\bar{x}/H = 4$).

Table 19. LDV flowfield data in TAD ($x/H = 5$)

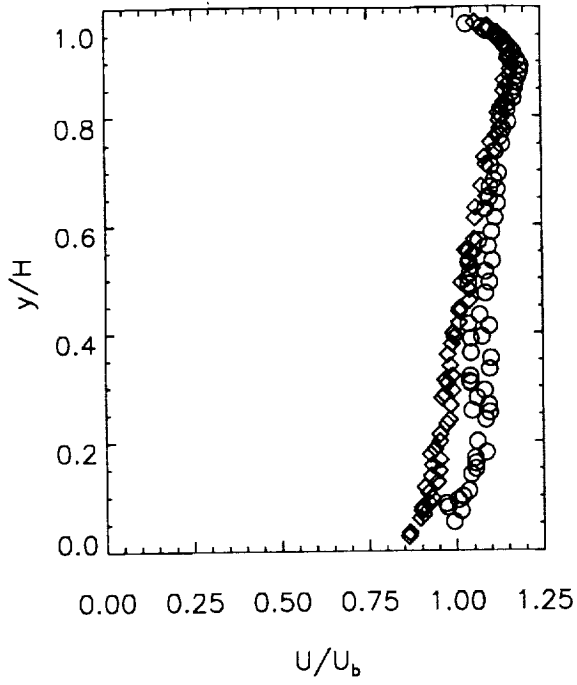
($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.053	0.992	7.160^{-4}	1.820^{-2}	-2.629^{-3}	0.560	1.095	-4.175^{-4}	1.818^{-2}	-6.705^{-3}
0.073	1.012	-1.139^{-2}	1.827^{-2}	-2.538^{-3}	0.570	1.068	1.787^{-2}	1.931^{-2}	-7.823^{-3}
0.080	0.974	1.737^{-2}	1.892^{-2}	-2.295^{-3}	0.586	1.105	-1.128^{-2}	1.833^{-2}	-6.146^{-3}
0.086	0.970	1.230^{-2}	1.818^{-2}	-3.189^{-3}	0.613	1.115	-1.169^{-2}	1.666^{-2}	-5.243^{-3}
0.093	1.003	2.134^{-2}	1.731^{-2}	-2.946^{-3}	0.630	1.088	9.003^{-4}	1.767^{-2}	-6.527^{-3}
0.100	1.018	1.068^{-2}	1.859^{-2}	-3.932^{-3}	0.640	1.122	-1.420^{-2}	1.564^{-2}	-4.899^{-3}
0.110	1.035	6.189^{-3}	1.782^{-2}	-4.558^{-3}	0.650	1.099	8.733^{-4}	1.565^{-2}	-6.033^{-3}
0.140	1.042	2.282^{-2}	1.737^{-2}	-3.837^{-3}	0.666	1.122	-5.641^{-4}	1.470^{-2}	-4.716^{-3}
0.150	1.055	-5.119^{-3}	1.874^{-2}	-4.777^{-3}	0.670	1.102	-1.333^{-2}	1.474^{-2}	-5.105^{-3}
0.160	1.056	3.713^{-3}	1.906^{-2}	-5.199^{-3}	0.683	1.114	-9.976^{-3}	1.388^{-2}	-4.584^{-3}
0.170	1.054	8.425^{-3}	1.880^{-2}	-4.799^{-3}	0.696	1.127	-2.939^{-2}	1.257^{-2}	-3.732^{-3}
0.180	1.086	-4.900^{-2}	1.850^{-2}	-5.176^{-3}	0.710	1.105	2.287^{-3}	1.393^{-2}	-5.108^{-3}
0.200	1.061	-2.364^{-3}	1.892^{-2}	-4.856^{-3}	0.736	1.118	1.596^{-2}	1.204^{-2}	-4.186^{-3}
0.240	1.085	-1.263^{-2}	1.962^{-2}	-4.970^{-3}	0.750	1.137	-2.294^{-2}	1.036^{-2}	-2.796^{-3}
0.253	1.097	-5.010^{-2}	1.906^{-2}	-6.022^{-3}	0.763	1.131	-1.465^{-2}	1.097^{-2}	-3.109^{-3}
0.256	1.045	2.276^{-2}	2.069^{-2}	-5.825^{-3}	0.776	1.140	-6.853^{-3}	1.049^{-2}	-2.993^{-3}
0.266	1.094	-4.605^{-2}	1.969^{-2}	-5.504^{-3}	0.790	1.155	-2.359^{-2}	8.451^{-3}	-1.899^{-3}
0.280	1.060	1.079^{-2}	2.180^{-2}	-5.796^{-3}	0.803	1.137	-1.033^{-3}	1.008^{-2}	-2.885^{-3}
0.293	1.082	-3.600^{-2}	2.133^{-2}	-6.757^{-3}	0.813	1.154	3.080^{-3}	8.878^{-3}	-2.145^{-3}
0.306	1.043	2.508^{-2}	2.193^{-2}	-6.566^{-3}	0.823	1.154	-3.182^{-3}	8.065^{-3}	-1.815^{-3}
0.310	1.038	3.397^{-2}	2.170^{-2}	-6.151^{-3}	0.833	1.171	-7.700^{-4}	7.039^{-3}	-1.607^{-3}
0.320	1.041	2.523^{-2}	2.158^{-2}	-6.489^{-3}	0.843	1.167	4.290^{-3}	6.969^{-3}	-1.713^{-3}
0.333	1.097	-5.064^{-2}	2.076^{-2}	-6.384^{-3}	0.853	1.176	3.692^{-3}	6.490^{-3}	-1.402^{-3}
0.353	1.100	-4.976^{-2}	1.998^{-2}	-6.309^{-3}	0.863	1.179	-4.840^{-3}	5.519^{-3}	-8.297^{-4}
0.363	1.043	5.326^{-2}	2.214^{-2}	-5.991^{-3}	0.873	1.185	4.947^{-4}	4.969^{-3}	-4.979^{-4}
0.390	1.043	4.822^{-2}	2.277^{-2}	-7.340^{-3}	0.883	1.191	6.610^{-4}	4.346^{-3}	-4.780^{-4}
0.393	1.076	-8.157^{-3}	2.166^{-2}	-7.377^{-3}	0.893	1.191	1.525^{-3}	4.036^{-3}	-1.537^{-4}
0.413	1.096	-3.132^{-2}	2.146^{-2}	-7.424^{-3}	0.903	1.182	-1.687^{-3}	3.955^{-3}	1.281^{-4}
0.416	1.037	3.312^{-2}	2.155^{-2}	-7.693^{-3}	0.910	1.165	-4.773^{-3}	4.359^{-3}	3.218^{-4}
0.433	1.070	7.053^{-3}	2.150^{-2}	-7.205^{-3}	0.916	1.172	-3.416^{-4}	4.085^{-3}	2.953^{-4}
0.473	1.086	-1.427^{-2}	2.195^{-2}	-7.885^{-3}	0.923	1.163	9.916^{-5}	4.213^{-3}	4.099^{-4}
0.490	1.038	3.810^{-2}	2.069^{-2}	-8.068^{-3}	0.930	1.154	2.965^{-5}	4.471^{-3}	5.647^{-4}
0.493	1.098	-2.054^{-2}	2.025^{-2}	-7.050^{-3}	0.936	1.145	2.242^{-4}	4.859^{-3}	5.884^{-4}
0.510	1.042	4.318^{-2}	2.067^{-2}	-7.132^{-3}	0.943	1.137	1.023^{-3}	5.224^{-3}	4.807^{-4}
0.513	1.087	-9.719^{-3}	2.082^{-2}	-7.251^{-3}	0.950	1.122	2.900^{-3}	5.725^{-3}	8.990^{-4}
0.530	1.038	4.888^{-2}	2.166^{-2}	-7.502^{-3}	0.956	1.095	3.751^{-3}	6.165^{-3}	1.012^{-3}
0.533	1.107	-3.302^{-2}	1.914^{-2}	-6.521^{-3}	0.963	1.082	5.193^{-3}	6.479^{-3}	1.179^{-3}
0.550	1.041	5.484^{-2}	1.945^{-2}	-6.603^{-3}	0.970	1.035	5.097^{-3}	6.643^{-3}	1.436^{-3}

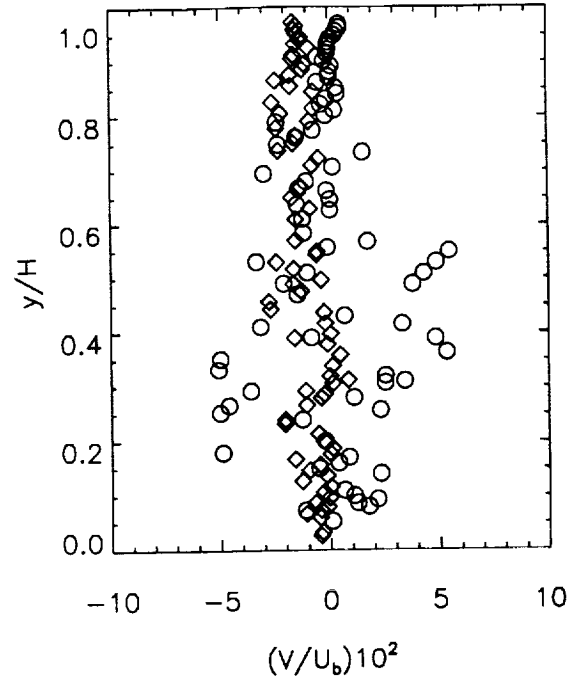
Table 19. Concluded ($x/H = 5$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.026	0.862	-4.338 ⁻³	1.980 ⁻²	-2.982 ⁻³	0.492	1.017	-1.608 ⁻²	2.336 ⁻²	-9.174 ⁻³
0.033	0.865	-3.718 ⁻³	2.025 ⁻²	-3.927 ⁻³	0.500	1.034	-3.410 ⁻³	2.424 ⁻²	-8.921 ⁻³
0.060	0.895	-4.727 ⁻³	1.926 ⁻²	-3.977 ⁻³	0.520	1.049	-1.589 ⁻²	2.500 ⁻²	-9.007 ⁻³
0.066	0.905	-1.103 ⁻²	2.024 ⁻²	-3.251 ⁻³	0.532	1.039	-2.382 ⁻²	2.216 ⁻²	-7.564 ⁻³
0.073	0.900	-4.422 ⁻³	1.961 ⁻²	-3.741 ⁻³	0.546	1.051	-5.447 ⁻³	2.442 ⁻²	-8.561 ⁻³
0.080	0.901	-1.390 ⁻³	1.962 ⁻²	-4.935 ⁻³	0.552	1.029	-5.249 ⁻³	2.198 ⁻²	-8.543 ⁻³
0.086	0.922	-6.874 ⁻³	1.989 ⁻²	-3.701 ⁻³	0.573	1.055	-1.502 ⁻²	2.211 ⁻²	-7.618 ⁻³
0.096	0.930	-5.374 ⁻⁴	1.995 ⁻²	-4.124 ⁻³	0.612	1.057	-1.480 ⁻²	1.997 ⁻²	-6.884 ⁻³
0.106	0.918	-3.000 ⁻³	2.000 ⁻²	-4.535 ⁻³	0.632	1.059	-8.377 ⁻³	1.946 ⁻²	-7.226 ⁻³
0.116	0.909	9.972 ⁻⁶	1.920 ⁻²	-4.090 ⁻³	0.653	1.091	-1.667 ⁻²	2.039 ⁻²	-6.721 ⁻³
0.126	0.945	-1.283 ⁻²	2.115 ⁻²	-6.188 ⁻³	0.672	1.077	-1.231 ⁻²	1.783 ⁻²	-6.700 ⁻³
0.136	0.927	-1.700 ⁻³	2.100 ⁻²	-5.722 ⁻³	0.712	1.090	-7.304 ⁻³	1.698 ⁻²	-5.183 ⁻³
0.146	0.951	-9.428 ⁻³	2.093 ⁻²	-6.022 ⁻³	0.726	1.086	-4.348 ⁻³	1.752 ⁻²	-5.952 ⁻³
0.156	0.931	-4.815 ⁻³	2.074 ⁻²	-5.915 ⁻³	0.739	1.117	-2.281 ⁻²	1.472 ⁻²	-4.129 ⁻³
0.166	0.953	-1.605 ⁻²	2.124 ⁻²	-6.450 ⁻³	0.752	1.104	-1.591 ⁻²	1.604 ⁻²	-5.038 ⁻³
0.176	0.925	1.341 ⁻⁴	1.974 ⁻²	-6.480 ⁻³	0.766	1.120	-1.471 ⁻²	1.503 ⁻²	-3.642 ⁻³
0.186	0.938	1.013 ⁻³	2.065 ⁻²	-6.464 ⁻³	0.779	1.132	-2.372 ⁻²	1.402 ⁻²	-3.504 ⁻³
0.200	0.953	-2.745 ⁻³	2.157 ⁻²	-7.360 ⁻³	0.792	1.129	-8.646 ⁻³	1.454 ⁻²	-3.784 ⁻³
0.213	0.953	-5.333 ⁻³	2.293 ⁻²	-8.466 ⁻³	0.806	1.126	-2.178 ⁻²	1.415 ⁻²	-1.995 ⁻³
0.232	0.973	-2.052 ⁻²	2.181 ⁻²	-6.166 ⁻³	0.816	1.133	-6.764 ⁻³	1.293 ⁻²	-2.196 ⁻³
0.240	0.981	-2.039 ⁻²	2.347 ⁻²	-8.649 ⁻³	0.826	1.143	-2.565 ⁻²	1.209 ⁻²	-1.601 ⁻³
0.266	0.984	-1.073 ⁻²	2.319 ⁻²	-8.907 ⁻³	0.846	1.143	-6.716 ⁻³	1.233 ⁻²	-1.483 ⁻³
0.280	0.960	-4.023 ⁻³	2.345 ⁻²	-8.077 ⁻³	0.856	1.151	-1.723 ⁻²	1.069 ⁻²	-1.041 ⁻³
0.286	0.966	-2.666 ⁻³	2.195 ⁻²	-7.685 ⁻³	0.866	1.144	-2.414 ⁻²	1.152 ⁻²	-4.039 ⁻⁴
0.293	0.990	-1.102 ⁻²	2.380 ⁻²	-9.091 ⁻³	0.876	1.160	-1.745 ⁻²	9.745 ⁻³	-2.911 ⁻⁴
0.306	0.975	1.299 ⁻³	2.282 ⁻²	-7.941 ⁻³	0.886	1.162	-1.162 ⁻²	9.823 ⁻³	-5.758 ⁻⁴
0.312	0.968	8.335 ⁻³	2.303 ⁻²	-7.016 ⁻³	0.896	1.166	-1.072 ⁻²	9.412 ⁻³	1.707 ⁻⁴
0.320	0.989	8.927 ⁻⁵	2.426 ⁻²	-8.580 ⁻³	0.906	1.154	-1.636 ⁻²	1.012 ⁻²	9.201 ⁻⁵
0.339	0.984	1.229 ⁻³	2.450 ⁻²	-7.953 ⁻³	0.912	1.156	-1.580 ⁻²	9.222 ⁻³	4.742 ⁻⁴
0.360	0.977	4.776 ⁻³	2.458 ⁻²	-9.120 ⁻³	0.926	1.147	-8.954 ⁻³	9.443 ⁻³	2.575 ⁻⁵
0.380	0.989	-8.894 ⁻⁴	2.408 ⁻²	-9.238 ⁻³	0.932	1.146	-1.496 ⁻²	9.170 ⁻³	4.903 ⁻⁴
0.392	0.996	-1.578 ⁻²	2.311 ⁻²	-7.789 ⁻³	0.939	1.129	-1.276 ⁻²	1.049 ⁻²	6.616 ⁻⁴
0.400	0.993	5.957 ⁻⁴	2.500 ⁻²	-8.933 ⁻³	0.946	1.132	-1.257 ⁻²	9.372 ⁻³	7.740 ⁻⁴
0.419	1.010	-1.715 ⁻³	2.394 ⁻²	-8.383 ⁻³	0.952	1.126	-1.453 ⁻²	8.922 ⁻³	1.106 ⁻³
0.440	1.011	-2.172 ⁻³	2.374 ⁻²	-9.554 ⁻³	0.959	1.099	-1.523 ⁻²	9.273 ⁻³	1.323 ⁻³
0.446	1.013	-2.658 ⁻²	2.418 ⁻²	-9.364 ⁻³	0.966	1.097	-1.458 ⁻²	9.427 ⁻³	9.446 ⁻⁴
0.460	1.040	-2.735 ⁻²	2.454 ⁻²	-9.732 ⁻³	0.972	1.061	-1.602 ⁻²	1.060 ⁻²	9.863 ⁻⁴
0.480	1.041	-1.249 ⁻²	2.430 ⁻²	-9.257 ⁻³					

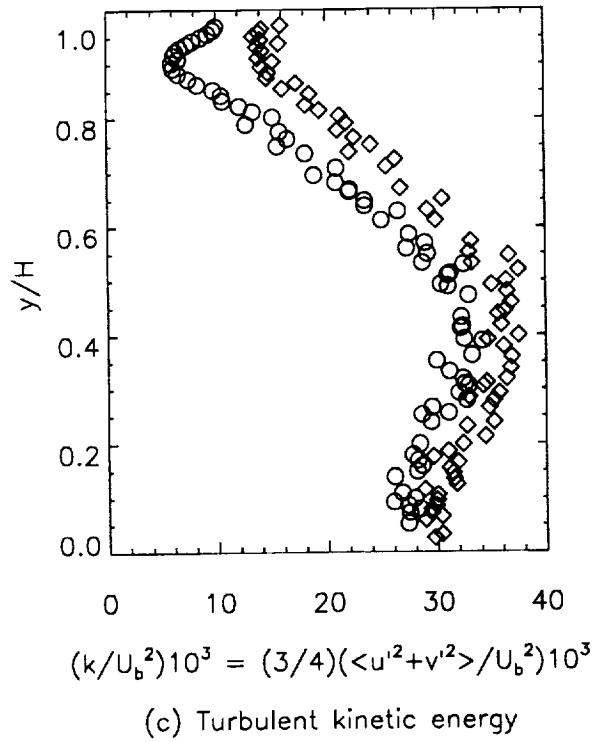
Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)



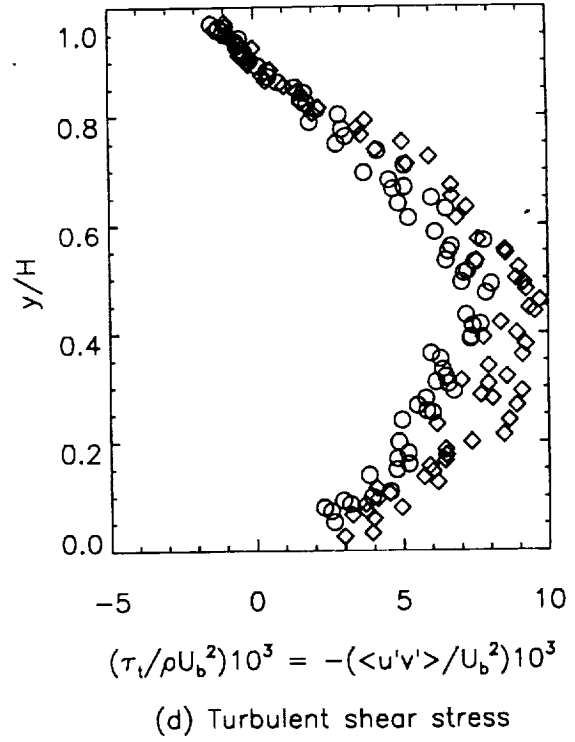
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 19. Summary of Table 19 ($x/H = 5$).

Table 20. LDV flowfield data in TAD ($x/H = 6$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.028	0.856	-5.156 ⁻³	1.667 ⁻²	-1.692 ⁻³	0.511	1.043	3.882 ⁻²	1.625 ⁻²	-5.021 ⁻³
0.034	0.853	-2.865 ⁻³	1.615 ⁻²	-1.595 ⁻³	0.528	1.070	2.634 ⁻²	1.642 ⁻²	-5.108 ⁻³
0.041	0.876	-2.588 ⁻³	1.545 ⁻²	-2.194 ⁻³	0.551	1.082	-6.934 ⁻³	1.568 ⁻²	-5.898 ⁻³
0.048	0.875	1.202 ⁻³	1.451 ⁻²	-2.416 ⁻³	0.554	1.066	2.838 ⁻²	1.664 ⁻²	-5.128 ⁻³
0.054	0.868	7.733 ⁻⁴	1.405 ⁻²	-1.557 ⁻³	0.571	1.068	6.725 ⁻³	1.610 ⁻²	-5.836 ⁻³
0.061	0.894	-4.075 ⁻⁵	1.534 ⁻²	-1.537 ⁻³	0.591	1.057	3.064 ⁻²	1.442 ⁻²	-4.646 ⁻³
0.068	0.937	7.324 ⁻³	1.554 ⁻²	-1.849 ⁻³	0.631	1.067	2.423 ⁻²	1.424 ⁻²	-5.223 ⁻³
0.074	0.989	6.942 ⁻³	1.539 ⁻²	-1.913 ⁻³	0.661	1.099	1.780 ⁻²	1.389 ⁻²	-4.556 ⁻³
0.081	1.023	1.147 ⁻³	1.470 ⁻²	-2.939 ⁻³	0.671	1.072	2.426 ⁻²	1.314 ⁻²	-4.558 ⁻³
0.088	1.014	-2.274 ⁻³	1.496 ⁻²	-3.236 ⁻³	0.684	1.101	-9.221 ⁻³	1.176 ⁻²	-3.877 ⁻³
0.094	0.985	1.419 ⁻²	1.404 ⁻²	-2.622 ⁻³	0.698	1.080	1.685 ⁻²	1.286 ⁻²	-4.432 ⁻³
0.114	1.038	6.837 ⁻³	1.482 ⁻²	-2.791 ⁻³	0.711	1.094	1.631 ⁻²	1.213 ⁻²	-4.311 ⁻³
0.124	1.023	2.394 ⁻²	1.431 ⁻²	-2.276 ⁻³	0.714	1.112	1.452 ⁻²	1.258 ⁻²	-3.902 ⁻³
0.134	1.050	2.305 ⁻²	1.393 ⁻²	-2.635 ⁻³	0.724	1.084	1.990 ⁻²	1.160 ⁻²	-3.711 ⁻³
0.144	1.017	1.813 ⁻²	1.460 ⁻²	-2.646 ⁻³	0.738	1.105	-5.211 ⁻³	1.063 ⁻²	-3.414 ⁻³
0.154	1.018	1.730 ⁻²	1.433 ⁻²	-2.400 ⁻³	0.751	1.098	1.649 ⁻²	1.103 ⁻²	-3.709 ⁻³
0.164	1.027	2.696 ⁻²	1.494 ⁻²	-2.855 ⁻³	0.764	1.120	-5.835 ⁻³	8.690 ⁻³	-1.791 ⁻³
0.174	1.042	3.279 ⁻²	1.502 ⁻²	-3.109 ⁻³	0.778	1.121	1.234 ⁻²	8.871 ⁻³	-2.794 ⁻³
0.184	1.044	2.007 ⁻²	1.540 ⁻²	-3.157 ⁻³	0.791	1.119	6.181 ⁻³	9.068 ⁻³	-2.690 ⁻³
0.194	1.007	2.327 ⁻²	1.488 ⁻²	-3.035 ⁻³	0.804	1.128	-8.862 ⁻³	8.183 ⁻³	-1.580 ⁻³
0.208	1.042	3.020 ⁻²	1.548 ⁻²	-2.931 ⁻³	0.814	1.137	8.489 ⁻³	7.893 ⁻³	-1.891 ⁻³
0.221	1.035	3.897 ⁻²	1.578 ⁻²	-3.145 ⁻³	0.824	1.143	-5.229 ⁻³	7.205 ⁻³	-1.488 ⁻³
0.231	1.017	2.947 ⁻²	1.671 ⁻²	-4.360 ⁻³	0.844	1.159	-4.184 ⁻³	6.329 ⁻³	-1.276 ⁻³
0.234	1.065	1.940 ⁻²	1.614 ⁻²	-4.104 ⁻³	0.854	1.162	-8.088 ⁻⁴	5.735 ⁻³	-9.976 ⁻⁴
0.248	1.062	1.148 ⁻²	1.733 ⁻²	-3.909 ⁻³	0.864	1.173	7.456 ⁻⁴	4.909 ⁻³	-6.946 ⁻⁴
0.258	1.054	9.451 ⁻³	1.707 ⁻²	-5.087 ⁻³	0.874	1.163	2.241 ⁻⁴	5.278 ⁻³	-6.224 ⁻⁴
0.261	1.070	3.573 ⁻³	1.665 ⁻²	-4.134 ⁻³	0.884	1.174	3.144 ⁻³	4.667 ⁻³	-6.367 ⁻⁴
0.274	1.065	3.230 ⁻²	1.784 ⁻²	-4.257 ⁻³	0.894	1.174	5.691 ⁻⁴	4.035 ⁻³	-2.079 ⁻⁴
0.288	1.057	1.444 ⁻²	1.647 ⁻²	-3.932 ⁻³	0.904	1.160	-1.459 ⁻³	4.454 ⁻³	6.146 ⁻⁵
0.311	1.058	7.011 ⁻³	1.774 ⁻²	-5.443 ⁻³	0.911	1.164	1.095 ⁻³	3.820 ⁻³	1.383 ⁻⁴
0.314	1.074	1.049 ⁻²	1.772 ⁻²	-5.311 ⁻³	0.918	1.159	1.136 ⁻³	4.248 ⁻³	2.580 ⁻⁴
0.328	1.071	7.996 ⁻³	1.805 ⁻²	-4.855 ⁻³	0.924	1.138	3.659 ⁻⁴	4.518 ⁻³	4.902 ⁻⁴
0.348	1.073	1.776 ⁻²	1.831 ⁻²	-4.484 ⁻³	0.931	1.126	1.416 ⁻³	4.897 ⁻³	7.251 ⁻⁴
0.364	1.056	-7.188 ⁻⁴	1.775 ⁻²	-5.859 ⁻³	0.938	1.110	8.888 ⁻⁴	5.012 ⁻³	6.873 ⁻⁴
0.428	1.069	4.383 ⁻³	1.804 ⁻²	-5.552 ⁻³	0.944	1.094	3.056 ⁻³	5.594 ⁻³	9.731 ⁻⁴
0.448	1.040	3.715 ⁻²	1.753 ⁻²	-5.365 ⁻³	0.951	1.088	4.875 ⁻³	5.628 ⁻³	1.032 ⁻³
0.468	1.071	6.847 ⁻³	1.719 ⁻²	-5.341 ⁻³	0.958	1.056	3.494 ⁻³	6.037 ⁻³	9.947 ⁻⁴
0.471	1.069	-2.243 ⁻³	1.689 ⁻²	-4.904 ⁻³	0.964	1.024	4.571 ⁻³	6.658 ⁻³	1.367 ⁻³
0.508	1.082	5.877 ⁻³	1.766 ⁻²	-5.747 ⁻³	0.971	1.000	6.584 ⁻³	5.961 ⁻³	1.217 ⁻³

Table 20. Continued ($x/H = 6$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.033	0.862	3.767^{-3}	1.372^{-2}	-1.989^{-3}	0.494	1.035	-1.656^{-2}	1.878^{-2}	-7.272^{-3}
0.040	0.886	5.166^{-3}	1.521^{-2}	-2.087^{-3}	0.500	1.032	-2.396^{-2}	1.790^{-2}	-6.544^{-3}
0.046	0.883	3.895^{-3}	1.519^{-2}	-1.842^{-3}	0.514	1.035	-3.908^{-3}	1.885^{-2}	-7.071^{-3}
0.053	0.886	4.035^{-3}	1.409^{-2}	-1.855^{-3}	0.534	1.041	-2.393^{-2}	1.821^{-2}	-6.945^{-3}
0.060	0.917	-1.213^{-3}	1.511^{-2}	-1.994^{-3}	0.554	1.053	-2.617^{-2}	1.764^{-2}	-6.950^{-3}
0.066	0.920	-4.775^{-3}	1.624^{-2}	-2.800^{-3}	0.573	1.055	-1.485^{-2}	1.721^{-2}	-6.099^{-3}
0.073	0.928	6.269^{-5}	1.517^{-2}	-2.465^{-3}	0.594	1.066	-2.370^{-2}	1.697^{-2}	-5.930^{-3}
0.080	0.916	3.533^{-3}	1.428^{-2}	-2.413^{-3}	0.634	1.073	-2.665^{-2}	1.587^{-2}	-5.093^{-3}
0.086	0.925	-3.975^{-3}	1.458^{-2}	-2.511^{-3}	0.653	1.077	-1.826^{-2}	1.582^{-2}	-5.547^{-3}
0.096	0.941	-3.588^{-4}	1.621^{-2}	-2.749^{-3}	0.674	1.087	-2.886^{-2}	1.476^{-2}	-5.019^{-3}
0.106	0.943	-2.996^{-3}	1.576^{-2}	-3.624^{-3}	0.687	1.099	-3.926^{-2}	1.451^{-2}	-4.161^{-3}
0.116	0.940	2.281^{-3}	1.484^{-2}	-3.438^{-3}	0.700	1.109	-3.733^{-2}	1.377^{-2}	-4.281^{-3}
0.136	0.932	9.779^{-4}	1.525^{-2}	-3.772^{-3}	0.740	1.118	-2.762^{-2}	1.319^{-2}	-3.242^{-3}
0.146	0.952	-5.239^{-3}	1.651^{-2}	-4.259^{-3}	0.754	1.115	-3.091^{-2}	1.374^{-2}	-3.436^{-3}
0.156	0.936	4.912^{-3}	1.518^{-2}	-3.351^{-3}	0.767	1.119	-3.347^{-2}	1.234^{-2}	-2.900^{-3}
0.166	0.965	-7.397^{-4}	1.611^{-2}	-3.184^{-3}	0.780	1.130	-3.939^{-2}	1.193^{-2}	-2.167^{-3}
0.200	0.952	1.425^{-2}	1.648^{-2}	-3.428^{-3}	0.794	1.127	-2.285^{-2}	1.198^{-2}	-2.295^{-3}
0.213	0.969	1.047^{-2}	1.635^{-2}	-3.633^{-3}	0.817	1.134	-2.138^{-2}	1.136^{-2}	-1.854^{-3}
0.226	0.963	4.627^{-3}	1.682^{-2}	-4.390^{-3}	0.827	1.132	-1.878^{-2}	1.143^{-2}	-2.488^{-3}
0.240	0.980	2.203^{-3}	1.684^{-2}	-3.891^{-3}	0.837	1.134	-1.904^{-2}	9.929^{-3}	-1.408^{-3}
0.253	0.969	-1.459^{-2}	1.674^{-2}	-5.246^{-3}	0.857	1.139	-2.085^{-2}	9.730^{-3}	-1.168^{-3}
0.266	0.972	9.642^{-3}	1.807^{-2}	-5.378^{-3}	0.867	1.142	-1.787^{-2}	9.441^{-3}	-8.204^{-4}
0.280	0.975	5.283^{-3}	1.826^{-2}	-5.828^{-3}	0.877	1.141	-1.421^{-2}	1.031^{-2}	-6.516^{-4}
0.287	0.989	-1.524^{-3}	1.852^{-2}	-5.916^{-3}	0.887	1.145	-2.446^{-2}	8.921^{-3}	1.067^{-4}
0.293	0.972	3.190^{-3}	1.793^{-2}	-5.865^{-3}	0.897	1.132	-1.897^{-2}	8.869^{-3}	-1.107^{-4}
0.306	0.974	8.579^{-3}	1.819^{-2}	-5.500^{-3}	0.914	1.130	-1.517^{-2}	8.055^{-3}	7.140^{-5}
0.320	0.976	7.650^{-3}	1.743^{-2}	-5.416^{-3}	0.920	1.129	-1.750^{-2}	8.218^{-3}	1.965^{-4}
0.340	1.009	-1.928^{-2}	1.891^{-2}	-6.877^{-3}	0.927	1.108	-6.234^{-3}	8.935^{-3}	-6.249^{-4}
0.394	1.006	-9.212^{-3}	1.922^{-2}	-7.226^{-3}	0.934	1.116	-1.383^{-2}	8.440^{-3}	4.576^{-4}
0.420	1.000	7.315^{-3}	1.872^{-2}	-5.931^{-3}	0.940	1.112	-1.445^{-2}	8.267^{-3}	3.456^{-4}
0.440	0.997	1.121^{-2}	1.829^{-2}	-6.196^{-3}	0.947	1.097	-1.231^{-2}	8.655^{-3}	1.042^{-4}
0.460	1.007	-5.068^{-3}	1.890^{-2}	-6.757^{-3}	0.954	1.107	-1.201^{-2}	8.566^{-3}	7.778^{-4}
0.474	1.020	-1.752^{-2}	1.948^{-2}	-7.640^{-3}	0.960	1.064	-1.891^{-2}	8.698^{-3}	1.012^{-3}
0.480	1.017	-5.097^{-3}	1.823^{-2}	-7.176^{-3}	0.974	1.044	-1.014^{-2}	7.555^{-3}	1.099^{-3}

Table 20. Continued ($x/H = 6$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.046	1.054	-2.377 ⁻²	1.482 ⁻²	-1.273 ⁻³	0.554	1.114	-1.090 ⁻¹	1.468 ⁻²	-1.998 ⁻³
0.060	1.093	-2.254 ⁻²	1.361 ⁻²	-4.354 ⁻⁴	0.573	1.107	-8.742 ⁻²	1.519 ⁻²	-3.502 ⁻³
0.066	1.082	-1.867 ⁻²	1.444 ⁻²	-8.778 ⁻⁴	0.594	1.127	-1.028 ⁻¹	1.274 ⁻²	-2.123 ⁻³
0.073	1.084	-2.898 ⁻²	1.432 ⁻²	-4.773 ⁻⁴	0.614	1.120	-7.645 ⁻²	1.488 ⁻²	-2.986 ⁻³
0.080	1.077	-2.651 ⁻²	1.549 ⁻²	-1.547 ⁻³	0.626	1.120	-8.405 ⁻²	1.355 ⁻²	-1.816 ⁻³
0.096	1.085	-3.322 ⁻²	1.404 ⁻²	-9.871 ⁻⁴	0.653	1.120	-8.632 ⁻²	1.316 ⁻²	-1.771 ⁻³
0.106	1.085	-3.501 ⁻²	1.412 ⁻²	-1.927 ⁻³	0.674	1.120	-9.187 ⁻²	1.180 ⁻²	-1.499 ⁻³
0.116	1.103	-3.671 ⁻²	1.309 ⁻²	-9.599 ⁻⁴	0.687	1.125	-8.487 ⁻²	1.244 ⁻²	-1.507 ⁻³
0.126	1.091	-4.094 ⁻²	1.361 ⁻²	-1.226 ⁻³	0.714	1.121	-6.912 ⁻²	1.492 ⁻²	-2.055 ⁻³
0.136	1.076	-2.362 ⁻²	1.512 ⁻²	-1.735 ⁻³	0.727	1.133	-8.169 ⁻²	1.126 ⁻²	-4.270 ⁻⁴
0.146	1.090	-4.488 ⁻²	1.454 ⁻²	-1.562 ⁻³	0.733	1.122	-6.684 ⁻²	1.308 ⁻²	-9.259 ⁻⁴
0.156	1.099	-6.092 ⁻²	1.442 ⁻²	-2.445 ⁻³	0.740	1.131	-7.140 ⁻²	1.166 ⁻²	-6.243 ⁻⁴
0.166	1.084	-3.886 ⁻²	1.583 ⁻²	-1.606 ⁻³	0.754	1.127	-6.580 ⁻²	1.422 ⁻²	-3.664 ⁻⁴
0.176	1.100	-5.749 ⁻²	1.475 ⁻²	-1.201 ⁻³	0.767	1.123	-7.335 ⁻²	1.356 ⁻²	-1.741 ⁻⁴
0.186	1.079	-4.177 ⁻²	1.641 ⁻²	-2.596 ⁻³	0.780	1.122	-6.433 ⁻²	1.301 ⁻²	8.063 ⁻⁴
0.200	1.101	-7.460 ⁻²	1.445 ⁻²	-2.335 ⁻³	0.794	1.138	-5.355 ⁻²	1.143 ⁻²	-3.810 ⁻⁴
0.213	1.098	-8.018 ⁻²	1.485 ⁻²	-1.385 ⁻³	0.807	1.138	-6.732 ⁻²	1.141 ⁻²	1.052 ⁻³
0.240	1.075	-4.866 ⁻²	1.751 ⁻²	-3.564 ⁻³	0.817	1.130	-7.268 ⁻²	1.302 ⁻²	1.644 ⁻³
0.253	1.080	-6.908 ⁻²	1.702 ⁻²	-3.738 ⁻³	0.827	1.125	-5.338 ⁻²	1.442 ⁻²	4.773 ⁻⁴
0.314	1.100	-1.051 ⁻¹	1.664 ⁻²	-2.875 ⁻³	0.847	1.123	-6.350 ⁻²	1.200 ⁻²	1.976 ⁻³
0.320	1.100	-8.817 ⁻²	1.625 ⁻²	-3.154 ⁻³	0.867	1.116	-5.830 ⁻²	1.218 ⁻²	2.472 ⁻³
0.340	1.089	-9.320 ⁻²	1.679 ⁻²	-3.401 ⁻³	0.877	1.102	-6.525 ⁻²	1.379 ⁻²	4.842 ⁻³
0.360	1.088	-8.981 ⁻²	1.706 ⁻²	-2.665 ⁻³	0.887	1.116	-4.121 ⁻²	1.384 ⁻²	2.160 ⁻³
0.367	1.088	-9.099 ⁻²	1.752 ⁻²	-4.233 ⁻³	0.897	1.101	-4.815 ⁻²	1.489 ⁻²	3.198 ⁻³
0.380	1.085	-7.549 ⁻²	1.722 ⁻²	-3.675 ⁻³	0.907	1.101	-5.738 ⁻²	1.294 ⁻²	3.630 ⁻³
0.447	1.108	-1.084 ⁻¹	1.581 ⁻²	-3.185 ⁻³	0.914	1.091	-5.868 ⁻²	1.407 ⁻²	5.034 ⁻³
0.460	1.100	-1.081 ⁻¹	1.570 ⁻²	-2.419 ⁻³	0.927	1.074	-5.201 ⁻²	1.516 ⁻²	5.201 ⁻³
0.480	1.111	-9.764 ⁻²	1.467 ⁻²	-2.465 ⁻³	0.940	1.082	-5.278 ⁻²	1.435 ⁻²	5.574 ⁻³
0.494	1.103	-9.369 ⁻²	1.652 ⁻²	-4.047 ⁻³	0.947	1.073	-4.984 ⁻²	1.446 ⁻²	5.520 ⁻³
0.514	1.111	-1.034 ⁻¹	1.572 ⁻²	-2.577 ⁻³	0.954	1.063	-5.103 ⁻²	1.399 ⁻²	5.957 ⁻³
0.546	1.110	-7.984 ⁻²	1.507 ⁻²	-2.956 ⁻³					

Table 20. Continued ($x/H = 6$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

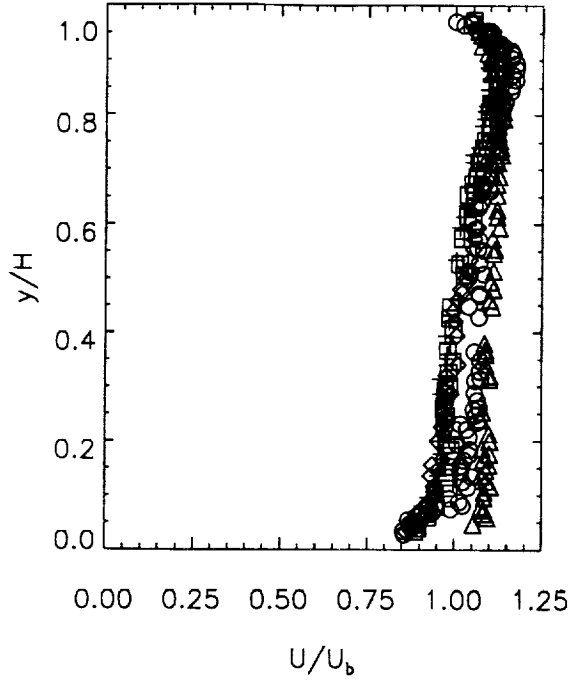
y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.033	0.886	-3.785^{-3}	1.497^{-2}	-9.115^{-4}	0.526	1.014	1.312^{-2}	1.821^{-2}	-4.598^{-3}
0.040	0.895	2.696^{-4}	1.478^{-2}	-6.889^{-4}	0.574	1.020	7.940^{-3}	1.648^{-2}	-5.589^{-3}
0.046	0.889	3.532^{-3}	1.451^{-2}	-3.720^{-4}	0.606	1.051	-7.490^{-3}	1.741^{-2}	-4.468^{-3}
0.060	0.924	7.177^{-3}	1.523^{-2}	-5.859^{-4}	0.614	1.035	1.337^{-2}	1.632^{-2}	-5.755^{-3}
0.066	0.924	7.734^{-3}	1.506^{-2}	-4.356^{-4}	0.633	1.055	-7.926^{-4}	1.590^{-2}	-4.597^{-3}
0.073	0.926	1.230^{-2}	1.503^{-2}	-2.598^{-4}	0.654	1.037	1.152^{-2}	1.632^{-2}	-4.907^{-3}
0.080	0.949	1.238^{-2}	1.529^{-2}	-4.009^{-4}	0.660	1.056	-3.886^{-3}	1.594^{-2}	-4.141^{-3}
0.086	0.944	1.953^{-2}	1.440^{-2}	-1.938^{-4}	0.674	1.049	6.020^{-3}	1.556^{-2}	-4.347^{-3}
0.103	0.946	1.316^{-2}	1.598^{-2}	-6.763^{-4}	0.686	1.062	-1.849^{-3}	1.561^{-2}	-4.237^{-3}
0.113	0.985	2.566^{-2}	1.511^{-2}	-3.462^{-4}	0.713	1.067	-2.164^{-3}	1.562^{-2}	-4.346^{-3}
0.123	0.974	2.652^{-2}	1.553^{-2}	4.486^{-5}	0.727	1.074	-8.258^{-3}	1.465^{-2}	-3.601^{-3}
0.133	0.977	2.314^{-2}	1.549^{-2}	-3.528^{-4}	0.740	1.079	-6.626^{-3}	1.548^{-2}	-3.927^{-3}
0.143	0.978	2.913^{-2}	1.542^{-2}	-3.525^{-4}	0.754	1.086	-7.216^{-3}	1.477^{-2}	-3.796^{-3}
0.153	0.986	2.456^{-2}	1.555^{-2}	-4.805^{-4}	0.766	1.098	-1.123^{-2}	1.299^{-2}	-2.730^{-3}
0.173	0.993	2.943^{-2}	1.616^{-2}	-9.837^{-4}	0.780	1.101	-6.482^{-3}	1.283^{-2}	-2.802^{-3}
0.183	0.991	2.932^{-2}	1.581^{-2}	-1.091^{-3}	0.807	1.096	-9.841^{-3}	1.290^{-2}	-2.843^{-3}
0.193	0.978	3.233^{-2}	1.703^{-2}	-3.259^{-4}	0.817	1.100	-1.474^{-2}	1.220^{-2}	-2.759^{-3}
0.220	0.992	2.830^{-2}	1.663^{-2}	-8.390^{-4}	0.827	1.116	-8.854^{-3}	1.153^{-2}	-1.830^{-3}
0.233	0.971	3.343^{-2}	1.739^{-2}	-1.168^{-3}	0.847	1.128	-5.147^{-3}	1.032^{-2}	-1.674^{-3}
0.246	0.976	2.952^{-2}	1.751^{-2}	-8.588^{-4}	0.877	1.124	-1.052^{-2}	1.028^{-2}	-1.036^{-3}
0.260	0.968	2.917^{-2}	1.756^{-2}	-2.448^{-3}	0.897	1.132	-1.400^{-2}	9.565^{-3}	-2.473^{-4}
0.286	0.974	3.640^{-2}	1.847^{-2}	-1.334^{-3}	0.914	1.131	-1.416^{-2}	8.828^{-3}	-3.776^{-5}
0.300	0.986	2.187^{-2}	1.877^{-2}	-2.375^{-3}	0.920	1.130	-1.261^{-2}	8.447^{-3}	3.145^{-5}
0.326	0.983	2.805^{-2}	1.805^{-2}	-2.087^{-3}	0.927	1.110	-1.362^{-2}	8.948^{-3}	1.009^{-4}
0.346	0.995	1.899^{-2}	1.789^{-2}	-2.918^{-3}	0.934	1.099	-1.585^{-2}	8.942^{-3}	4.222^{-4}
0.366	0.980	3.256^{-2}	1.941^{-2}	-2.917^{-3}	0.940	1.098	-1.351^{-2}	8.509^{-3}	5.076^{-4}
0.406	0.996	2.081^{-2}	1.856^{-2}	-2.754^{-3}	0.947	1.089	-1.614^{-2}	8.180^{-3}	8.494^{-4}
0.426	0.985	2.875^{-2}	1.836^{-2}	-3.183^{-3}	0.954	1.085	-1.594^{-2}	7.596^{-3}	8.506^{-4}
0.446	0.988	3.086^{-2}	1.898^{-2}	-3.660^{-3}	0.967	1.045	-1.533^{-2}	7.689^{-3}	1.052^{-3}
0.506	1.027	4.185^{-3}	1.860^{-2}	-4.749^{-3}	0.974	1.051	-7.426^{-3}	8.144^{-3}	1.595^{-3}

Table 20. Concluded ($x/H = 6$)

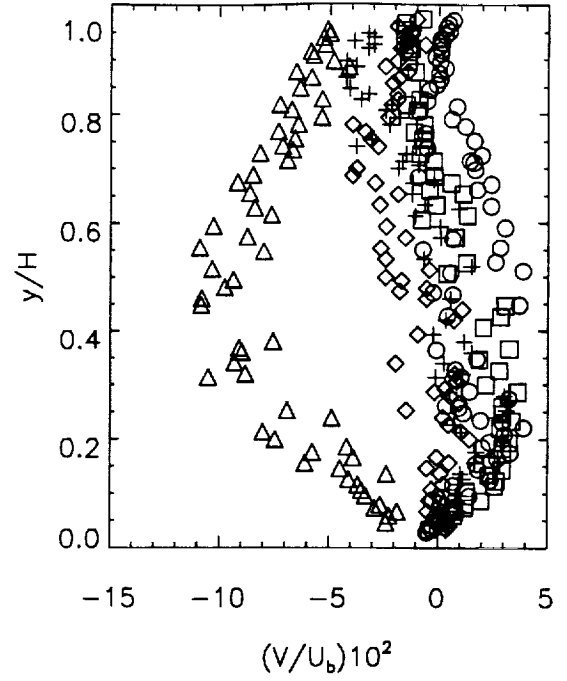
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.053	0.882	7.542^{-3}	1.269^{-2}	-1.921^{-3}	0.534	1.004	-6.331^{-3}	1.900^{-2}	-6.552^{-3}
0.060	0.901	6.747^{-4}	1.531^{-2}	-2.647^{-3}	0.573	1.026	1.175^{-3}	1.803^{-2}	-6.018^{-3}
0.066	0.887	9.201^{-3}	1.396^{-2}	-2.507^{-3}	0.594	1.013	9.388^{-4}	1.971^{-2}	-6.126^{-3}
0.080	0.934	3.359^{-3}	1.486^{-2}	-2.796^{-3}	0.614	1.025	-1.032^{-2}	1.765^{-2}	-5.938^{-3}
0.086	0.931	7.635^{-3}	1.558^{-2}	-2.768^{-3}	0.626	1.050	9.590^{-3}	1.913^{-2}	-5.993^{-3}
0.096	0.924	8.405^{-3}	1.498^{-2}	-2.883^{-3}	0.634	1.033	-6.020^{-3}	1.640^{-2}	-5.263^{-3}
0.106	0.947	4.998^{-3}	1.657^{-2}	-3.692^{-3}	0.653	1.070	-1.194^{-2}	1.735^{-2}	-4.687^{-3}
0.116	0.941	9.303^{-3}	1.588^{-2}	-3.533^{-3}	0.674	1.053	-1.153^{-2}	1.663^{-2}	-3.922^{-3}
0.126	0.950	1.131^{-2}	1.548^{-2}	-3.228^{-3}	0.680	1.081	-1.844^{-3}	1.851^{-2}	-5.468^{-3}
0.136	0.951	9.972^{-3}	1.630^{-2}	-3.959^{-3}	0.700	1.059	-1.828^{-2}	1.680^{-2}	-4.330^{-3}
0.156	0.973	1.666^{-2}	1.646^{-2}	-4.082^{-3}	0.706	1.085	-8.972^{-3}	1.849^{-2}	-5.582^{-3}
0.166	0.967	2.737^{-2}	1.598^{-2}	-4.061^{-3}	0.714	1.050	-1.622^{-2}	1.835^{-2}	-4.540^{-3}
0.176	0.961	1.727^{-2}	1.629^{-2}	-3.797^{-3}	0.727	1.050	-1.491^{-2}	1.807^{-2}	-4.626^{-3}
0.200	0.958	2.927^{-2}	1.700^{-2}	-4.401^{-3}	0.740	1.067	-3.756^{-2}	1.558^{-2}	-2.807^{-3}
0.213	0.968	1.051^{-2}	1.746^{-2}	-4.431^{-3}	0.754	1.090	-3.056^{-2}	1.433^{-2}	-2.518^{-3}
0.226	0.968	7.259^{-3}	1.666^{-2}	-4.750^{-3}	0.780	1.076	-2.244^{-2}	1.529^{-2}	-3.179^{-3}
0.240	0.974	2.574^{-2}	1.830^{-2}	-5.705^{-3}	0.794	1.083	-1.784^{-2}	1.713^{-2}	-2.553^{-3}
0.253	0.978	3.111^{-2}	1.788^{-2}	-3.911^{-3}	0.807	1.086	-2.423^{-2}	1.635^{-2}	-1.414^{-3}
0.266	0.973	3.161^{-2}	1.821^{-2}	-4.598^{-3}	0.817	1.087	-2.167^{-2}	1.556^{-2}	-1.197^{-3}
0.280	0.969	3.024^{-2}	1.862^{-2}	-5.187^{-3}	0.827	1.098	-3.563^{-2}	1.507^{-2}	-1.762^{-4}
0.287	0.959	5.282^{-3}	1.932^{-2}	-4.931^{-3}	0.837	1.096	-3.198^{-2}	1.428^{-2}	-4.564^{-4}
0.314	0.958	-9.855^{-4}	1.838^{-2}	-4.150^{-3}	0.847	1.096	-4.094^{-2}	1.477^{-2}	-8.415^{-5}
0.320	0.979	1.129^{-2}	1.894^{-2}	-5.966^{-3}	0.867	1.098	-4.245^{-2}	1.297^{-2}	1.372^{-3}
0.340	0.975	2.617^{-3}	1.930^{-2}	-5.108^{-3}	0.887	1.093	-3.801^{-2}	1.406^{-2}	1.340^{-3}
0.360	0.979	1.540^{-2}	1.978^{-2}	-5.879^{-3}	0.897	1.099	-4.223^{-2}	1.399^{-2}	3.247^{-3}
0.380	0.986	1.175^{-2}	1.922^{-2}	-6.076^{-3}	0.920	1.102	-3.234^{-2}	1.195^{-2}	2.347^{-3}
0.394	0.973	-2.358^{-3}	1.916^{-2}	-5.965^{-3}	0.927	1.087	-2.984^{-2}	1.213^{-2}	2.455^{-3}
0.420	0.985	3.748^{-3}	1.936^{-2}	-6.180^{-3}	0.934	1.081	-3.876^{-2}	1.344^{-2}	4.037^{-3}
0.460	1.013	5.631^{-3}	1.920^{-2}	-6.646^{-3}	0.940	1.085	-2.976^{-2}	1.271^{-2}	2.696^{-3}
0.520	1.023	1.519^{-2}	1.972^{-2}	-6.934^{-3}	0.947	1.082	-3.226^{-2}	1.311^{-2}	3.713^{-3}

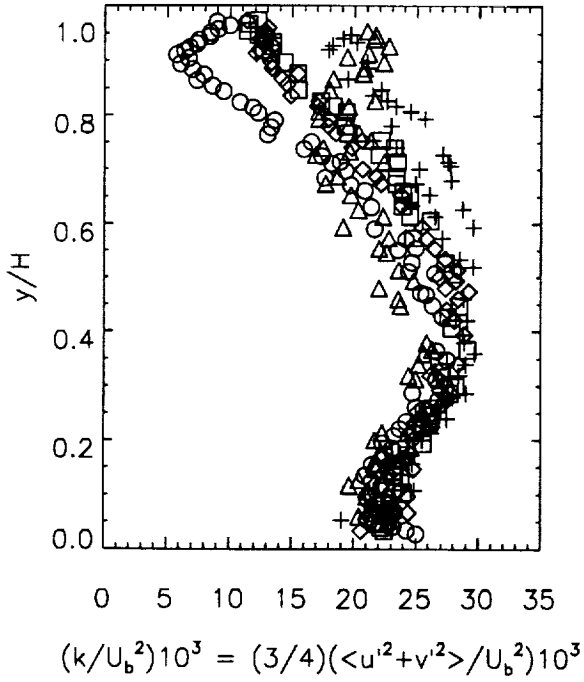
Legend: $Re=1 \times 10^5: z/H=0 (\odot)$; $Re=1 \times 10^6: z/H=0 (\diamond)$, $z/H=1 (\Delta)$, $z/H=2 (\square)$, $z/H=3 (+)$



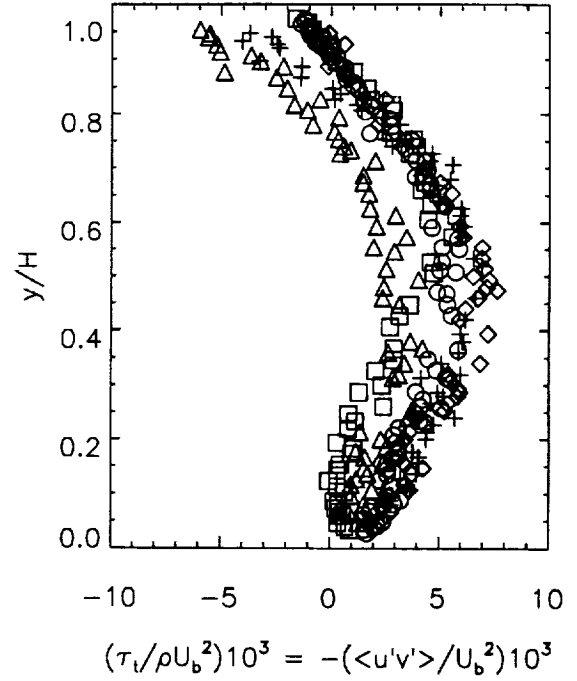
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 20. Summary of Table 20 ($x/H = 6$).

Table 21. LDV flowfield in TAD ($x/H = 8$)

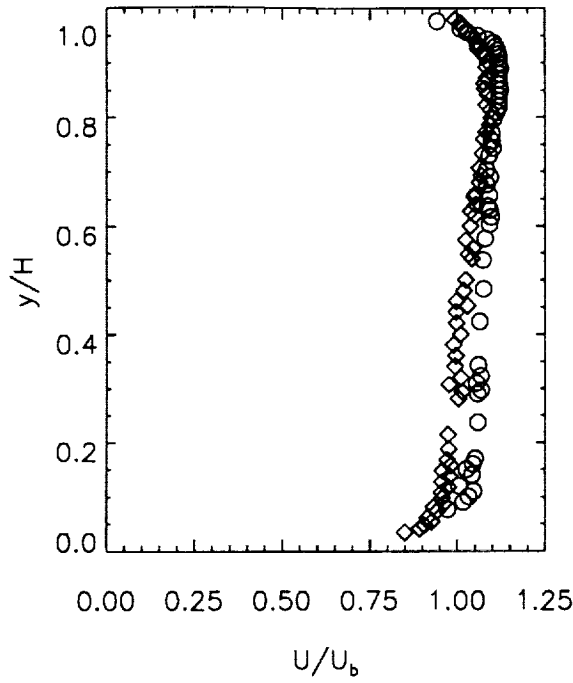
($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.077	0.972	6.552^{-4}	1.121^{-2}	-2.368^{-3}	0.703	1.083	1.927^{-2}	9.825^{-3}	-3.377^{-3}
0.090	1.016	2.769^{-3}	1.084^{-2}	-2.286^{-3}	0.730	1.091	1.004^{-2}	9.565^{-3}	-3.687^{-3}
0.100	1.032	-3.807^{-3}	1.045^{-2}	-2.223^{-3}	0.743	1.102	4.308^{-3}	8.482^{-3}	-2.945^{-3}
0.110	1.046	-2.319^{-4}	1.016^{-2}	-2.436^{-3}	0.757	1.098	1.504^{-2}	8.389^{-3}	-2.944^{-3}
0.120	1.004	1.643^{-2}	1.042^{-2}	-2.072^{-3}	0.770	1.099	9.708^{-3}	8.170^{-3}	-2.855^{-3}
0.140	1.041	1.012^{-3}	9.876^{-3}	-2.061^{-3}	0.797	1.104	6.144^{-3}	8.194^{-3}	-2.523^{-3}
0.150	1.026	1.182^{-2}	1.017^{-2}	-2.192^{-3}	0.810	1.112	1.646^{-3}	7.603^{-3}	-2.295^{-3}
0.160	1.044	1.549^{-2}	1.044^{-2}	-2.346^{-3}	0.820	1.120	2.005^{-3}	7.282^{-3}	-2.079^{-3}
0.170	1.051	1.198^{-2}	1.070^{-2}	-2.688^{-3}	0.830	1.118	4.270^{-3}	7.009^{-3}	-1.726^{-3}
0.237	1.059	3.291^{-2}	1.147^{-2}	-3.143^{-3}	0.840	1.120	-1.801^{-3}	6.608^{-3}	-1.492^{-3}
0.290	1.057	3.100^{-2}	1.189^{-2}	-3.891^{-3}	0.850	1.122	4.586^{-3}	6.553^{-3}	-1.499^{-3}
0.297	1.068	1.632^{-2}	1.152^{-2}	-3.084^{-3}	0.860	1.120	5.879^{-3}	6.418^{-3}	-1.546^{-3}
0.310	1.055	1.327^{-2}	1.130^{-2}	-3.176^{-3}	0.870	1.119	1.011^{-2}	6.444^{-3}	-1.168^{-3}
0.323	1.067	1.108^{-2}	1.160^{-2}	-2.961^{-3}	0.880	1.119	8.269^{-3}	6.245^{-3}	-1.199^{-3}
0.343	1.060	2.661^{-2}	1.206^{-2}	-3.453^{-3}	0.890	1.123	7.349^{-3}	5.835^{-3}	-9.084^{-4}
0.423	1.064	2.783^{-2}	1.280^{-2}	-3.925^{-3}	0.900	1.119	6.369^{-3}	5.983^{-3}	-7.785^{-4}
0.483	1.075	9.023^{-3}	1.141^{-2}	-3.952^{-3}	0.910	1.119	5.404^{-3}	5.707^{-3}	-4.804^{-4}
0.537	1.073	1.081^{-2}	1.217^{-2}	-4.518^{-3}	0.917	1.117	8.711^{-3}	5.563^{-3}	-5.185^{-4}
0.577	1.079	1.383^{-2}	1.116^{-2}	-4.002^{-3}	0.923	1.115	8.763^{-3}	5.304^{-3}	-3.260^{-4}
0.603	1.092	1.981^{-3}	1.048^{-2}	-3.273^{-3}	0.930	1.109	6.171^{-3}	4.876^{-3}	-1.717^{-5}
0.617	1.096	-9.425^{-4}	1.110^{-2}	-4.205^{-3}	0.937	1.104	7.959^{-3}	4.747^{-3}	2.318^{-4}
0.630	1.093	2.254^{-3}	1.014^{-2}	-3.113^{-3}	0.943	1.086	5.507^{-3}	5.068^{-3}	4.834^{-4}
0.637	1.087	1.025^{-2}	1.068^{-2}	-4.288^{-3}	0.950	1.058	5.602^{-3}	5.362^{-3}	8.075^{-4}
0.657	1.091	3.526^{-3}	1.029^{-2}	-3.524^{-3}	0.957	1.027	5.836^{-3}	5.361^{-3}	8.882^{-4}
0.677	1.084	1.359^{-2}	1.043^{-2}	-3.867^{-3}	0.963	1.008	6.514^{-3}	5.207^{-3}	1.043^{-3}
0.690	1.094	8.809^{-3}	1.006^{-2}	-4.129^{-3}	0.977	0.942	6.037^{-3}	5.474^{-3}	1.217^{-3}

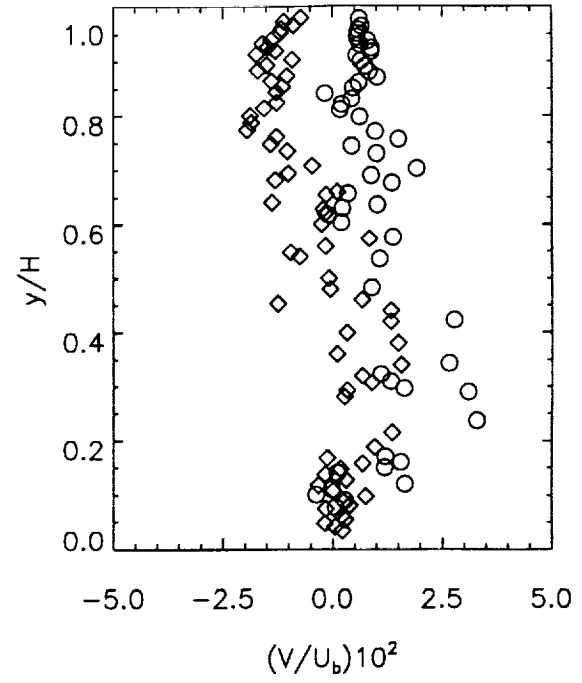
Table 21. Concluded ($x/H = 8$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.034	0.850	2.177^{-3}	9.278^{-3}	-1.877^{-3}	0.574	1.024	8.459^{-3}	1.229^{-2}	-4.014^{-3}
0.041	0.892	5.363^{-4}	9.986^{-3}	-1.598^{-3}	0.600	1.037	-2.504^{-3}	1.215^{-2}	-3.946^{-3}
0.047	0.906	-1.789^{-3}	9.568^{-3}	-1.528^{-3}	0.619	1.050	-1.735^{-3}	1.163^{-2}	-3.664^{-3}
0.054	0.926	2.877^{-3}	1.061^{-2}	-2.101^{-3}	0.627	1.038	-2.146^{-3}	1.180^{-2}	-3.328^{-3}
0.061	0.913	2.072^{-3}	9.925^{-3}	-1.885^{-3}	0.639	1.053	-1.382^{-2}	1.156^{-2}	-3.738^{-3}
0.074	0.943	-1.626^{-3}	9.847^{-3}	-2.077^{-3}	0.654	1.048	-1.482^{-3}	1.194^{-2}	-4.008^{-3}
0.081	0.932	3.826^{-3}	1.043^{-2}	-2.163^{-3}	0.659	1.051	1.038^{-3}	1.221^{-2}	-4.020^{-3}
0.087	0.962	2.418^{-3}	1.052^{-2}	-1.589^{-3}	0.680	1.064	-1.310^{-2}	1.150^{-2}	-3.344^{-3}
0.097	0.956	7.471^{-3}	1.006^{-2}	-1.755^{-3}	0.693	1.068	-1.013^{-2}	1.076^{-2}	-3.207^{-3}
0.107	0.954	9.982^{-5}	1.007^{-2}	-2.131^{-3}	0.707	1.063	-4.661^{-3}	1.139^{-2}	-3.625^{-3}
0.117	0.974	-3.253^{-3}	1.018^{-2}	-1.892^{-3}	0.733	1.072	-1.037^{-2}	1.090^{-2}	-2.814^{-3}
0.127	0.956	2.997^{-3}	9.695^{-3}	-2.018^{-3}	0.746	1.093	-1.413^{-2}	9.772^{-3}	-2.576^{-3}
0.137	0.977	-1.658^{-3}	1.084^{-2}	-2.526^{-3}	0.760	1.075	-1.281^{-2}	1.062^{-2}	-2.542^{-3}
0.147	0.957	1.752^{-3}	1.018^{-2}	-2.233^{-3}	0.773	1.082	-1.946^{-2}	9.749^{-3}	-1.974^{-3}
0.157	0.981	6.805^{-3}	1.022^{-2}	-2.069^{-3}	0.786	1.092	-1.856^{-2}	9.214^{-3}	-1.676^{-3}
0.167	0.971	-1.256^{-3}	1.044^{-2}	-2.660^{-3}	0.799	1.097	-1.880^{-2}	9.066^{-3}	-1.483^{-3}
0.187	0.975	9.558^{-3}	1.021^{-2}	-1.971^{-3}	0.813	1.094	-1.559^{-2}	8.992^{-3}	-1.570^{-3}
0.214	0.973	1.351^{-2}	1.021^{-2}	-2.111^{-3}	0.823	1.082	-1.274^{-2}	9.795^{-3}	-1.509^{-3}
0.281	1.003	2.747^{-3}	1.151^{-2}	-2.777^{-3}	0.843	1.085	-1.281^{-2}	9.253^{-3}	-1.357^{-3}
0.293	1.014	3.329^{-3}	1.227^{-2}	-3.021^{-3}	0.853	1.078	-1.146^{-2}	8.989^{-3}	-1.391^{-3}
0.307	0.976	9.006^{-3}	1.116^{-2}	-2.702^{-3}	0.863	1.077	-1.392^{-2}	9.243^{-3}	-7.952^{-4}
0.320	1.010	6.855^{-3}	1.231^{-2}	-3.480^{-3}	0.873	1.083	-1.040^{-2}	9.035^{-3}	-1.283^{-3}
0.341	0.993	1.570^{-2}	1.148^{-2}	-3.530^{-3}	0.883	1.096	-1.698^{-2}	7.282^{-3}	-2.814^{-4}
0.361	0.995	1.091^{-3}	1.131^{-2}	-3.773^{-3}	0.893	1.082	-1.498^{-2}	8.181^{-3}	-7.748^{-4}
0.381	0.989	1.502^{-2}	1.176^{-2}	-3.289^{-3}	0.903	1.086	-9.194^{-3}	7.969^{-3}	-7.347^{-4}
0.400	1.009	3.343^{-3}	1.204^{-2}	-3.538^{-3}	0.913	1.077	-1.729^{-2}	7.308^{-3}	3.134^{-5}
0.421	0.998	1.340^{-2}	1.200^{-2}	-3.724^{-3}	0.919	1.074	-1.297^{-2}	7.487^{-3}	-2.238^{-4}
0.441	0.997	1.341^{-2}	1.221^{-2}	-3.826^{-3}	0.926	1.058	-1.473^{-2}	8.533^{-3}	-3.514^{-4}
0.453	1.029	-1.245^{-2}	1.185^{-2}	-4.167^{-3}	0.933	1.058	-1.588^{-2}	7.560^{-3}	1.159^{-4}
0.461	0.997	6.831^{-3}	1.120^{-2}	-3.988^{-3}	0.939	1.054	-1.385^{-2}	7.186^{-3}	-1.855^{-4}
0.480	1.019	-4.804^{-4}	1.207^{-2}	-3.957^{-3}	0.953	1.040	-1.184^{-2}	6.786^{-3}	4.830^{-4}
0.500	1.023	-7.723^{-4}	1.203^{-2}	-4.114^{-3}	0.959	1.025	-1.154^{-2}	6.985^{-3}	4.551^{-4}
0.539	1.041	-7.478^{-3}	1.205^{-2}	-3.725^{-3}	0.966	1.015	-8.878^{-3}	6.830^{-3}	3.745^{-4}
0.547	1.032	-9.539^{-3}	1.160^{-2}	-3.919^{-3}	0.973	1.008	-1.103^{-2}	6.699^{-3}	4.903^{-4}
0.559	1.045	-1.605^{-3}	1.204^{-2}	-3.475^{-3}	0.979	0.992	-7.209^{-3}	6.104^{-3}	5.414^{-4}

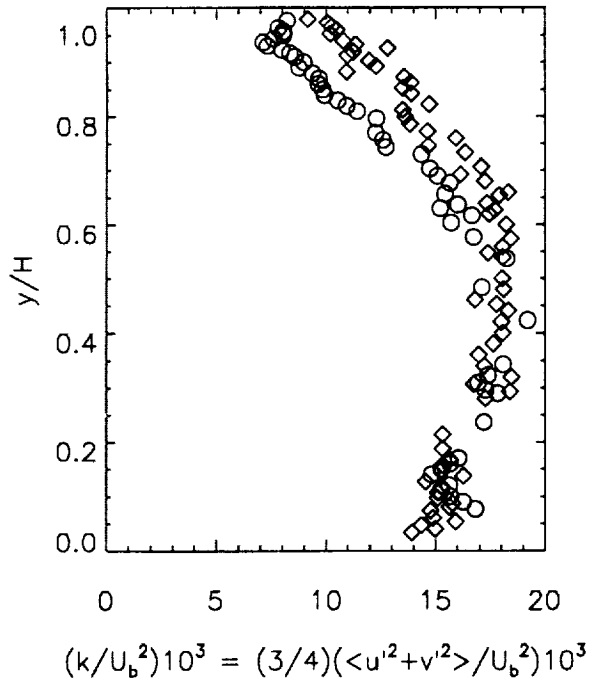
Legend: $Re = 1 \times 10^5$: $z/H = 0$ (\odot); $Re = 1 \times 10^6$: $z/H = 0$ (\diamond)



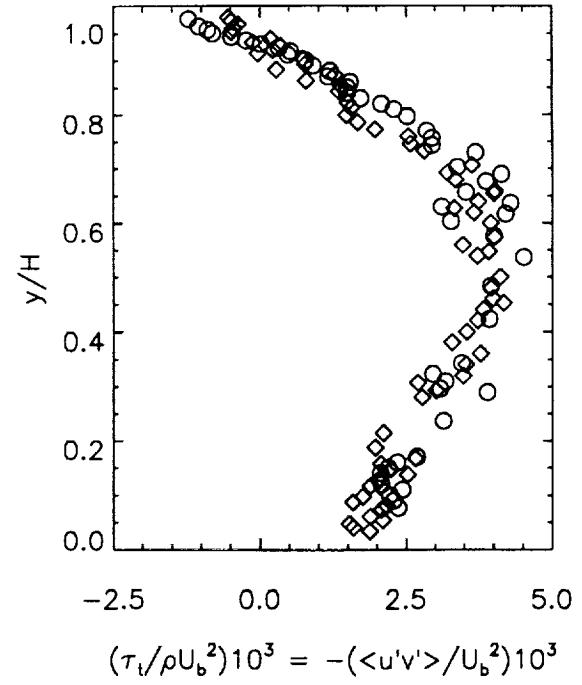
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



(d) Turbulent shear stress

Figure 21. Summary of Table 21 ($x/H = 8$).

Table 22. LDV flowfield data in TAD ($x/H = 10$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.039	0.827	6.625^{-3}	7.022^{-3}	-1.349^{-3}	0.637	1.081	2.985^{-3}	7.405^{-3}	-2.354^{-3}
0.053	0.881	5.510^{-3}	7.172^{-3}	-1.588^{-3}	0.658	1.075	-3.437^{-4}	6.628^{-3}	-1.986^{-3}
0.066	0.922	1.537^{-3}	7.275^{-3}	-1.523^{-3}	0.677	1.065	1.991^{-2}	7.609^{-3}	-2.426^{-3}
0.073	0.921	7.772^{-3}	7.683^{-3}	-1.659^{-3}	0.691	1.061	2.126^{-2}	6.989^{-3}	-2.103^{-3}
0.079	0.915	6.219^{-3}	7.253^{-3}	-1.858^{-3}	0.704	1.061	1.851^{-2}	6.667^{-3}	-2.142^{-3}
0.086	0.956	3.651^{-3}	7.853^{-3}	-1.849^{-3}	0.713	1.066	3.511^{-3}	5.998^{-3}	-1.761^{-3}
0.093	0.945	7.374^{-3}	7.592^{-3}	-2.144^{-3}	0.717	1.070	1.323^{-2}	6.737^{-3}	-1.836^{-3}
0.103	0.965	1.294^{-2}	7.394^{-3}	-1.861^{-3}	0.731	1.074	1.255^{-2}	6.820^{-3}	-2.085^{-3}
0.113	0.963	1.998^{-2}	7.861^{-3}	-1.937^{-3}	0.739	1.071	5.826^{-4}	5.992^{-3}	-1.453^{-3}
0.143	0.990	2.607^{-2}	7.217^{-3}	-1.676^{-3}	0.744	1.072	1.798^{-2}	6.559^{-3}	-1.905^{-3}
0.173	1.010	2.746^{-2}	7.018^{-3}	-1.901^{-3}	0.771	1.076	5.229^{-3}	6.035^{-3}	-1.538^{-3}
0.183	1.027	2.491^{-2}	7.809^{-3}	-1.998^{-3}	0.784	1.078	9.216^{-3}	5.605^{-3}	-1.301^{-3}
0.193	1.027	3.018^{-2}	7.592^{-3}	-2.190^{-3}	0.797	1.065	1.629^{-2}	5.638^{-3}	-1.265^{-3}
0.206	1.046	2.376^{-2}	7.378^{-3}	-2.181^{-3}	0.811	1.065	1.869^{-2}	5.784^{-3}	-1.678^{-3}
0.219	1.047	2.542^{-2}	7.980^{-3}	-2.280^{-3}	0.821	1.078	1.172^{-2}	5.407^{-3}	-1.091^{-3}
0.233	1.071	-1.915^{-3}	6.961^{-3}	-1.962^{-3}	0.831	1.076	1.752^{-2}	5.359^{-3}	-1.400^{-3}
0.237	1.065	2.579^{-2}	7.521^{-3}	-1.845^{-3}	0.841	1.068	1.920^{-2}	5.456^{-3}	-1.245^{-3}
0.246	1.056	8.955^{-3}	6.997^{-3}	-1.488^{-3}	0.851	1.069	2.200^{-2}	5.824^{-3}	-1.464^{-3}
0.259	1.060	1.435^{-2}	7.143^{-3}	-1.749^{-3}	0.861	1.064	1.591^{-2}	5.316^{-3}	-1.192^{-3}
0.291	1.080	1.307^{-2}	7.962^{-3}	-2.127^{-3}	0.871	1.079	1.206^{-2}	5.103^{-3}	-1.118^{-3}
0.299	1.043	1.856^{-2}	7.235^{-3}	-2.207^{-3}	0.881	1.093	7.108^{-3}	4.661^{-3}	-6.445^{-4}
0.313	1.051	1.523^{-2}	7.390^{-3}	-2.123^{-3}	0.891	1.093	6.110^{-3}	4.322^{-3}	-4.197^{-4}
0.345	1.073	1.495^{-2}	8.038^{-3}	-2.382^{-3}	0.901	1.088	6.828^{-3}	4.230^{-3}	-2.531^{-4}
0.366	1.050	1.993^{-2}	7.772^{-3}	-2.368^{-3}	0.911	1.078	4.764^{-3}	4.208^{-3}	-3.055^{-5}
0.406	1.055	8.264^{-3}	8.277^{-3}	-2.568^{-3}	0.917	1.070	6.965^{-4}	4.281^{-3}	4.925^{-4}
0.446	1.063	-1.636^{-3}	8.389^{-3}	-2.565^{-3}	0.924	1.064	3.159^{-3}	4.178^{-3}	3.829^{-4}
0.466	1.049	1.462^{-2}	7.922^{-3}	-2.430^{-3}	0.931	1.046	-2.085^{-4}	4.590^{-3}	7.632^{-4}
0.506	1.054	1.372^{-2}	7.676^{-3}	-2.368^{-3}	0.937	1.044	2.395^{-3}	4.239^{-3}	7.266^{-4}
0.526	1.058	-3.069^{-3}	7.721^{-3}	-2.632^{-3}	0.944	1.030	3.389^{-3}	4.508^{-3}	7.962^{-4}
0.553	1.062	4.158^{-3}	7.591^{-3}	-2.433^{-3}	0.951	1.014	3.240^{-3}	4.642^{-3}	8.339^{-4}
0.557	1.068	2.449^{-2}	8.422^{-3}	-2.350^{-3}	0.957	0.989	5.323^{-3}	4.819^{-3}	9.498^{-4}
0.597	1.081	4.648^{-3}	8.117^{-3}	-2.501^{-3}	0.964	0.986	6.739^{-3}	5.148^{-3}	1.174^{-3}
0.606	1.070	3.363^{-3}	7.347^{-3}	-2.383^{-3}	0.971	0.943	5.427^{-3}	4.603^{-3}	1.088^{-3}
0.617	1.078	1.031^{-2}	8.160^{-3}	-2.515^{-3}	0.977	0.914	5.751^{-3}	4.659^{-3}	1.246^{-3}
0.633	1.068	-2.231^{-3}	6.799^{-3}	-2.112^{-3}					

Table 22. Concluded ($x/H = 10$)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.062	0.950	4.960 ⁻³	7.774 ⁻³	-1.338 ⁻³	0.540	1.036	1.141 ⁻²	8.963 ⁻³	-2.518 ⁻³
0.075	0.960	5.955 ⁻³	7.712 ⁻³	-1.312 ⁻³	0.555	1.020	1.219 ⁻²	8.960 ⁻³	-2.579 ⁻³
0.089	0.962	4.406 ⁻³	7.588 ⁻³	-1.543 ⁻³	0.581	1.025	1.208 ⁻²	9.428 ⁻³	-2.581 ⁻³
0.095	0.971	6.377 ⁻³	7.511 ⁻³	-1.402 ⁻³	0.600	1.036	1.172 ⁻²	8.843 ⁻³	-2.364 ⁻³
0.105	0.972	6.490 ⁻³	7.573 ⁻³	-1.545 ⁻³	0.635	1.029	5.602 ⁻³	9.212 ⁻³	-2.367 ⁻³
0.115	0.972	1.279 ⁻²	7.795 ⁻³	-1.446 ⁻³	0.661	1.040	4.454 ⁻³	8.900 ⁻³	-2.330 ⁻³
0.135	0.988	1.031 ⁻²	8.124 ⁻³	-1.769 ⁻³	0.689	1.031	7.238 ⁻³	9.090 ⁻³	-2.568 ⁻³
0.145	0.971	1.024 ⁻²	7.555 ⁻³	-1.354 ⁻³	0.693	1.045	2.604 ⁻³	8.589 ⁻³	-2.396 ⁻³
0.155	0.999	1.184 ⁻²	7.723 ⁻³	-1.846 ⁻³	0.720	1.047	-4.172 ⁻³	9.392 ⁻³	-2.389 ⁻³
0.165	0.980	1.322 ⁻²	7.516 ⁻³	-1.431 ⁻³	0.733	1.046	2.413 ⁻³	8.872 ⁻³	-1.963 ⁻³
0.175	0.987	9.910 ⁻³	8.008 ⁻³	-1.590 ⁻³	0.742	1.040	2.723 ⁻³	8.535 ⁻³	-2.116 ⁻³
0.195	0.995	1.464 ⁻²	8.104 ⁻³	-1.420 ⁻³	0.747	1.061	-1.202 ⁻²	7.776 ⁻³	-1.622 ⁻³
0.209	0.990	1.206 ⁻²	7.916 ⁻³	-1.555 ⁻³	0.760	1.062	-4.838 ⁻³	7.636 ⁻³	-1.508 ⁻³
0.222	1.010	1.427 ⁻²	7.963 ⁻³	-1.400 ⁻³	0.773	1.055	-5.726 ⁻³	8.198 ⁻³	-1.806 ⁻³
0.235	1.013	1.250 ⁻²	8.780 ⁻³	-1.714 ⁻³	0.787	1.059	-1.147 ⁻²	8.019 ⁻³	-1.638 ⁻³
0.249	1.005	1.755 ⁻²	8.086 ⁻³	-1.574 ⁻³	0.800	1.062	-8.822 ⁻³	8.239 ⁻³	-1.483 ⁻³
0.262	1.017	1.681 ⁻²	8.449 ⁻³	-1.677 ⁻³	0.813	1.060	-1.229 ⁻²	7.438 ⁻³	-9.650 ⁻⁴
0.275	0.996	1.855 ⁻²	8.419 ⁻³	-1.823 ⁻³	0.823	1.067	-1.227 ⁻²	7.838 ⁻³	-1.115 ⁻³
0.289	1.009	2.611 ⁻²	8.828 ⁻³	-1.940 ⁻³	0.833	1.064	-9.752 ⁻³	7.405 ⁻³	-1.128 ⁻³
0.293	1.017	8.371 ⁻³	8.925 ⁻³	-2.140 ⁻³	0.843	1.063	-7.770 ⁻³	8.638 ⁻³	-1.261 ⁻³
0.302	1.002	2.160 ⁻²	8.281 ⁻³	-1.947 ⁻³	0.863	1.062	-8.388 ⁻³	7.185 ⁻³	-7.783 ⁻⁴
0.315	1.013	1.868 ⁻²	8.314 ⁻³	-1.947 ⁻³	0.873	1.048	-6.614 ⁻³	8.372 ⁻³	-9.347 ⁻⁴
0.348	1.015	1.861 ⁻²	9.264 ⁻³	-2.242 ⁻³	0.883	1.052	-7.445 ⁻³	8.156 ⁻³	-7.321 ⁻⁴
0.369	1.010	1.919 ⁻²	8.350 ⁻³	-1.929 ⁻³	0.893	1.057	-1.341 ⁻²	7.195 ⁻³	-8.156 ⁻⁵
0.373	1.022	2.051 ⁻²	9.507 ⁻³	-2.431 ⁻³	0.903	1.046	-1.587 ⁻²	7.789 ⁻³	4.075 ⁻⁴
0.389	1.006	1.644 ⁻²	8.345 ⁻³	-2.148 ⁻³	0.913	1.041	-1.555 ⁻²	8.040 ⁻³	4.455 ⁻⁴
0.400	1.016	1.411 ⁻²	9.541 ⁻³	-2.562 ⁻³	0.920	1.055	-1.677 ⁻²	7.208 ⁻³	4.563 ⁻⁴
0.409	1.010	2.372 ⁻²	8.766 ⁻³	-1.956 ⁻³	0.927	1.038	-1.293 ⁻²	7.670 ⁻³	3.112 ⁻⁴
0.428	1.016	2.301 ⁻²	9.130 ⁻³	-2.075 ⁻³	0.933	1.038	-1.380 ⁻²	7.437 ⁻³	7.840 ⁻⁴
0.449	1.024	8.187 ⁻³	8.443 ⁻³	-2.092 ⁻³	0.940	1.035	-1.559 ⁻²	7.877 ⁻³	7.270 ⁻⁴
0.453	1.021	2.042 ⁻²	9.343 ⁻³	-2.537 ⁻³	0.947	1.022	-1.820 ⁻²	7.668 ⁻³	1.219 ⁻³
0.469	1.014	2.293 ⁻²	8.744 ⁻³	-2.221 ⁻³	0.953	1.011	-1.843 ⁻²	7.726 ⁻³	1.351 ⁻³
0.480	1.033	1.007 ⁻²	9.874 ⁻³	-2.665 ⁻³	0.980	0.972	-1.572 ⁻²	7.365 ⁻³	1.901 ⁻³
0.500	1.019	1.502 ⁻²	9.651 ⁻³	-2.632 ⁻³					

Legend: $Re = 1 \times 10^5$: $z/H = 0(\odot)$; $Re = 1 \times 10^6$: $z/H = 0(\diamond)$

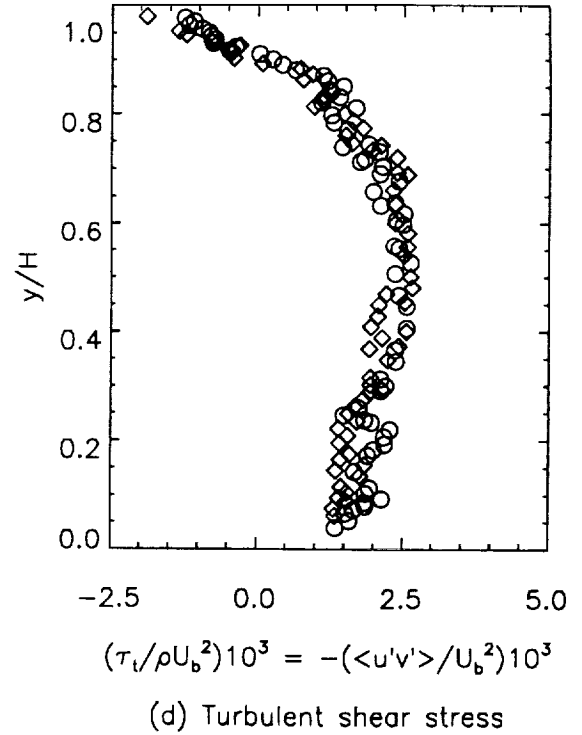
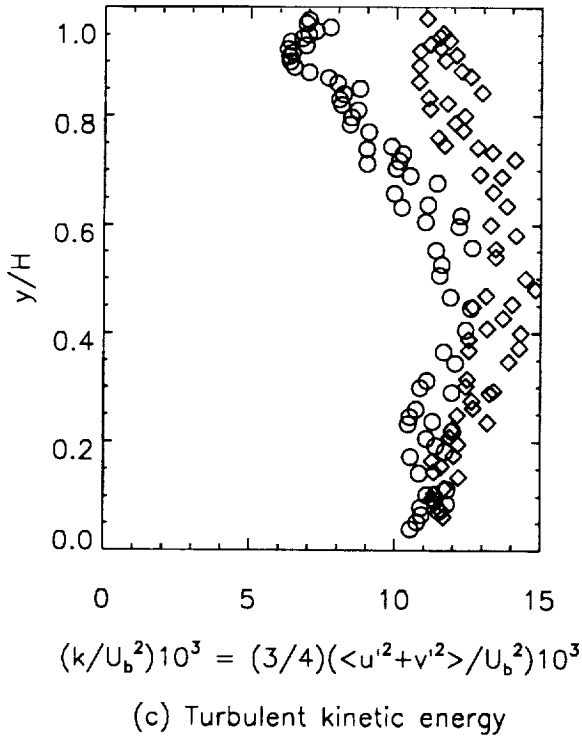
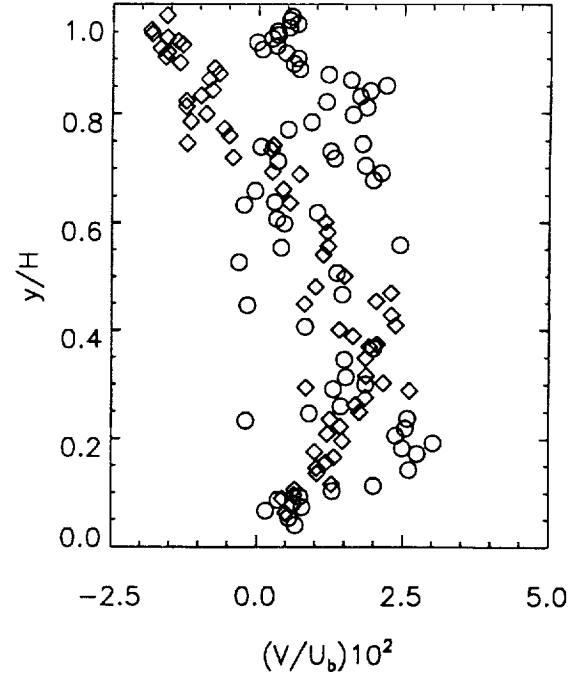
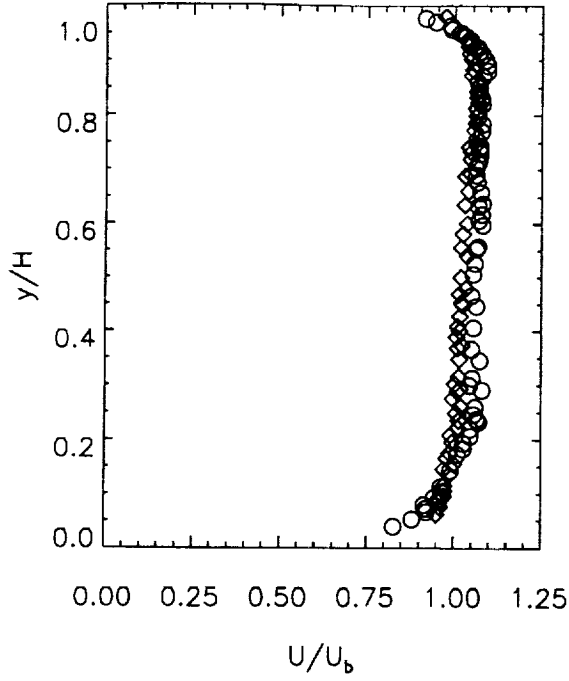


Figure 22. Summary of Table 22 ($x/H = 10$).

Table 23. LDV flowfield data in TAD ($x/H = 12$)

($Re = 1 \times 10^5$, $U_b = 30.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.029	0.835	-3.564 ⁻³	5.031 ⁻³	-5.029 ⁻⁴	0.557	1.048	-1.755 ⁻³	5.801 ⁻³	-1.121 ⁻³
0.042	0.881	-5.072 ⁻³	5.749 ⁻³	-4.647 ⁻⁴	0.577	1.048	-2.807 ⁻³	5.627 ⁻³	-8.004 ⁻⁴
0.049	0.922	-5.791 ⁻³	6.154 ⁻³	-7.088 ⁻⁴	0.582	1.028	2.122 ⁻²	4.737 ⁻³	-1.311 ⁻³
0.055	0.907	-3.171 ⁻³	5.697 ⁻³	-8.377 ⁻⁴	0.597	1.059	-9.436 ⁻³	5.279 ⁻³	-7.480 ⁻⁴
0.062	0.902	-1.479 ⁻³	5.048 ⁻³	-7.766 ⁻⁴	0.609	1.036	2.723 ⁻²	4.539 ⁻³	-1.057 ⁻³
0.075	0.909	3.741 ⁻⁴	4.696 ⁻³	-8.728 ⁻⁴	0.657	1.056	-6.538 ⁻⁴	5.343 ⁻³	-9.884 ⁻⁴
0.082	0.919	8.684 ⁻⁴	4.956 ⁻³	-8.800 ⁻⁴	0.662	1.037	2.666 ⁻²	4.364 ⁻³	-1.026 ⁻³
0.089	0.946	2.337 ⁻⁴	5.772 ⁻³	-9.929 ⁻⁴	0.677	1.060	-3.973 ⁻³	5.222 ⁻³	-4.560 ⁻⁴
0.095	0.962	4.629 ⁻⁴	5.626 ⁻³	-9.874 ⁻⁴	0.689	1.045	1.267 ⁻²	4.356 ⁻³	-8.472 ⁻⁴
0.105	0.950	2.522 ⁻³	5.092 ⁻³	-1.025 ⁻³	0.691	1.064	-9.373 ⁻³	5.154 ⁻³	-6.250 ⁻⁴
0.115	0.979	-2.852 ⁻³	5.321 ⁻³	-1.052 ⁻³	0.704	1.056	3.057 ⁻³	4.996 ⁻³	-6.780 ⁻⁴
0.125	0.970	2.183 ⁻³	4.965 ⁻³	-1.080 ⁻³	0.717	1.045	3.674 ⁻³	5.023 ⁻³	-7.831 ⁻⁴
0.135	0.988	3.667 ⁻⁴	5.308 ⁻³	-1.074 ⁻³	0.744	1.064	1.024 ⁻³	4.901 ⁻³	-7.098 ⁻⁴
0.145	0.982	4.007 ⁻³	5.081 ⁻³	-1.195 ⁻³	0.757	1.062	-9.009 ⁻³	4.517 ⁻³	-2.491 ⁻⁴
0.155	0.982	7.649 ⁻³	5.203 ⁻³	-1.210 ⁻³	0.771	1.063	-6.139 ⁻³	4.538 ⁻³	-1.754 ⁻⁴
0.165	0.983	1.837 ⁻²	4.690 ⁻³	-8.089 ⁻⁴	0.821	1.055	-7.355 ⁻³	5.644 ⁻³	4.875 ⁻⁴
0.175	0.989	5.637 ⁻³	5.181 ⁻³	-1.290 ⁻³	0.831	1.053	-1.277 ⁻²	5.305 ⁻³	9.014 ⁻⁴
0.185	0.992	1.741 ⁻²	4.822 ⁻³	-9.707 ⁻⁴	0.841	1.050	-8.459 ⁻³	5.318 ⁻³	6.632 ⁻⁴
0.195	0.985	2.154 ⁻²	4.504 ⁻³	-8.950 ⁻⁴	0.851	1.051	-1.092 ⁻²	5.467 ⁻³	1.011 ⁻³
0.209	1.015	4.706 ⁻⁴	4.695 ⁻³	-1.199 ⁻³	0.861	1.056	-4.177 ⁻³	5.400 ⁻³	5.968 ⁻⁴
0.222	0.996	2.606 ⁻²	4.455 ⁻³	-9.034 ⁻⁴	0.871	1.040	-8.891 ⁻³	5.558 ⁻³	1.201 ⁻³
0.249	1.012	3.130 ⁻²	4.575 ⁻³	-8.679 ⁻⁴	0.881	1.036	-7.919 ⁻³	5.450 ⁻³	1.111 ⁻³
0.262	1.000	2.964 ⁻²	4.648 ⁻³	-8.485 ⁻⁴	0.891	1.041	-4.656 ⁻³	5.542 ⁻³	1.092 ⁻³
0.275	1.000	2.857 ⁻²	4.593 ⁻³	-1.048 ⁻³	0.901	1.036	-4.527 ⁻³	5.172 ⁻³	8.722 ⁻⁴
0.289	1.009	1.989 ⁻²	4.568 ⁻³	-1.042 ⁻³	0.911	1.024	-3.340 ⁻³	5.318 ⁻³	1.148 ⁻³
0.302	1.012	2.637 ⁻²	4.632 ⁻³	-1.006 ⁻³	0.917	1.019	-7.020 ⁻³	5.698 ⁻³	1.500 ⁻³
0.349	1.022	2.258 ⁻²	4.793 ⁻³	-1.290 ⁻³	0.924	1.004	-4.791 ⁻³	5.136 ⁻³	1.241 ⁻³
0.371	1.047	-1.415 ⁻²	5.602 ⁻³	-1.220 ⁻³	0.931	1.010	-4.199 ⁻³	5.165 ⁻³	1.353 ⁻³
0.449	1.030	2.767 ⁻²	4.776 ⁻³	-1.094 ⁻³	0.937	0.980	-5.608 ⁻³	5.469 ⁻³	1.522 ⁻³
0.451	1.051	-1.136 ⁻²	5.805 ⁻³	-1.347 ⁻³	0.944	0.969	-7.118 ⁻³	6.115 ⁻³	1.921 ⁻³
0.469	1.025	2.152 ⁻²	4.668 ⁻³	-1.313 ⁻³	0.951	0.957	-6.001 ⁻³	5.956 ⁻³	1.782 ⁻³
0.509	1.028	3.047 ⁻²	4.788 ⁻³	-1.172 ⁻³	0.957	0.936	-7.487 ⁻³	6.662 ⁻³	2.158 ⁻³
0.529	1.030	2.895 ⁻²	5.004 ⁻³	-1.244 ⁻³	0.971	0.893	-7.690 ⁻³	6.689 ⁻³	2.344 ⁻³
0.555	1.032	2.482 ⁻²	4.799 ⁻³	-1.288 ⁻³					

Table 23. Continued ($x/H = 12$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 0$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.045	0.950	-6.521 ⁻³	6.003 ⁻³	-1.042 ⁻³	0.620	1.030	1.286 ⁻³	6.856 ⁻³	-1.801 ⁻³
0.051	0.930	-6.517 ⁻³	5.719 ⁻³	-9.937 ⁻⁴	0.638	1.036	3.875 ⁻³	6.616 ⁻³	-1.566 ⁻³
0.065	0.934	-4.848 ⁻⁵	5.796 ⁻³	-1.152 ⁻³	0.640	1.020	9.904 ⁻³	7.177 ⁻³	-1.825 ⁻³
0.078	0.975	-4.506 ⁻³	6.052 ⁻³	-1.082 ⁻³	0.660	1.030	1.672 ⁻³	6.672 ⁻³	-1.699 ⁻³
0.085	0.957	-2.564 ⁻³	5.890 ⁻³	-1.279 ⁻³	0.665	1.035	9.547 ⁻³	6.769 ⁻³	-1.446 ⁻³
0.091	0.971	-1.726 ⁻³	5.773 ⁻³	-1.190 ⁻³	0.680	1.030	2.733 ⁻³	6.715 ⁻³	-1.686 ⁻³
0.098	0.985	-5.488 ⁻⁴	5.734 ⁻³	-1.086 ⁻³	0.691	1.039	-5.275 ⁻³	6.386 ⁻³	-1.166 ⁻³
0.108	0.986	-2.577 ⁻³	5.767 ⁻³	-1.083 ⁻³	0.693	1.031	-2.894 ⁻³	6.524 ⁻³	-1.194 ⁻³
0.118	0.986	5.404 ⁻³	5.868 ⁻³	-1.189 ⁻³	0.707	1.028	4.887 ⁻³	6.994 ⁻³	-1.438 ⁻³
0.128	0.983	7.264 ⁻⁴	6.002 ⁻³	-1.249 ⁻³	0.720	1.041	-2.605 ⁻³	6.351 ⁻³	-1.304 ⁻³
0.138	1.004	-3.232 ⁻³	5.942 ⁻³	-1.216 ⁻³	0.733	1.033	2.251 ⁻³	6.366 ⁻³	-1.530 ⁻³
0.168	1.004	-2.497 ⁻³	5.708 ⁻³	-1.291 ⁻³	0.745	1.041	-5.543 ⁻³	6.448 ⁻³	-9.166 ⁻⁴
0.178	0.993	5.910 ⁻³	5.746 ⁻³	-1.243 ⁻³	0.747	1.029	1.608 ⁻³	6.665 ⁻³	-1.432 ⁻³
0.188	1.003	9.620 ⁻⁴	5.911 ⁻³	-1.160 ⁻³	0.760	1.035	-3.248 ⁻³	6.435 ⁻³	-9.822 ⁻⁴
0.198	1.006	-1.252 ⁻³	5.738 ⁻³	-1.213 ⁻³	0.773	1.033	1.415 ⁻³	6.276 ⁻³	-1.181 ⁻³
0.211	1.000	9.484 ⁻³	6.095 ⁻³	-1.187 ⁻³	0.787	1.027	6.559 ⁻³	6.252 ⁻³	-1.159 ⁻³
0.225	1.009	1.757 ⁻³	5.830 ⁻³	-1.265 ⁻³	0.800	1.021	2.508 ⁻³	6.264 ⁻³	-1.330 ⁻³
0.238	1.016	-4.365 ⁻⁵	6.265 ⁻³	-1.449 ⁻³	0.813	1.034	-1.093 ⁻³	5.892 ⁻³	-1.206 ⁻³
0.251	1.019	-5.883 ⁻³	5.857 ⁻³	-1.529 ⁻³	0.823	1.033	-3.505 ⁻³	5.679 ⁻³	-7.403 ⁻⁴
0.278	1.014	2.224 ⁻³	6.198 ⁻³	-1.227 ⁻³	0.833	1.028	-4.823 ⁻⁴	5.797 ⁻³	-9.078 ⁻⁴
0.305	1.019	1.014 ⁻²	6.327 ⁻³	-1.326 ⁻³	0.843	1.028	-1.608 ⁻⁴	5.662 ⁻³	-9.264 ⁻⁴
0.318	1.009	1.224 ⁻²	5.927 ⁻³	-1.155 ⁻³	0.853	1.021	1.061 ⁻³	5.825 ⁻³	-9.450 ⁻⁴
0.320	1.022	1.994 ⁻³	6.792 ⁻³	-1.660 ⁻³	0.863	1.026	-5.177 ⁻³	5.334 ⁻³	-3.484 ⁻⁴
0.331	1.023	2.452 ⁻³	6.199 ⁻³	-1.304 ⁻³	0.873	1.025	1.286 ⁻⁴	5.201 ⁻³	-6.296 ⁻⁴
0.347	1.018	7.042 ⁻³	7.084 ⁻³	-1.853 ⁻³	0.883	1.022	-3.441 ⁻³	4.886 ⁻³	-4.198 ⁻⁴
0.411	1.029	-6.349 ⁻³	6.296 ⁻³	-1.654 ⁻³	0.893	1.010	-3.344 ⁻³	5.190 ⁻³	-2.254 ⁻⁴
0.451	1.026	-9.843 ⁻⁴	6.271 ⁻³	-1.497 ⁻³	0.903	1.006	-5.723 ⁻³	5.440 ⁻³	1.654 ⁻⁵
0.480	1.025	8.039 ⁻³	7.176 ⁻³	-1.702 ⁻³	0.913	1.011	-3.569 ⁻³	4.920 ⁻³	-6.307 ⁻⁵
0.491	1.032	-2.915 ⁻³	6.655 ⁻³	-1.734 ⁻³	0.920	1.008	-5.402 ⁻³	4.842 ⁻³	1.634 ⁻⁴
0.511	1.020	5.228 ⁻³	6.760 ⁻³	-1.497 ⁻³	0.927	1.001	2.251 ⁻⁴	4.876 ⁻³	8.375 ⁻⁵
0.520	1.024	8.264 ⁻³	7.344 ⁻³	-1.837 ⁻³	0.933	0.997	-1.897 ⁻³	5.155 ⁻³	8.995 ⁻⁵
0.531	1.033	-3.590 ⁻³	6.786 ⁻³	-1.372 ⁻³	0.940	0.992	-4.277 ⁻³	4.816 ⁻³	1.696 ⁻⁴
0.558	1.034	1.678 ⁻³	6.801 ⁻³	-1.493 ⁻³	0.947	0.992	-5.434 ⁻³	4.665 ⁻³	5.728 ⁻⁴
0.585	1.032	-2.358 ⁻³	7.215 ⁻³	-1.594 ⁻³	0.953	0.977	-4.019 ⁻³	4.714 ⁻³	5.045 ⁻⁴
0.600	1.023	9.293 ⁻³	7.143 ⁻³	-1.850 ⁻³	0.960	0.968	-4.502 ⁻³	4.796 ⁻³	5.728 ⁻⁴
0.611	1.032	1.514 ⁻⁴	6.311 ⁻³	-1.562 ⁻³					

Table 23. Continued ($x/H = 12$)(Re = 1×10^6 , $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 1$)

y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.051	1.039	-9.149 ⁻³	5.662 ⁻³	-6.637 ⁻⁴	0.611	1.073	-3.158 ⁻²	6.585 ⁻³	-2.084 ⁻⁴
0.058	1.045	-1.025 ⁻²	5.409 ⁻³	-5.793 ⁻⁴	0.638	1.065	-3.890 ⁻²	6.058 ⁻³	-3.054 ⁻⁴
0.065	1.049	-5.799 ⁻³	5.862 ⁻³	-8.993 ⁻⁴	0.640	1.070	-3.548 ⁻²	6.161 ⁻³	-3.532 ⁻⁴
0.098	1.075	-7.879 ⁻³	5.278 ⁻³	-5.974 ⁻⁴	0.660	1.068	-3.695 ⁻²	6.341 ⁻³	-1.072 ⁻⁴
0.108	1.073	-1.043 ⁻²	5.654 ⁻³	-4.635 ⁻⁴	0.665	1.065	-3.783 ⁻²	6.293 ⁻³	1.438 ⁻⁵
0.118	1.082	-1.361 ⁻²	4.867 ⁻³	-3.972 ⁻⁴	0.691	1.072	-3.826 ⁻²	6.087 ⁻³	3.087 ⁻⁴
0.128	1.099	-1.576 ⁻²	4.970 ⁻³	-3.677 ⁻⁴	0.693	1.067	-4.043 ⁻²	6.377 ⁻³	4.515 ⁻⁴
0.138	1.088	-1.248 ⁻²	5.281 ⁻³	-4.234 ⁻⁴	0.707	1.053	-3.485 ⁻²	6.826 ⁻³	1.693 ⁻⁴
0.148	1.089	-1.307 ⁻²	5.146 ⁻³	-3.952 ⁻⁴	0.720	1.062	-3.855 ⁻²	6.000 ⁻³	2.183 ⁻⁴
0.158	1.101	-2.389 ⁻²	5.194 ⁻³	-4.133 ⁻⁴	0.733	1.057	-3.636 ⁻²	6.457 ⁻³	4.755 ⁻⁴
0.168	1.086	-1.802 ⁻²	5.640 ⁻³	-6.664 ⁻⁴	0.745	1.058	-3.277 ⁻²	7.124 ⁻³	2.873 ⁻⁴
0.178	1.094	-2.537 ⁻²	5.187 ⁻³	-3.819 ⁻⁴	0.760	1.049	-3.141 ⁻²	7.456 ⁻³	6.283 ⁻⁴
0.188	1.088	-1.792 ⁻²	5.308 ⁻³	-5.477 ⁻⁴	0.773	1.051	-2.743 ⁻²	7.073 ⁻³	8.861 ⁻⁴
0.198	1.085	-1.657 ⁻²	5.749 ⁻³	-6.710 ⁻⁴	0.787	1.053	-3.338 ⁻²	7.026 ⁻³	1.051 ⁻³
0.211	1.098	-2.258 ⁻²	5.512 ⁻³	-3.543 ⁻⁴	0.800	1.035	-3.784 ⁻²	7.774 ⁻³	1.704 ⁻³
0.225	1.094	-2.522 ⁻²	5.568 ⁻³	-4.332 ⁻⁴	0.813	1.038	-3.898 ⁻²	7.029 ⁻³	1.539 ⁻³
0.238	1.087	-1.885 ⁻²	6.010 ⁻³	-7.250 ⁻⁴	0.823	1.041	-3.468 ⁻²	7.534 ⁻³	1.933 ⁻³
0.251	1.089	-2.585 ⁻²	5.550 ⁻³	-3.231 ⁻⁴	0.833	1.037	-3.535 ⁻²	7.780 ⁻³	2.134 ⁻³
0.265	1.095	-3.328 ⁻²	5.451 ⁻³	-2.097 ⁻⁴	0.843	1.037	-3.205 ⁻²	6.964 ⁻³	1.498 ⁻³
0.291	1.092	-2.912 ⁻²	5.394 ⁻³	-3.073 ⁻⁴	0.853	1.035	-3.468 ⁻²	7.645 ⁻³	2.466 ⁻³
0.305	1.086	-3.056 ⁻²	5.652 ⁻³	-3.408 ⁻⁴	0.883	1.026	-2.867 ⁻²	7.360 ⁻³	2.233 ⁻³
0.318	1.089	-3.125 ⁻²	5.693 ⁻³	-3.492 ⁻⁴	0.893	1.017	-2.656 ⁻²	7.315 ⁻³	2.343 ⁻³
0.331	1.088	-2.724 ⁻²	5.863 ⁻³	-5.422 ⁻⁴	0.903	1.017	-2.758 ⁻²	7.955 ⁻³	2.703 ⁻³
0.351	1.084	-3.081 ⁻²	6.051 ⁻³	-5.693 ⁻⁴	0.913	1.005	-2.682 ⁻²	6.951 ⁻³	2.206 ⁻³
0.371	1.082	-2.954 ⁻²	5.918 ⁻³	-6.592 ⁻⁴	0.920	0.998	-2.945 ⁻²	6.964 ⁻³	2.348 ⁻³
0.411	1.076	-2.761 ⁻²	6.170 ⁻³	-5.078 ⁻⁴	0.927	1.000	-2.777 ⁻²	7.559 ⁻³	2.523 ⁻³
0.471	1.075	-3.395 ⁻²	5.935 ⁻³	-4.816 ⁻⁴	0.933	0.982	-2.842 ⁻²	8.118 ⁻³	3.046 ⁻³
0.491	1.082	-3.627 ⁻²	5.904 ⁻³	-5.890 ⁻⁴	0.940	0.983	-2.497 ⁻²	7.602 ⁻³	2.633 ⁻³
0.511	1.070	-2.961 ⁻²	6.029 ⁻³	-3.978 ⁻⁴	0.947	0.971	-2.758 ⁻²	8.037 ⁻³	2.892 ⁻³
0.531	1.081	-3.965 ⁻²	5.997 ⁻³	-5.122 ⁻⁴	0.953	0.972	-2.381 ⁻²	7.562 ⁻³	2.612 ⁻³
0.560	1.077	-4.010 ⁻²	6.698 ⁻³	-3.354 ⁻⁴	0.960	0.960	-2.310 ⁻²	7.901 ⁻³	2.997 ⁻³
0.585	1.076	-3.429 ⁻²	6.502 ⁻³	-3.394 ⁻⁴					

Table 23. Continued ($x/H = 12$)

($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 2$)

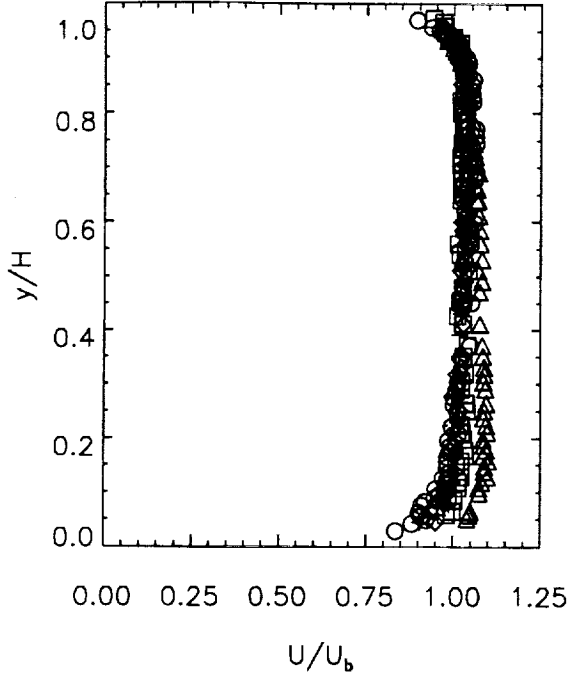
y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	y/H	U/U_b	V/U_b	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.058	0.981	-4.411 ⁻⁵	5.813 ⁻³	-1.119 ⁻³	0.660	1.021	3.792 ⁻³	6.743 ⁻³	-1.103 ⁻³
0.065	0.998	-1.067 ⁻³	6.323 ⁻³	-1.113 ⁻³	0.665	1.029	-3.328 ⁻³	6.317 ⁻³	-1.066 ⁻³
0.085	1.003	2.946 ⁻³	5.696 ⁻³	-9.317 ⁻⁴	0.680	1.021	3.513 ⁻³	7.679 ⁻³	-9.175 ⁻⁴
0.091	0.986	1.033 ⁻²	5.906 ⁻³	-1.108 ⁻³	0.693	1.023	3.717 ⁻³	6.899 ⁻³	-1.190 ⁻³
0.108	1.014	4.162 ⁻³	6.205 ⁻³	-8.452 ⁻⁴	0.707	1.019	8.017 ⁻³	6.784 ⁻³	-1.015 ⁻³
0.118	1.014	3.748 ⁻³	5.677 ⁻³	-1.003 ⁻³	0.718	1.041	-3.915 ⁻³	5.926 ⁻³	-9.806 ⁻⁴
0.128	1.022	4.639 ⁻³	5.715 ⁻³	-9.990 ⁻⁴	0.720	1.020	5.281 ⁻³	7.792 ⁻³	-1.043 ⁻³
0.148	1.010	1.318 ⁻²	6.400 ⁻³	-9.303 ⁻⁴	0.733	1.028	1.257 ⁻³	6.657 ⁻³	-1.043 ⁻³
0.158	1.023	1.128 ⁻²	5.741 ⁻³	-9.651 ⁻⁴	0.745	1.033	-3.369 ⁻³	6.047 ⁻³	-9.874 ⁻⁴
0.168	1.035	8.182 ⁻³	5.653 ⁻³	-7.237 ⁻⁴	0.747	1.022	3.658 ⁻³	7.369 ⁻³	-9.988 ⁻⁴
0.178	1.033	7.860 ⁻³	5.907 ⁻³	-9.352 ⁻⁴	0.760	1.026	3.037 ⁻³	7.164 ⁻³	-9.066 ⁻⁴
0.198	1.029	5.836 ⁻³	6.052 ⁻³	-7.711 ⁻⁴	0.771	1.033	-2.461 ⁻³	5.959 ⁻³	-7.946 ⁻⁴
0.211	1.025	8.296 ⁻³	5.916 ⁻³	-7.644 ⁻⁴	0.773	1.026	2.641 ⁻³	6.966 ⁻³	-8.386 ⁻⁴
0.225	1.021	1.360 ⁻²	6.032 ⁻³	-7.824 ⁻⁴	0.787	1.028	2.604 ⁻³	6.875 ⁻³	-8.475 ⁻⁴
0.251	1.039	3.276 ⁻³	6.195 ⁻³	-9.731 ⁻⁴	0.800	1.021	3.540 ⁻³	6.789 ⁻³	-9.255 ⁻⁴
0.265	1.036	1.122 ⁻²	6.119 ⁻³	-7.693 ⁻⁴	0.813	1.024	2.166 ⁻³	6.620 ⁻³	-6.504 ⁻⁴
0.291	1.023	1.453 ⁻²	6.530 ⁻³	-1.032 ⁻³	0.823	1.019	2.010 ⁻³	5.950 ⁻³	-7.712 ⁻⁴
0.305	1.023	1.322 ⁻²	6.729 ⁻³	-1.112 ⁻³	0.833	1.030	-8.432 ⁻⁴	5.794 ⁻³	-6.719 ⁻⁴
0.318	1.034	8.849 ⁻³	6.832 ⁻³	-8.538 ⁻⁴	0.843	1.028	-3.827 ⁻³	5.852 ⁻³	-3.024 ⁻⁴
0.351	1.029	1.500 ⁻²	6.248 ⁻³	-8.681 ⁻⁴	0.863	1.029	-2.664 ⁻³	5.155 ⁻³	-5.120 ⁻⁴
0.371	1.040	9.795 ⁻³	6.611 ⁻³	-8.728 ⁻⁴	0.873	1.032	-2.094 ⁻³	5.309 ⁻³	-2.644 ⁻⁴
0.411	1.027	1.471 ⁻²	6.560 ⁻³	-1.114 ⁻³	0.883	1.025	-3.119 ⁻³	5.232 ⁻³	-2.232 ⁻⁴
0.427	1.012	1.549 ⁻²	7.689 ⁻³	-1.135 ⁻³	0.893	1.023	-3.391 ⁻³	5.569 ⁻³	1.737 ⁻⁵
0.451	1.025	9.378 ⁻³	6.242 ⁻³	-9.184 ⁻⁴	0.903	1.020	-4.103 ⁻³	5.721 ⁻³	6.129 ⁻⁵
0.453	1.020	2.639 ⁻³	7.616 ⁻³	-1.103 ⁻³	0.913	1.017	-3.435 ⁻³	4.982 ⁻³	1.679 ⁻⁴
0.471	1.026	3.205 ⁻³	6.476 ⁻³	-1.027 ⁻³	0.920	1.010	-1.760 ⁻³	5.483 ⁻³	2.094 ⁻⁴
0.480	1.026	3.738 ⁻³	7.792 ⁻³	-8.429 ⁻⁴	0.927	1.018	-2.521 ⁻³	4.896 ⁻³	2.905 ⁻⁴
0.511	1.042	-5.668 ⁻³	6.616 ⁻³	-9.889 ⁻⁴	0.933	0.993	-3.924 ⁻³	6.138 ⁻³	6.908 ⁻⁴
0.540	1.019	7.135 ⁻³	7.770 ⁻³	-1.029 ⁻³	0.940	0.999	-4.631 ⁻³	5.146 ⁻³	4.753 ⁻⁴
0.560	1.013	1.366 ⁻²	7.182 ⁻³	-1.095 ⁻³	0.960	0.974	-3.202 ⁻³	5.467 ⁻³	1.010 ⁻³
0.585	1.039	3.091 ⁻³	6.255 ⁻³	-8.693 ⁻⁴	0.967	0.968	-4.058 ⁻³	4.739 ⁻³	6.178 ⁻⁴
0.611	1.034	-1.675 ⁻³	6.383 ⁻³	-7.908 ⁻⁴	0.973	0.941	-4.526 ⁻³	4.750 ⁻³	9.041 ⁻⁴
0.640	1.021	8.022 ⁻³	7.812 ⁻³	-8.657 ⁻⁴					

Table 23. Concluded ($x/H = 12$)

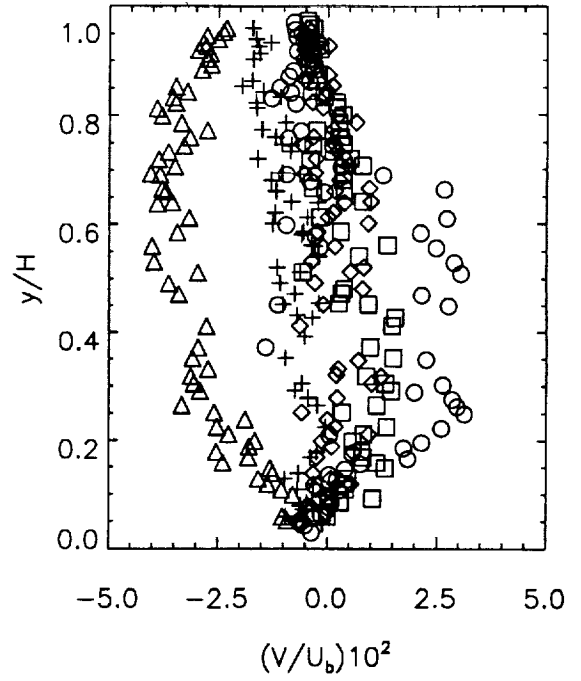
($Re = 1 \times 10^6$, $U_b = 31.1$ m/s, $H = 3.81$ cm, $z/H = 3$)

$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$	$\frac{y}{H}$	$\frac{U}{U_b}$	$\frac{V}{U_b}$	$\frac{\langle u'^2 + v'^2 \rangle}{2U_b^2}$	$\frac{\langle u'v' \rangle}{U_b^2}$
0.045	0.904	-1.036 ⁻³	6.436 ⁻³	-1.036 ⁻³	0.580	1.036	-5.952 ⁻³	7.121 ⁻³	-1.423 ⁻³
0.058	0.957	-9.499 ⁻³	6.485 ⁻³	-6.321 ⁻⁴	0.585	1.023	-5.488 ⁻³	6.884 ⁻³	-1.589 ⁻³
0.071	0.957	-5.514 ⁻³	6.597 ⁻³	-1.039 ⁻³	0.600	1.043	-1.247 ⁻²	6.603 ⁻³	-1.327 ⁻³
0.078	0.988	-6.153 ⁻³	5.757 ⁻³	-9.514 ⁻⁴	0.611	1.033	-4.634 ⁻³	6.580 ⁻³	-1.513 ⁻³
0.085	0.974	-4.596 ⁻³	5.706 ⁻³	-8.250 ⁻⁴	0.620	1.042	-1.191 ⁻²	6.649 ⁻³	-1.479 ⁻³
0.091	0.959	1.376 ⁻³	5.700 ⁻³	-1.066 ⁻³	0.638	1.025	-2.194 ⁻³	6.685 ⁻³	-1.188 ⁻³
0.098	0.983	-1.561 ⁻³	5.913 ⁻³	-1.268 ⁻³	0.640	1.039	-8.234 ⁻³	6.839 ⁻³	-1.624 ⁻³
0.108	0.975	-6.778 ⁻³	5.851 ⁻³	-9.160 ⁻⁴	0.660	1.037	-1.174 ⁻²	6.526 ⁻³	-1.096 ⁻³
0.118	0.997	-3.151 ⁻³	5.855 ⁻³	-9.538 ⁻⁴	0.680	1.040	-1.284 ⁻²	7.028 ⁻³	-1.255 ⁻³
0.128	0.992	-9.748 ⁻³	5.944 ⁻³	-1.209 ⁻³	0.691	1.029	-6.416 ⁻³	6.740 ⁻³	-1.164 ⁻³
0.138	0.994	-6.605 ⁻³	5.811 ⁻³	-1.197 ⁻³	0.693	1.040	-1.040 ⁻²	6.518 ⁻³	-1.006 ⁻³
0.168	1.006	-3.914 ⁻³	5.853 ⁻³	-1.003 ⁻³	0.720	1.048	-1.596 ⁻²	6.401 ⁻³	-9.050 ⁻⁴
0.178	1.006	-2.473 ⁻³	5.857 ⁻³	-9.035 ⁻⁴	0.733	1.037	-8.411 ⁻³	7.154 ⁻³	-1.079 ⁻³
0.225	0.992	-3.984 ⁻⁴	6.045 ⁻³	-1.329 ⁻³	0.745	1.033	-8.328 ⁻³	7.081 ⁻³	-1.270 ⁻³
0.265	1.008	-2.362 ⁻³	6.389 ⁻³	-1.319 ⁻³	0.747	1.045	-1.044 ⁻²	6.355 ⁻³	-8.547 ⁻⁴
0.278	0.997	-4.422 ⁻³	6.294 ⁻³	-1.381 ⁻³	0.760	1.043	-1.186 ⁻²	6.858 ⁻³	-6.604 ⁻⁴
0.291	1.008	-7.396 ⁻³	6.401 ⁻³	-1.359 ⁻³	0.773	1.043	-1.494 ⁻²	6.661 ⁻³	-6.228 ⁻⁴
0.305	1.010	-5.855 ⁻³	5.924 ⁻³	-1.224 ⁻³	0.787	1.035	-9.636 ⁻³	6.693 ⁻³	-6.383 ⁻⁴
0.351	1.015	-9.566 ⁻³	6.651 ⁻³	-1.524 ⁻³	0.813	1.044	-1.616 ⁻²	6.407 ⁻³	-1.970 ⁻⁴
0.391	1.018	-5.197 ⁻³	6.535 ⁻³	-1.303 ⁻³	0.823	1.048	-1.637 ⁻²	6.416 ⁻³	1.013 ⁻⁴
0.427	1.025	-3.438 ⁻³	7.201 ⁻³	-1.728 ⁻³	0.833	1.047	-1.081 ⁻²	6.657 ⁻³	-1.476 ⁻⁴
0.431	1.021	-7.005 ⁻³	6.579 ⁻³	-1.311 ⁻³	0.843	1.042	-1.467 ⁻²	6.264 ⁻³	-2.863 ⁻⁵
0.451	1.017	-1.014 ⁻²	6.632 ⁻³	-1.574 ⁻³	0.853	1.045	-1.956 ⁻²	6.269 ⁻³	3.993 ⁻⁴
0.453	1.022	-1.944 ⁻³	7.073 ⁻³	-1.211 ⁻³	0.863	1.034	-1.718 ⁻²	6.500 ⁻³	6.074 ⁻⁴
0.471	1.020	-7.479 ⁻³	6.465 ⁻³	-1.480 ⁻³	0.903	1.023	-1.698 ⁻²	6.485 ⁻³	1.293 ⁻³
0.491	1.023	-1.085 ⁻²	6.786 ⁻³	-1.740 ⁻³	0.913	1.013	-1.550 ⁻²	6.698 ⁻³	1.161 ⁻³
0.511	1.028	-6.239 ⁻³	6.302 ⁻³	-1.292 ⁻³	0.927	1.013	-1.577 ⁻²	6.549 ⁻³	1.636 ⁻³
0.520	1.034	-1.145 ⁻²	6.924 ⁻³	-1.662 ⁻³	0.933	1.007	-1.294 ⁻²	6.793 ⁻³	1.542 ⁻³
0.540	1.030	-2.055 ⁻³	7.006 ⁻³	-1.621 ⁻³	0.940	0.999	-1.629 ⁻²	6.235 ⁻³	1.210 ⁻³
0.558	1.023	-2.855 ⁻³	6.659 ⁻³	-1.357 ⁻³	0.960	0.968	-1.712 ⁻²	6.628 ⁻³	1.833 ⁻³
0.560	1.033	-3.602 ⁻³	6.952 ⁻³	-1.401 ⁻³					

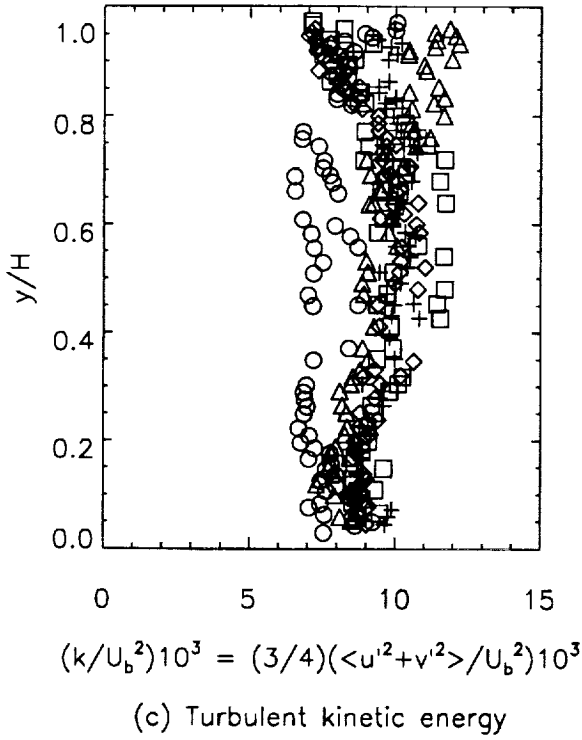
Legend: $Re=1 \times 10^5: z/H=0(\odot)$; $Re=1 \times 10^6: z/H=0(\diamond), z/H=1(\Delta), z/H=2(\square), z/H=3(+)$



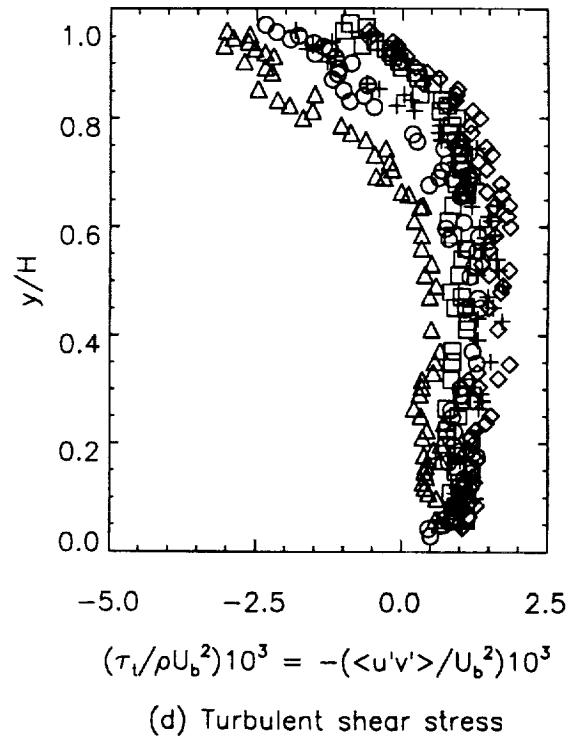
(a) Longitudinal mean velocity



(b) Vertical mean velocity



(c) Turbulent kinetic energy



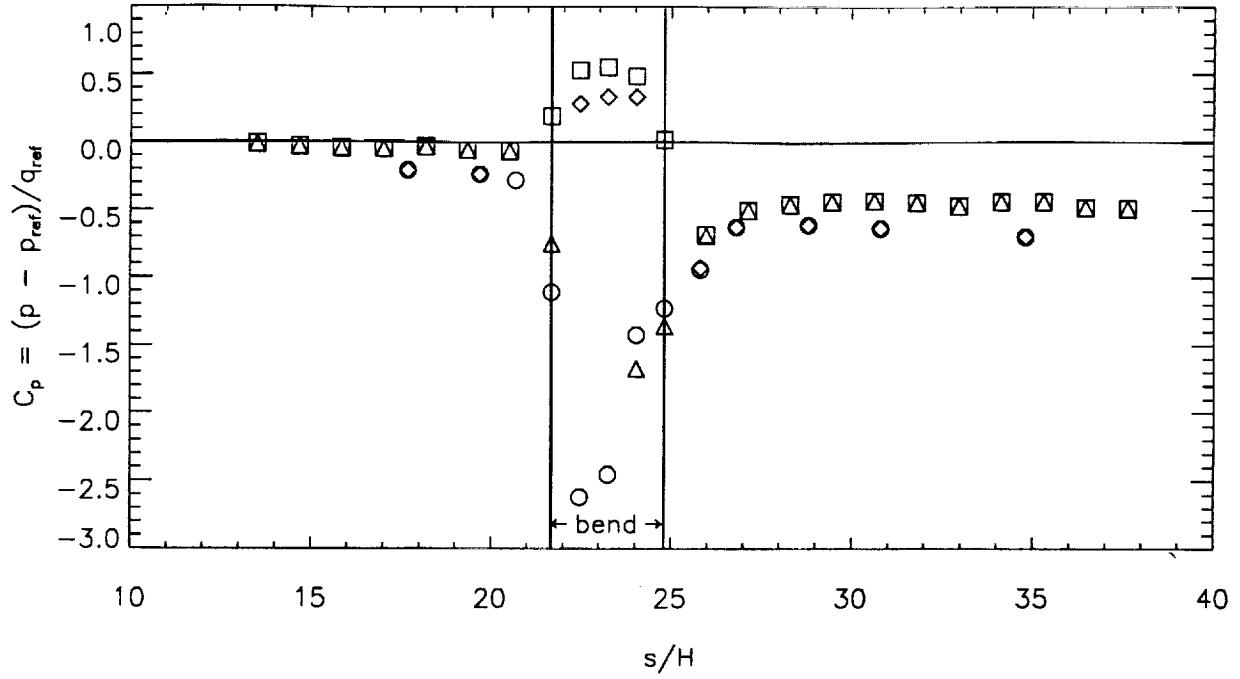
(d) Turbulent shear stress

Figure 23. Summary of Table 23 ($x/H = 12$).

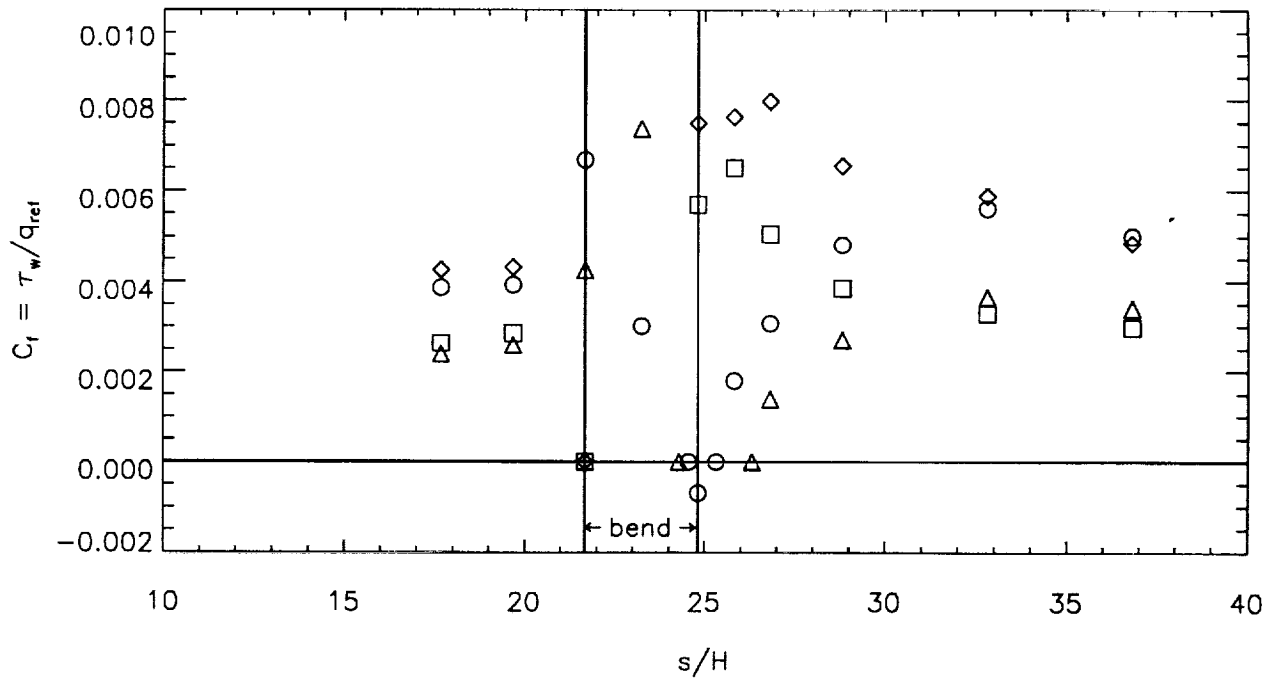
Table 24. Surface pressure and skin friction coefficients in TAD (H = 3.81 cm)

Re	s/H	x/H	θ (deg)	$C_{p,inner}$	$C_{p,outer}$	$C_{f,inner}$	$C_{f,outer}$
10^5	17.67	-4.00		-2.097^{-1}	-2.097^{-1}	3.870^{-3}	4.260^{-3}
	19.67	-2.00		-2.373^{-1}	-2.373^{-1}	3.930^{-3}	4.320^{-3}
	20.67	-1.00		-2.807^{-1}			
	21.67	0.00	0	-1.110^{+0}		6.690^{-3}	0.000^{+0}
	22.46		45	-2.620^{+0}	2.809^{-1}		
	23.24		90	-2.455^{+0}	3.314^{-1}	3.020^{-3}	
	24.03		135	-1.423^{+0}	3.314^{-1}		
	24.55		165			0.000^{+0}	
	24.81	0.00	180	-1.228^{+0}		-6.900^{-4}	7.500^{-3}
	25.31	0.50				0.000^{+0}	
	25.81	1.00		-9.419^{-1}	-9.280^{-1}	1.800^{-3}	7.640^{-3}
	26.81	2.00		-6.236^{-1}	-6.236^{-1}	3.080^{-3}	7.990^{-3}
	28.81	4.00		-6.084^{-1}	-6.084^{-1}	4.820^{-3}	6.560^{-3}
	30.81	6.00		-6.348^{-1}	-6.348^{-1}		
	32.81	8.00				5.610^{-3}	5.880^{-3}
	34.81	10.00		-6.985^{-1}	-6.985^{-1}		
	36.81	12.00				5.000^{-3}	4.850^{-3}
10^5	13.50	-8.17		-1.420^{-2}	-1.420^{-2}		
	14.67	-7.00		-3.310^{-2}	-3.310^{-2}		
	15.83	-5.84		-4.660^{-2}	-4.660^{-2}		
	17.00	-4.67		-5.020^{-2}	-5.020^{-2}		
	17.67	-4.00				2.390^{-3}	2.630^{-3}
	18.17	-3.50		-3.490^{-2}	-3.490^{-2}		
	19.33	-2.34		-5.810^{-2}	-5.810^{-2}		
	19.67	-2.00				2.590^{-3}	2.850^{-3}
	20.50	-1.17		-6.770^{-2}	-6.770^{-2}		
	21.67	0.00	0	-7.518^{-1}	1.900^{-1}	4.260^{-3}	0.000^{+0}
	22.46		45		5.289^{-1}		
	23.24		90		5.530^{-1}	7.380^{-3}	
	24.03		135	-1.674^{+0}	4.859^{-1}		
	24.28		150			0.000^{+0}	
	24.81	0.00	180	-1.357^{+0}	1.780^{-2}		5.700^{-3}
	25.81	1.00					6.510^{-3}
	25.97	1.17		-6.903^{-1}	-6.801^{-1}		
	26.31	1.50				0.000^{+0}	
	26.81	2.00				1.390^{-3}	5.060^{-3}
	27.14	2.34		-5.004^{-1}	-5.004^{-1}		
	28.31	3.50		-4.570^{-1}	-4.570^{-1}		
	28.81	4.00				2.710^{-3}	3.860^{-3}
	29.47	4.67		-4.374^{-1}	-4.374^{-1}		
	30.64	5.84		-4.323^{-1}	-4.323^{-1}		
	31.81	7.00		-4.460^{-1}	-4.460^{-1}		
	32.81	8.00				3.660^{-3}	3.300^{-3}
	32.97	8.17		-4.718^{-1}	-4.718^{-1}		
	34.14	9.34		-4.408^{-1}	-4.408^{-1}		
	35.31	10.50		-4.415^{-1}	-4.415^{-1}		
	36.47	11.67		-4.826^{-1}	-4.826^{-1}		
	36.81	12.00				3.410^{-3}	2.980^{-3}
	37.64	12.84		-4.889^{-1}	-4.889^{-1}		

Legend: $Re=1 \times 10^5$:inner(\odot),outer(\diamond); $Re=1 \times 10^6$:inner(Δ),outer(\square)



(a) Static pressure coefficient



(b) Skin friction coefficient

Figure 24. Summary of Table 24.

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0.29255	29.2474	0.019722	10.1596	-2.14527
0.34335	30.5948	0.083347	9.8180	-2.07070
0.38145	31.0601	0.114581	9.4683	-2.01373
0.41955	31.4845	0.006981	9.2029	-2.20707
0.45765	30.2214	0.494415	9.4403	-1.87735
0.53385	31.3399	0.030467	8.9477	-1.86725
0.57195	30.8784	0.355705	9.2180	-1.98622
0.61005	31.4231	0.466208	9.4566	-2.12587
0.64815	31.6318	0.360486	9.6957	-2.43512
0.90215	31.8623	0.990681	10.3930	-2.84785
1.10536	31.8210	0.933071	10.7703	-3.52544
1.13076	32.1421	0.491273	10.4358	-2.79451
1.18156	31.7504	0.399312	10.2355	-2.87708
1.23236	32.1189	0.333385	10.5069	-2.68231
1.30856	31.8998	0.800902	10.9258	-3.12825
1.61336	32.0281	0.837788	11.6007	-3.55583
1.84196	32.3516	0.271581	10.3388	-3.58068
2.04516	32.2960	0.325500	11.0217	-4.09338
2.19756	32.4867	0.416225	10.1080	-3.62592
2.29915	32.8733	0.059613	9.4906	-2.96551
2.34996	32.9995	0.028368	10.0598	-3.80996
2.40075	32.9080	0.067853	9.1897	-2.82012
2.42616	32.7098	0.308496	9.6748	-3.88539
2.50236	32.8525	0.106142	9.3191	-3.19285
2.57856	32.6240	0.409189	9.4537	-3.50387
2.62936	32.9348	0.265143	9.1111	-3.74124
2.68016	32.6007	0.580029	8.9015	-3.05995
2.78176	32.8384	0.302129	8.6656	-3.34023
2.83256	33.1630	0.129671	7.6851	-2.66846
2.88336	33.0529	0.452731	7.6006	-2.66699
2.93416	33.0713	0.292207	7.4019	-2.58699
3.03576	33.2170	0.184938	7.4239	-2.28563
3.08656	33.4784	0.049531	6.8888	-2.07945
3.12466	33.6972	0.060339	6.5977	-1.88391
3.16276	33.6654	0.128518	6.3503	-1.56341
3.20086	33.6992	0.054198	5.9871	-1.35156
3.23896	33.7655	0.138045	5.9373	-1.35843
3.27706	33.7184	0.176945	5.8147	-1.40037
3.31516	33.6964	0.304439	5.8383	-1.05800
3.35326	33.6918	0.248888	5.6583	-1.08625
3.39136	33.7931	0.221193	5.2863	-0.82299
3.42946	33.6889	0.191700	5.4205	-0.70530
3.46756	33.6751	0.162648	5.1707	-0.43528
3.49296	33.6265	0.262190	5.0398	-0.46979

Figure 26. Sample diskette file 5_8_0.dat.

17.6700	-4.0000	100.000	-0.20970	-0.20970	0.00387	0.00426
19.6700	-2.0000	100.000	-0.23730	-0.23730	0.00393	0.00432
20.6700	-1.0000	100.000	-0.28070	100.00000	100.00000	100.00000
21.6700	0.0000	0.000	-1.11000	100.00000	0.00669	0.00000
22.4600	100.0000	45.000	-2.62000	0.28090	100.00000	100.00000
23.2400	100.0000	90.000	-2.45500	0.33140	0.00302	100.00000
24.0300	100.0000	135.000	-1.42300	0.33140	100.00000	100.00000
24.5500	100.0000	165.000	100.00000	100.00000	0.00000	100.00000
24.8100	0.0000	180.000	-1.22800	100.00000	-0.00069	0.00750
25.3100	0.5000	100.000	100.00000	100.00000	0.00000	100.00000
25.8100	1.0000	100.000	-0.94190	-0.92800	0.00180	0.00764
26.8100	2.0000	100.000	-0.62360	-0.62360	0.00308	0.00799
28.8100	4.0000	100.000	-0.60840	-0.60840	0.00482	0.00656
30.8100	6.0000	100.000	-0.63480	-0.63480	100.00000	100.00000
32.8100	8.0000	100.000	100.00000	100.00000	0.00561	0.00588
34.8100	10.0000	100.000	-0.69850	-0.69850	100.00000	100.00000
36.8100	12.0000	100.000	100.00000	100.00000	0.00500	0.00485

Figure 27. Sample diskette file 5_cp_cf.dat.

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13. ABSTRACT (Maximum 200 words) An experimental study of the low speed internal flow in a two-dimensional strongly-curved U-duct has been conducted in order to acquire fluid dynamic data suitable for evaluating numerical-flow codes. The measurements include surface oil-flow patterns, static pressure distributions obtained with an electronically-scanned pressure system, mean and turbulent velocity profiles acquired with laser-Doppler velocimetry and surface skin friction measured with a laser interferometer skin friction method. The tests were performed at an average Mach number of 0.1, and at Reynolds numbers (based on channel height) of 1×10^5 and 1×10^6 . A high-aspect-ratio geometry together with sidewall boundary-layer suction panels was employed to minimize wall interference effects and obtain nominally two-dimensional flow data.				
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